



FLS 3-phase TEFV cage induction motors Cast iron frame - 0.55 to 750 kW Technical catalogue

# 3-phase TEFV induction motors FLS cast iron 0.55 to 750 kW

# The LEROY-SOMER range of 3-phase motors



# Other LEROY-SOMER motor ranges



Single phase induction motor



3-phase induction motor Aluminium alloy frame



VARMECA variable speed motor



D.C. motor (drip-proof or enclosed)



Motor for variable speed drive systems

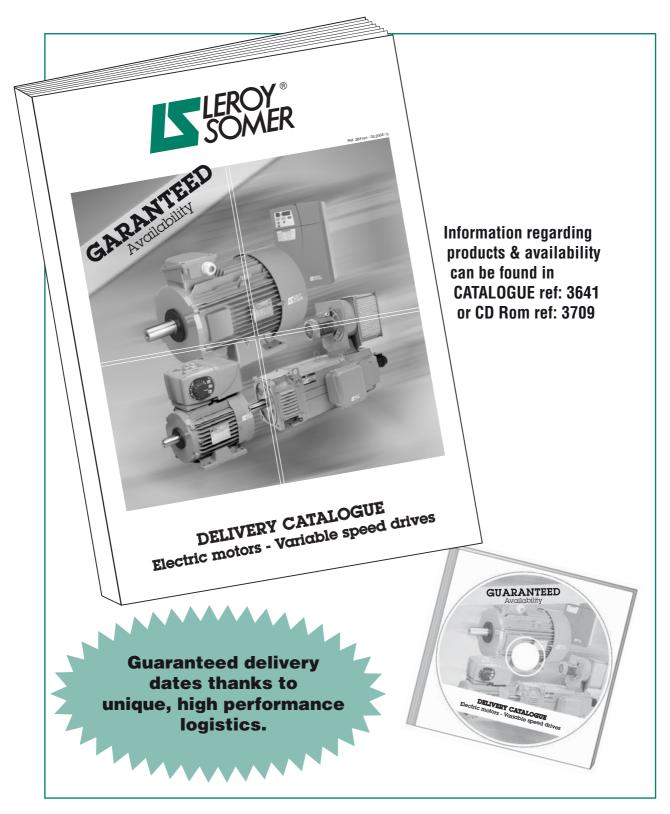


3-phase autosynchronous motor

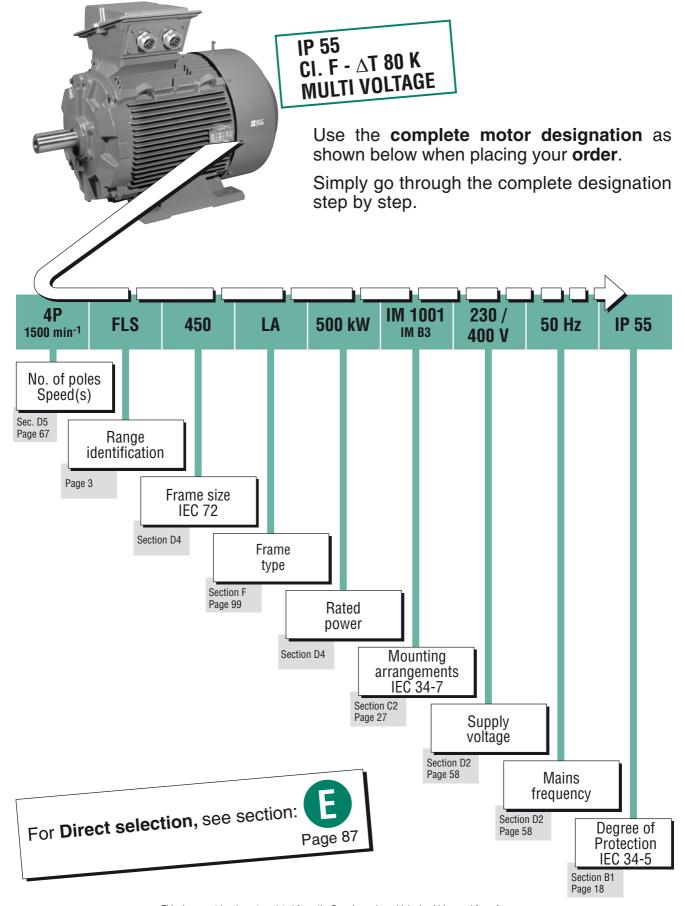


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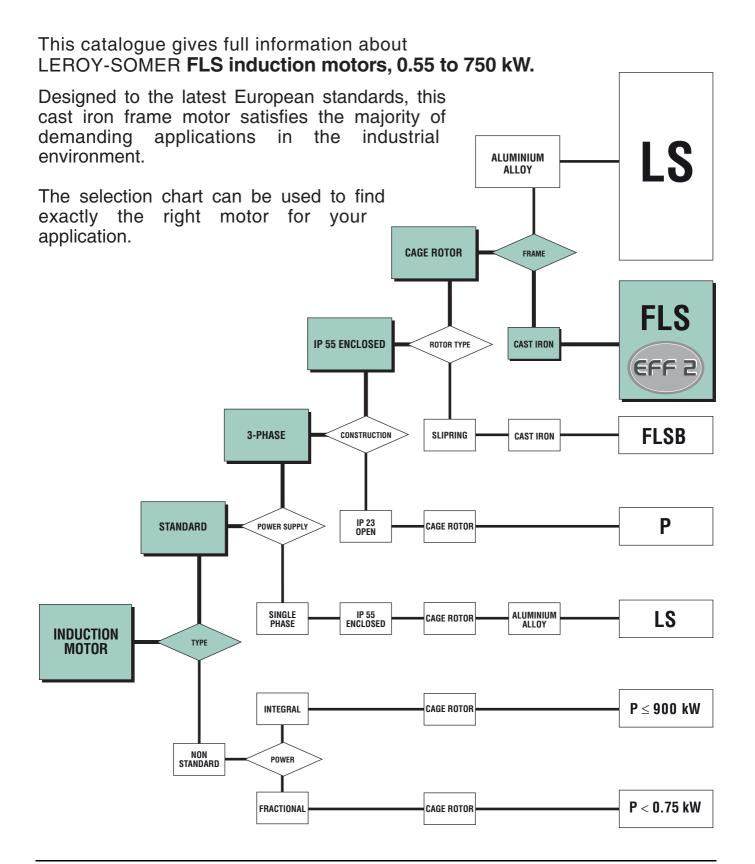
# **3-phase TEFV induction motors FLS** cast iron 0.55 to 750 kW



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# 3-phase TEFV induction motors FLS cast iron 0.55 to 750 kW





# 3-phase TEFV induction motors FLS cast iron

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# A1 - Quality assurance

LEROY-SOMER's quality management system is based on :

- control of procedures right from the initial sales offering until delivery to the customer, including desian. manufacturing start-up and production.

- a total quality policy based on making continuous progress in improving operational procedures, involving all departments in the company in order to give customer satisfaction as regards delivery times, conformity and cost.

- indicators used to monitor procedure performance.

- corrective actions and advancements with tools such as FMECA. QFD. MAVP. MSP/MSQ and Hoshin type improvement workshops on flows, process re-engineering, plus Lean Manufacturing and Lean Office.

- annual surveys, opinion polls and regular visits to customers in order to ascertain and detect their expectations.

Personnel are trained and take part in the analyses and the actions for continuously improving the procedures.

LEROY-SOMER has entrusted the certification of its expertise to various international organisations.

Certification is granted by independent professional auditors, and recognises the high standards of the company's quality assurance procedures. All activities resulting in the final version of the machine have therefore received official ISO 9001: 2000 certification from the DNV. Similarly, our environmental approach has enabled us to obtain ISO 14001: 2004 certification.

Products for particular applications or those designed to operate in specific environments are also approved or certified by the following organisations: CETIM, LCIE, DNV, INERIS, EFECTIS, UL, BSRIA, TUV, CCC, GOST, which check their technical performance against the various standards or recommendations.

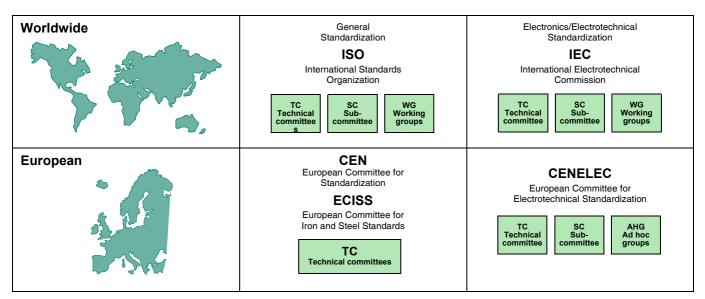




# A2 - Standards and approvals

#### **ORGANIZATION OF STANDARDS AUTHORITIES**

#### International bodies



Country	Initials	Designation
AUSTRALIA	SAA	Standards Association of Australia
BELGIUM	IBN	Institut Belge de Normalisation
CIS (ex-USSR)	GOST	Gosudarstvenne Komitet Standartov
DENMARK	DS	Dansk Standardisieringsraad
FINLAND	SFS	Suomen Standardisoimisliitto
FRANCE	AFNOR including UTE	Association Française de Normalisation including: Union Technique de l'Électricité
GERMANY	DIN/VDE	Verband Deutscher Elektrotechniker
GREAT BRITAIN	BSI	British Standards Institution
ITALY	IEC	Comitato Electtrotechnico Italiano
JAPAN	JIS	Japanese Industrial Standard
NETHERLANDS	NNI	Nederlands Normalisatie - Instituut
NORWAY	NFS	Norges Standardisieringsforbund
SAUDI ARABIA	SASO	Saudi Arabian Standards Organization
SPAIN	UNE	Una Norma Española
SWEDEN	SIS	Standardisieringskommissionen I Sverige
SWITZERLAND	SEV or ASE	Schweizerischer Elektrotechnischer Verein
UNITED STATES	ANSI including NEMA	American National Standards Institute including: National Electrical Manufacturers



# A2 - Standards and approvals

#### Approvals

Certain countries recommend or insist on approval from national organizations.

Approved products must carry the recognized mark on their identification plates.

Country	Initials	Organization
USA	UL	Underwriters Laboratories
CANADA	CSA	Canadian Standards Association
etc.		

Approvals for LEROY-SOMER motors (versions derived from standard construction):

Country	Initials	Certification No.	Application
CANADA	CSA	LR 57 008	Standard adapted range (see section D2.2.3)
USA	UL or AU	E 68554 SA 6704 E 206450	Impregnation systems Stator/rotor assemblies for sealed units Complete motors up to 160 size
SAUDI ARABIA	SASO		Standard range
FRANCE	LCIE INERIS	Various nos.	Sealing, shocks, safety

For specific approved products, see the relevant documents.

#### International and national standard equivalents

	International reference standards	National standards				
IEC	Title (summary)	FRANCE	GERMANY	U.K.	ITALY	SWITZERLAND
60034-1	Ratings and operating characteristics	NFEN 60034-1 NFC 51-120 NFC 51-200	DIN/VDE O530	BS 4999	CEI 2.3.VI.	SEV ASE 3009
60034-2	Determination of losses and efficiency	NFEN 60034-2	DIN/EN 60034-2	BS 4999-102		
60034-5	Classification of degrees of protection	NFEN 60034-5	DIN/EN 60034-5	BS EN 60034-5	UNEL B 1781	
60034-6	Cooling methods	NFEN 60034-6	DIN/EN 60034-6	BS EN 60034-6		
60034-7	Mounting arrangements and assembly layouts	NFEN 60034-7	DIN/EN 60034-7	BS EN 60034-7		
60034-8	Terminal markings and direction of rotation	NFC 51 118	DIN/VDE 0530 Teil 8	BS 4999-108		
60034-9	Noise limits	NFEN 60034-9	DIN/EN 60034-9	BS EN 60034-9		
60034-12	Starting characteristics for single-speed motors powered from the mains $\leq 660~V$	NFEN 60034-12	DIN/EN 60034-12	BS EN 60034-12		SEV ASE 3009-12
60034-14	Mechanical vibration in machines of frame size $>$ 56 mm	NFEN 60034-14	DIN/EN 60034-14	BS EN 60034-14		
60072-1	Dimensions and output powers for machines of between 56 and 400 frame and flanges of between 55 and 1080	NFC 51 104 NFC 51 105	DIN 748 (~) DIN 42672 DIN 42673 DIN 42631 DIN 42676 DIN 42677	BS 4999		
60085	Evaluation and thermal classification of electrical insulation	NFC 26206	DIN/EN 60085	BS 2757		SEV ASE 3584

Note: DIN 748 tolerances do not conform to IEC 60072-1.



# A2 - Standards and approvals

A

#### List of standards quoted in this document

FLS motors comply with the standards quoted in this catalogue

	-	(hore)				
Referenc	e	International standards				
IEC 60034-1	EN 60034-1	Electrical rotating machines: ratings and operating characteristics				
IEC 60034-5	EN 60034-5	Electrical rotating machines: classification of degrees of protection provided by casings of rotating machines.				
IEC 60034-6	EN 60034-6	Electrical rotating machines (except traction): cooling methods				
IEC 60034-7	EN 60034-7	Electrical rotating machines (except traction): symbols for mounting positions and assembly layouts				
IEC 60034-8		Electrical rotating machines: terminal markings and direction of rotation				
IEC 60034-9	EN 60034-9	Electrical rotating machines: noise limits				
IEC 60034-12	EN 60034-12	Starting characteristics for single-speed 3-phase cage induction motors for supply voltages less than or equal to 660V.				
IEC 60034-14	EN 60034-14	Electrical rotating machines: mechanical vibrations of certain machines with a frame size above or equal to 56 mm. Measurement, evaluation and limits of vibrational intensity.				
IEC 60038		IEC standard voltages				
IEC 60072-1		Dimensions and power series for electrical rotating machines: designation of casings between 56 and 400 and flanges between 55 and 1080.				
IEC 60085		Evaluation and thermal classification of electrical insulation.				
IEC 60721-2-1		Classification of natural environment conditions. Temperature and humidity.				
IEC 60892		Effects of an imbalance in the voltage system on the characteristics of three-phase squirrel-cage induction motors.				
IEC 61000-2-10/11 and 2-2		Electromagnetic compatibility (EMC): environment.				
IEC guide 106		Guidelines on the specification of environmental conditions for the determination of operating characteristics of equipment.				
ISO 281		Bearings - Basic dynamic loadings and nominal bearing life.				
ISO 1680	EN 21680	Acoustics - Test code for measuring airborne noise emitted by electrical rotating machines: a method for establishing an expert opinion for free field conditions over a reflective surface.				
ISO 8821		Mechanical vibration - Balancing. Conventions on shaft keys and related parts.				
	EN 50102	Degree of protection provided by the electrical housing against extreme mechanical impacts.				



# A3 - Tolerance on main performance parameters

#### **Tolerances for electromechanical characteristics**

IEC 60034-1 specifies standard tolerances for electromechanical characteristics.

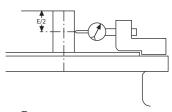
Parameters	Tolerances
Efficiency $\begin{cases} machines P \le 50 \text{ kW} \\ machines P > 50 \text{ kW} \end{cases}$	- 15 % (1 - η) - 10 % (1 - η)
Cos φ	- 1/6 (1 - cos φ) (min 0.02 - max 0.07)
$Slip \begin{cases} machines P < 1 kW \\ machines P \ge 1 kW \end{cases}$	± 30 % ± 20 %
Locked rotor torque	-15%, + 25% of rated torque
Starting current	+ 20 %
Run-up torque	-15 % of rated torque
Breakdown torque	-10 % of rated torque > 1.5 M <sub>N</sub>
Moment of inertia	± 10 %
Noise	+ 3 dB (A)
Vibration	+ 10% of the guaranteed class

- the tolerance is  $\pm$  10% in NEMA-MG1

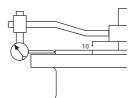
#### **Tolerances and adjustments**

The standard tolerances shown below are applicable to the drawing dimensions given in our catalogues. They comply fully with the requirements of IEC standard 60072-1.

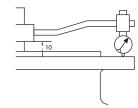
Characteristics	Tolerances
Frame size H ≤ 250	0, — 0.5 mm
≥ 280	0, — 1 mm
Diameter $\varnothing$ of shaft extension:	
- 11 to 28 mm	j6
- 32 to 48 mm	k6
- 55 mm and over	m6
Diameter N of flange spigot	j6 up to FF 500, js6 for FF 600 and over
Key width	h9
Width of drive shaft keyway (normal keying)	N9
Key depth	
- square section	h9
- rectangular section	h11
0 Eccentricity of shaft in flanged motors	
(standard class)	
- diameter > 10 up to 18 mm	0.035 mm
- diameter > 18 up to 30 mm	0.040 mm
- diameter > 30 up to 50 mm	0.050 mm
- diameter > 50 up to 80 mm	0.060 mm
- diameter > 80 up to 120 mm	0.070 mm
② Concentricity of spigot diameter and	
${\Im}$ perpendicularity of mating surface of flange in	
relation to shaft (standard class)	
Flange (FF) or Faceplate (FT):	
- F 55 to F 115	0.08 mm
- F 130 to F 265	0.10 mm
- FF 300 to FF 500	0.125 mm
- FF 600 to FF 740	0.16 mm
- FF 940 to FF 1080	0.20 mm



① Eccentricity of shaft in flanged motors



Concentricity of spigot diameter



③ Perpendicularity of mating surface of flange in relation to shaft





# A4 - Units of measurement and standard formulae

#### A4.1 - ELECTRICITY AND ELECTROMAGNETISM

Parameters				Unit		Units and expressions not recommended
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Frequency Period	Fréquence	f	$f = \frac{1}{T}$	Hz (hertz)		
Electric current	Courant électrique (intensité de)	1		A (ampere)		
Electric potential Voltage Electromotive force	Potentiel électrique Tension Force électromotrice	V U E		V (volt)		
Phase angle	Déphasage	φ	$U = Um \cos \omega t$ $i = im \cos (\omega t - \varphi)$	rad	° degree	
Power factor	Facteur de puissance	$\cos \varphi$				
Reactance Resistance	Réactance Résistance	X R	$Z =  Z ^{\psi \varphi}$ $= R + jX$ $ Z  = \sqrt{R^2 + x^2}$	$\Omega$ (ohm)		<i>j</i> is defined as $j^2 = -1$ $\omega$ pulsation = 2 $\pi$ . <i>f</i>
Impedance	Impédance	Ζ	$X = L\omega - \frac{1}{C\omega}$			
Self inductance	Inductance propre (self)	W	$L = \frac{\Phi}{I}$	H (henry)		
Capacitance	Capacité	С	$C = \frac{Q}{V}$	F (farad)		
Current load, Quantity of electricity	Quantité d'électricité	Q	Q = _/Idt	C (coulomb)	A.h 1 A.h = 3600 C	
Resistivity	Résistivité	ρ	$\rho = \frac{R \cdot S}{l}$	Ω.m		Ω/m
Conductance	Conductance	G	$G = \frac{1}{R}$	S (siemens)		1/Ω = 1 S
Number of turns (coil)	Nombre de tours (spires) de l'enroulement	Ν				
Number of phases	Nombre de phases	т				
Number of pairs of poles	Nombre de paires de pôles	p				
Magnetic field	Champ magnétique	Н		A/m		
Magnetic potential difference Magnetomotive force	Différence de potentiel magnétique Force magnétomotrice Solénation, courant totalisé	Um F, Fm H	$F = \phi H_s d_s$ H = NI	A		The unit AT (ampere-turns) is incorrect because it treats "turn" as a physical unit
Magnetic induction, Magnetic flux density	Induction magnétique, Densité de flux	В		T (tesla) = Wb/m <sup>2</sup>		(gauss) 1 G = 10 <sup>-4</sup> T
Magnetic flux,	Flux magnétique Flux d'induction	Φ	$\Phi = ff_s Bn ds$	Wb (weber)		(maxwell) 1 max = 10 <sup>-8</sup> Wb
Magnetic vector potential	Potentiel vecteur	А		Wb/m		
Permeability	Perméabilité du milieu	$\mu = \mu_o \mu_r$	B = μH	H/m		
Permeability of vacuum	Perméabilité du vide	$\mu_{o}$	μ <sub>o</sub> = 4π10 <sup>-7</sup> H/m			
Permittivity	Permittivité	$\mathcal{E} = \mathcal{E}_0 \mathcal{E}_r$	$\varepsilon_{\rm o} = \frac{1}{36 \pi 10^9}  {\rm F/m}$	F/m		



# A4 - Units of measurement and standard formulae

#### A4.2 - THERMODYNAMICS

Parameters	Parameters					Units and expressions not recommended	
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion	
Temperature Thermodynamic	Température Thermodynamique	Τ		K (kelvin)	temperature Celsius, t, °C T = t + 273.15	°C: Degree Celsius $t_C$ : temp. in °C $t_F$ : temp. in °F f temperature Fahrenheit °F $t = \frac{f-32}{1,8}$ $t_C = \frac{t_F-32}{1,8}$	
Temperature rise	Ecart de température	ΔT		К	°C	1°C = 1 K	
Thermal flux density	Densité de flux thermique	<b>q</b> , φ	$q = \frac{\Phi}{A}$	W/m <sup>2</sup>			
Thermal conductivity	Conductivité thermique	λ		W/m.K			
Total heat transmission coefficient	Coefficient de transmission thermique globale	К	$\varphi = K \left( Tr_2 - Tr_1 \right)$	W/m².K			
Thermal capacity	Capacité thermique	С	$C = \frac{dQ}{dT}$	J/K			
Specific thermal capacity	Capacité thermique massique	с	$c = \frac{C}{m}$	J/kg.K			
Internal energy	Energie interne	U		J			

#### A4.3 - NOISE AND VIBRATION

Parameters	Unit		Units and expressions not recommended			
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Sound power level	Niveau de puissance acoustique	L <sub>w</sub>	$L_{\rm W} = 10  \log(P/P_{\rm O})$ ( $P_{\rm O} = 10^{-12}  W$ )	dB (decibel)		Ig logarithm to base 10 Ig10 = 1
Sound pressure level	Niveau de pression acoustique	L <sub>P</sub>	$L_{\rm P} = 20  \log(P/P_{\odot})$ $(P_{\odot} = 2x10^{-5}  Pa)$	dB		

#### A4.4 - DIMENSIONS

Parameters						Units and expressions not recommended
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Angle (plane angle)	Angle (angle plan)	α, β, Τ, φ		rad	degree: ° minute: ' second: "	$180^\circ = \pi$ rad = 3.14 rad
Length Width Height Radius	Longeur Largeur Hauteur Rayon Longueur curviligne	l b h r s		m (metres)	micrometre	cm, dm, dam, hm 1 inch = 1" = 25.4 mm 1 foot = 1' = 304.8 mm μm micron μ angström: A = 0.10 nm
Area Volume	Aire, superficie Volume	A, S V		m <sup>2</sup> m <sup>3</sup>	litre: I liter: W	1 square inch = 6.45 10 <sup>-4</sup> m <sup>2</sup> UK gallon = 4.546 10 <sup>-3</sup> m <sup>3</sup> US gallon = 3.785 10 <sup>-3</sup> m <sup>3</sup>



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# A4 - Units of measurement and standard formulae

#### A4.5 - MECHANICS AND MOVEMENT

Parameters				Unit		Units and expressions not recommended	
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion	
Time	Temps	t			minute: min	Symbols ' and " are reserved for	
Time interval / duration	Intervalle de temps/durée			s (second)	hour: h	angles	
Period (duration of cycle)	Période (durée d'un cycle)	Т			day: d	minute not written as mn	
Angular velocity Rotational frequency	Vitesse angulaire Pulsation	ω	$\omega = \frac{d\varphi}{dt}$	rad/s			
Angular acceleration	Accélération angulaire	α	$\alpha = \frac{d\omega}{dt}$	rad/s <sup>2</sup>			
Speed	Vitesse	u, v, w,	$v = \frac{ds}{dt}$	_	1 km/h = 0.277 778 m/s		
Velocity	Célérité	с		m/s	1 m/min = 0.016 6 m/s		
Acceleration	Accélération	а	$a = \frac{dv}{dt}$	m/s²			
Acceleration	Accélération						
of free fall	de la pesanteur	$g = 9.81 m/s^2$	in Paris				
Speed of rotation	Vitesse de rotation	Ν		S <sup>-1</sup>	min <sup>-1</sup>	tr/mn, RPM, TM	
Weight	Masse	т		kg (kilogram)	tonne: t 1 t = 1000 kg	kilo, kgs, KG 1 pound: 1 lb = 0.4536 kg	
Mass density	Masse volumique	ρ	dm dV	kg/m³			
Linear density	Masse linéique	$ ho_{ m e}$	dm dL	kg/m			
Surface density	Masse surfacique	$ ho_{A}$	dm dS	kg/m <sup>2</sup>			
Momentum	Quantité de mouvement	Р	p = m.v	kg. m/s			
Moment of inertia	Moment d'inertie	J, I	$I = \sum m.r^2$	kg.m²		$J = \frac{MD^2}{4}   kg.m^2$ pound per square foot = 1 lb.ft <sup>2</sup> = 42.1 x 10 <sup>-3</sup> kg.m <sup>2</sup>	
Force Weight	Force Poids	F G	G = m.g	N (newton)		kgf = kgp = 9.81 N pound force = lbF = 4.448 N	
Moment of force	Moment d'une force	М	M = F.r	N.m		mdaN, mkg, m.N	
Torque		Τ				1 mkg = 9.81 N.m 30.48 cm.lbF = 1.356 N.m 1 in.lbF = 0.113 N.m	
Pressure	Pression	p	$p = \frac{F}{S} = \frac{F}{A}$	Pa (pascal)	bar 1 bar = 10⁵ Pa	1 kgf/cm <sup>2</sup> = 0.981 bar 1 psi = 6894 N/m <sup>2</sup> = 6894 Pa 1 psi = 0.06894 bar	
						1 atm = 1.013 x 10 <sup>5</sup> Pa	
Normal stress	Contrainte normale	$\sigma$		Pa		kg/mm <sup>2</sup> , 1 daN/mm <sup>2</sup> = 10 MPa	
Shear stress,	Contrainte tangentielle Cission	τ		Leroy-Somer use		psi = pound per square inch 1 psi = 6894 Pa	
Friction coefficient	Facteur de frottement	μ				incorrectly = cœfficient friction $f$	
Work	Travail	W	W = F.1			1 N.m = 1 W.s = 1 J	
Energy	Énergie	E			Wh = 3600 J	1 kgm = 9.81 J	
Potential energy	Énergie potentielle	Ep		J (joule)	(watt-hour)	(calorie) 1 cal = 4.18 J	
Kinetic energy	Énergie cinétique	Ek				1 Btu = 1055 J (British thermal unit)	
Quantity of heat	Quantité de chaleur	Q P	147	M (moth)		(British thermal unit) 1  ch = 736  W	
Power Volumetric flow	Puissance Débit volumique	Р qv	$P = \frac{W}{t}$	W (watt) m³/s		1 ch = 736 W 1 HP = 746 W	
			$q_{\rm V} = \frac{dV}{dt}$	_			
Efficiency	Rendement	η		< 1		%	
Dynamic viscosity	Viscosité dynamique	η, μ		Pa.s		poise, 1 P = 0.1 Pa.s	
Kinematic viscosity	Viscosité cinématique	v	$v = \frac{\eta}{\rho}$	m²/s		stokes, 1 St = 10 <sup>-4</sup> m <sup>2</sup> /s	



# A5 - Unit conversions

Unit	MKSA (IS international system)	AGMA (US system)		
Length	1 m = 3.2808 ft 1 mm = 0.03937 in	1 ft = 0.3048 m 1 in = 25.4 mm		
Weight	1 kg = 2.2046 lb	1 lb = 0.4536 kg		
Torque	1 Nm = 0.7376 lb.ft 1 N.m = 141.6 oz.in	1 lb.ft = 1.356 N.m 1 oz.in = 0.00706 N.m		
Force	1 N = 0.2248 lb	1 lb = 4.448 N		
Moment of inertia	1 kg.m² = 23.73 lb.ft²	1 lb.ft² = 0.04214 kg.m²		
Power	1 kW = 1.341 HP	1 HP = 0.746 kW		
Pressure	1 kPa = 0.14505 psi	1 psi = 6.894 kPa		
Magnetic flux	1 T = 1 Wb / m <sup>2</sup> = 6.452 10 <sup>4</sup> line / in <sup>2</sup>	1 line / in² = 1.550 10 <sup>-5</sup> Wb / m²		
Magnetic losses	1 W / kg = 0.4536 W / lb	1 W / lb = 2.204 W / kg		

Multiples and sub-multiples						
Factor by which the unit is multiplied	Prefix to be placed before the unit name	Symbol to be placed before that of the unit				
10 <sup>18</sup> or 1,000,000,000,000,000,000	exa	E				
10 <sup>15</sup> or 1,000,000,000,000,000	peta	Р				
10 <sup>12</sup> or 1,000,000,000,000	tera	т				
10 <sup>9</sup> or 1,000,000,000	giga	G				
10 <sup>6</sup> or 1,000,000	mega	М				
10 <sup>3</sup> or 1,000	kilo	k				
10 <sup>2</sup> or 100	hecto	h				
10 <sup>1</sup> or 10	deca	da				
10 <sup>-1</sup> or 0.1	deci	d				
10 <sup>-2</sup> or 0.01	centi	C				
10 <sup>-3</sup> or 0.001	milli	m				
10 <sup>-6</sup> or 0.000,001	micro	μ				
10 <sup>-9</sup> or 0.000,000,001	nano	n				
10 <sup>-12</sup> or 0.000,000,000,001	pico	р				
10 <sup>-15</sup> or 0.000,000,000,000,001	femto	f				
10 <sup>-18</sup> or 0.000,000,000,000,000,001	atto	a				



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# A6 - Standard formulae used in electrical engineering

#### A6.1 - MECHANICAL FORMULAE

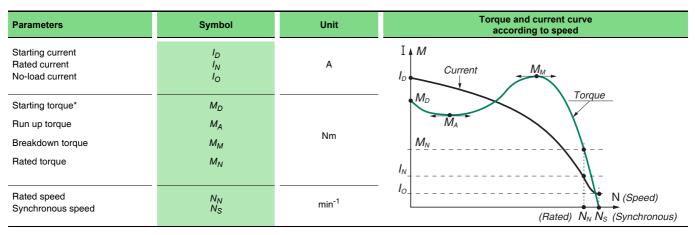
Title	Formula	Unit	Definitions / notes
Force	<i>F</i> = <i>m</i> · γ	F in N m in kg γ in m/s <sup>2</sup>	A force <i>F</i> is the product of a mass <i>m</i> by an acceleration $\gamma$
Weight	G = m ⋅ g	G in N <i>m</i> in kg g = 9.81 m/s <sup>2</sup>	
Torque	$M = F \cdot r$	<i>M</i> in N.m <i>F</i> in N <i>r</i> in m	The torque $M$ of a force in relation to an axis is the product of that force multiplied by the distance $r$ of the point of application of $F$ in relation to the axis.
Power - Rotation	$P = M \cdot \omega$	P in W M in N.m $\omega$ in rad/s	Power <i>P</i> is the quantity of work yielded per unit of time $\omega = 2\pi N/60$ where <i>N</i> is the speed of rotation in min <sup>-1</sup>
- Linear	P = F · V	P in W F in N V in m/s	V = linear velocity
Acceleration time	$t = J \cdot \frac{\omega}{M_{a}}$	<i>t</i> in s J in kg.m <sup>2</sup> $\omega$ in rad/s $M_{\rm a}$ in Nm	<i>J</i> is the moment of inertia of the system $M_a$ is the moment of acceleration Note: all the calculations refer to a single rotational speed $\omega$ where the inertias at speed $\omega$ " are corrected to speed $\omega$ by the following calculation: $J_{\omega} = J_{\omega'} \cdot \left(\frac{\omega}{\omega}\right)^2$
Moment of inertia Centre of gravity Solid cylinder	$J = m \cdot r^2$ $J = m \cdot \frac{r^2}{2}$	<i>J</i> in kg.m <sup>2</sup> <i>m</i> in kg	
around its shaft Hollow cylinder around its shaft	$J = m \cdot \frac{r^2}{2}$ $J = m \cdot \frac{r^2_1 + r^2_2}{2}$	<i>r</i> in m	
Inertia of a mass in linear motion	$J = m \cdot \left(\frac{v}{\omega}\right)^2$	J in kg.m <sup>2</sup> m in kg v in m/s $\omega$ in rad/s	The moment of inertia of a mass in linear motion transformed to a rotating motion.



# A6 - Standard formulae used in electrical engineering

#### A6.2 - ELECTRICAL FORMULAE

Title	Formula	Unit	Definitions / notes
Accelerating torque	$M_{a} = \frac{M_{D} + 2M_{A} + 2M_{M} + M_{N}}{6} - M_{r}$ General formula: $M_{a} = \frac{1}{N_{N}} \int_{0}^{N_{N}} (M_{mot} - M_{r}) dN$	Nm	Moment of acceleration $M_A$ is the difference between the motor torque $M_{mot}$ (estimated), and the resistive torque $M_r$ . N = instantaneous speed N <sub>N</sub> = rated speed
Power required by the machine	$\boldsymbol{P} = \frac{\boldsymbol{M} \cdot \boldsymbol{\omega}}{\eta_{A}}$	<i>P</i> in W <i>M</i> in N.m $\omega$ in rad/s $\eta_A$ no unit	$\eta_{\rm A}$ expresses the efficiency of the driven machine. M is the torque required by the driven machine.
Power drawn by the 3-phase motor	$P = \sqrt{3} \cdot U \cdot I \cdot \cos \varphi$	<i>P</i> in W <i>U</i> in V / in A	$\varphi$ phase angle by which the current lags or leads the voltage. U armature voltage. I current required by the driven machine.
Reactive power absorbed by the motor	$\mathbf{Q} = \sqrt{3} \cdot \mathbf{U} \cdot \mathbf{I} \cdot \boldsymbol{\sin} \varphi$	Q in VAR	
Reactive power supplied by a bank of capacitors	$\mathbf{Q} = \sqrt{3} \cdot \mathbf{U}^2 \cdot \mathbf{C} \cdot \boldsymbol{\omega}$	U in V C in $\mu$ F $\omega$ in rad/s	U = voltage at the capacitor terminals C = capacitor capacitance $\omega$ = rotational frequency of supply phases ( $\omega$ = 2 $\pi$ f)
Apparent power	$S = \sqrt{3} \cdot U \cdot I$ $S = \sqrt{P^2 + Q^2}$	S in VA	
Power supplied by 3-phase motor	$P = \sqrt{3} \cdot U \cdot I \cdot \cos \varphi \cdot \eta$		$\eta$ expresses motor efficiency at the point of operation under consideration.
Slip	$g = \frac{N_{\rm S} - N}{N_{\rm S}}$		Slip is the difference between the actual motor speed N and the synchronous speed $N_S$
Synchronous speed	$N_{\rm S} = \frac{120 \cdot f}{p}$	N <sub>S</sub> in min⁻¹ f in Hz	<i>p</i> = number of poles <i>f</i> = frequency of the power supply



\* Torque is the usual term for expressing the moment of a force.



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# B1 - Definition of "Index of Protection" (IP/IK)

#### Indices of protection of electrical equipment enclosures In accordance with IEC 60034-5 - EN 60034-5 (IP) - EN 50102 (IK)

FLS motors are IP 55 / IK 08 as standard

20 J

First nu	mber : on against solid	objects	Second number : protection against liquids				Third number: mechanical protection			
IP	Tests	Definition	IP	Tests	Definition	IK	Tests	Definition		
0		No protection	0		No protection	00		No protection		
1	Ø 50 mm	Protected against solid objects of over 50 mm (eg : accidental hand contact)	<b>1</b> ර		Protected against vertically dripping water (condensation)	01	150 g	Impact energy : 0.15 J		
2	Ø 12 mm	Protected against solid objects of over 12 mm (eg : finger)	2	15 I	Protected against water dripping up to 15 from the vertical	02	200 g † 10 cm	Impact energy : 0.20 J		
3	Ø 2.5 mm	Protected against solid objects of over 2.5 mm (eg : tools, wire)	<b>3</b> ර		Protected against rain falling at up to 60 from the vertical	03	250 g t t 15 cm	Impact energy : 0.37 J		
4	Ø1mm	Protected against solid objects of over 1 mm (eg : small tools, thin wire)	<b>4</b>	0	Protected against water splashes from all directions	04	250 g 20 cm	Impact energy : 0.50 J		
5	O	Protected against dust (no deposits of harmful material)	<b>5</b> ▲		Protected against jets of water from all directions	05	350 g t 20 cm	Impact energy : 0.70 J		
6	O	Totally protected against dust	6		Protected against jets of water comparable to heavy seas	06	250 g 40 cm	Impact energy : 1 J		
				0.15 m	Protected against the effects of immersion to depths of between 0.15 and 1 m	07	0.5 kg 40 cm	Impact energy : 2 J		
Example: IP 55 m	achine		8 ᠔᠔m		Protected against the effects of prolonged immersion under pressure	08	1.25 kg 40 cm	Impact energy : 5 J		
5. : Mach Test	<ul> <li>P: Index of protection</li> <li>G. Machine protected against dust and accidental contact. Test result: no dust enters in harmful quantities, no risk of direct contact</li> </ul>						2.5 kg 40 cm	Impact energy : 10 J		
.5 : Mach	ine protected ag	e test will last for 2 l ainst jets of water fr	3 m distance	10	5 kg 40 cm	Impact energy :				

Machine protected against jets of water from all directions from hoses at 3 m distance with a flow rate of 12.5 l/min at 0.3 bar. The test will last for 3 minutes. Test result: no damage from water projected onto the machine.



# **B2** - Environmental limitations

# B2.1 - NORMAL OPERATING CONDITIONS

**a** / According to IEC 60034-1, motors can operate in the following normal conditions:

- ambient temperature within the range -16 and +40°C
- altitude less than 1000 m
- atmospheric pressure: 1050 hPa (mbar)

#### b / Power correction factor:

For operating conditions outside these limits, apply the power correction coefficient shown in the chart on the right *which maintains the thermal reserve*, as a function of the altitude and ambient temperature.

#### **B2.2 - HARSH ENVIRONMENT**

The construction of FLS cast iron motors is particularly recommended for applications in harsh operating conditions (impact, vibration) such as the iron and steel, cement, paper or sugar industries, etc.

Also, for operation in high or low temperatures, the choice of materials for the enclosure (adjacent expansion coefficients and high thermal inertia) makes the cast iron motor the best choice for this type of duty.

Cast iron motor required	Cast iron or alu- minium motor*	Cast iron motor required	
-4	DC +10	DOC	

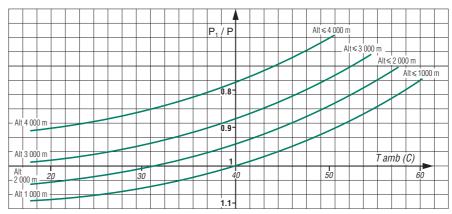
\* in this temperature zone, the choice of cast iron or aluminium motor depends on other requirements.

The construction of FLSC cast iron motors with CORROBLOC anti-corrosion finish is required when the environmental conditions are humid, corrosive or harsh, for example polluted with:

- halogen products (chlorine, fluoride, etc)
- alkaline, sulphurous products
- alcohol
- anhydrides
- hydraulic or vegetable oils
- mercury

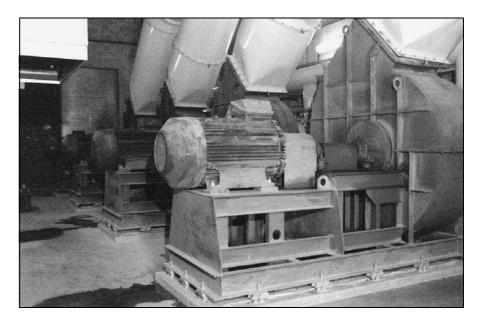
The essential criteria for anti-corrosion protection include stainless steel components, protection of active parts (stator and rotor), and special finishes.

#### Correction coefficient table



Note: the output power can only be corrected upwards once the ability of the motor to start the load has been checked.







# **B2** - Environmental limitations

#### B2.3 - RELATIVE AND ABSOLUTE HUMIDITY

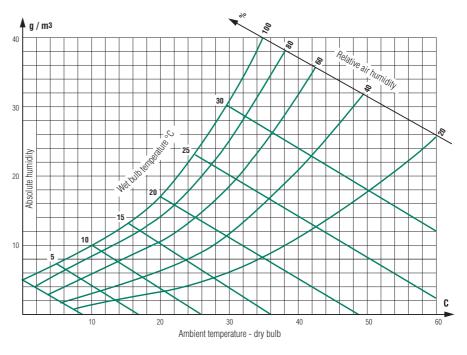
#### Measuring the humidity

Humidity is usually measured by the "wet and dry bulb thermometer" method.

Absolute humidity, calculated from the readings taken on the two thermometers, can be determined using the chart on the right. The chart also provides relative humidity figures.

To determine the humidity correctly, a good air flow is required for stable readings, and accurate readings must be taken on the thermometers. During the construction of cast iron motors, the materials of the various components which are in contact with one another are selected so as to minimise deterioration by galvanic effect. The voltages in the metal combinations used (cast iron-steel; cast iron-aluminium; steel-aluminium; steel-tin) are too low to cause deterioration. Only the brass cable gland in contact with the cast iron could cause problems, so it is fitted (when necessary) with an elastomer seal to reduce the risk.

In temperate climates, relative humidity is generally between 60 and 90%. For the relationship between relative humidity and motor impregnation, especially where humidity and temperature are high, see table on next page.



#### **B2.4 - DRAIN HOLES**

Drain holes (M6 up to and including frame size 250, M8 thereafter) are provided at the lowest points of the enclosure, depending on the operating position (IM etc), to drain off any moisture that may have accumulated inside during cooling of the machine.

These holes are sealed with plugs which must be removed and then refitted from time to time.

*Different types of plug:* screw, siphon, breather, plastic plug.

For certain applications in particular, it is advisable to leave the drain holes open at the expense of the IP... index of protection.

#### **B2.5 - DRIP COVERS**

For machines operating outdoors, with the drive shaft downwards, drip covers are recommended.

This is an option and should be specified on the order if required.

(dimensions: section G3)





# B3 - Impregnation and enhanced protection

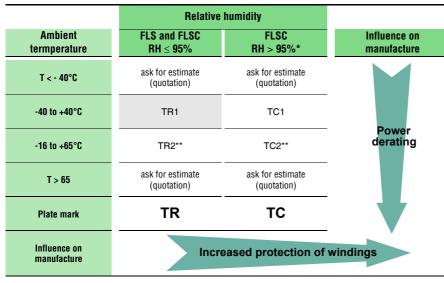
#### B3.1 - NORMAL ATMOSPHERIC PRESSURE (750 mm HG)

The selection table below can be used to find the method of manufacture best suited to particular environments in which temperature and relative humidity show large degrees of variation (see relative and absolute humidity calculation method, on preceding page).

The symbols used refer to permutations of components, materials, impregnation methods and finishes (varnish or paint).

The protection of the winding is generally described by the term "tropicalization".

For high humidity environments, we recommend that the windings are preheated (see section B4.1).



\* Non-condensing

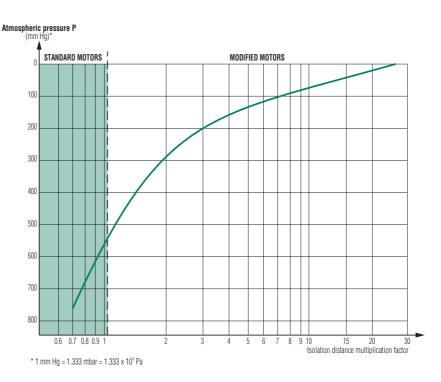
\*\* Caution, motor derating may be required (please consult Leroy-Somer).

Standard impregnation

#### B3.2 - INFLUENCE OF ATMOS-PHERIC PRESSURE

As atmospheric pressure decreases, air particles rarefy and the environment becomes increasingly conductive.

The curve below shows the increase in isolation distance required, according to atmospheric pressure.



#### Solutions for permanent applications: offers based on specification

- P > 550 mm Hg: Standard impregnation according to previous table - Possible derating or forced ventilation.

- P > 200 mm Hg: Coating of bearings Flying leads up to a zone at P ~ 750 mm Hg Derating to take account of insufficient ventilation - Forced ventilation.
- $\mathsf{P}$  < 200 mm Hg: Special manufacture based on specification.

In all cases, these problems should be resolved by a special contract worked out on the basis of a specification.



# **B4 - Heaters**

#### **B4.1 - SPACE HEATERS**

Severe climatic conditions, e.g.  $T \text{ amb} < -40^{\circ}\text{C}$ , RH > 95% etc, may require the use of space heaters (fitted to the motor windings) which serve to maintain the average temperature of the motor, provide trouble-free starting, and eliminate problems caused by condensation (loss of insulation).

The heater supply wires are brought out to a terminal block in the motor terminal box. The heaters must be switched off while the motor is running.

Motor type	No. of poles	Power: P(W)
FLS 80	2 - 4 - 6 - 8	10
FLS 90 to FLS 132	2 - 4 - 6 - 8	25
FLS 160 to FLS 200	2 - 4 - 6 - 8	50
FLS 225 and FLS 250	2 - 4 - 6 - 8	100
FLS 280 and FLS 315	2 - 4 - 6 - 8	100*
FLS 355 to FLS 450	2 - 4 - 6 - 8	150*

The space heaters use 200/240V, single-phase, 50 or 60 Hz.

\* It is possible to increase the power when asking for estimate (quotation).

#### **B4.2 - D.C. INJECTION**

An alternative to the use of space heaters is to inject direct current into two of the phases wired in series from a D.C. voltage source which can give the total power indicated in the table above. This method can only be used on motors of less than 10 kW.

This is easily calculated: if R is the resistance of the windings in series, the D.C. voltage will be given by the equation (Ohm's law):

$$\mathsf{U}_{(\mathsf{V})} = \sqrt{\mathsf{P}_{(\mathsf{W})} \cdot \mathsf{R}_{(\Omega)}}$$

Resistance should be measured with a micro-ohmmeter.

#### **B4.3 - A.C. INJECTION**

A single-phase A.C. voltage (from 10 to 15% of rated voltage), can be used between 2 phases placed in series.

This method can be used on the whole FLS range.





# B5 - External finish

LEROY-SOMER motors are protected with a range of surface finishes. The surfaces receive appropriate special treatments, as shown below. Standard FLSC motors conform to System IIIa

#### Preparation of surfaces

SURFACE	PARTS	TREATMENT
Cast iron	All cast iron elements (internal and external) (end shields, housing, terminal box, etc)	- SA 2.5 shot blasting - Application of primer (25 to 30 μm) or a coat of polyvinyl butyral 20 μm or epoxy ester
Steel	Terminal box accessories	Phosphatization + Primer
Steer	Covers	Electrostatic painting or Epoxy powder

#### Definition of atmospheres

An atmosphere is said to be harsh when components are attacked by bases, acids or salts. It is said to be corrosive when components are attacked by oxygen.

#### Painting systems

PRODUCTS	ATMOSPHERE	SYSTEM	APPLICATIONS	RESISTANCE TO SALINE MIST standard NFX 41002
	Moderately harsh, humid, accidental alkaline or acidic splashes	Па	1 base coat (surface treatment) 1 coat polyurethane 25/40 μm	250 hours
LEROY-SOMER motors	Coastal Corrosive	Ша	1 base coat (surface treatment) 1 base coat Epoxy before assembly on inside and outside of flanges, cast iron housings and terminal boxes 30/40 μm 1 coat polyurethane finish 25/40 μm	350 hours
	Special conditions Very harsh, polluted with chlorinated or sulphurous products	IVb	1 base coat (surface treatment) 1 base coat Epoxy 35/40 μm 1 intermediate coat Epoxy 35/40 μm 1 coat Epoxy finish 35/40 μm	500 hours

Exposure to saline mist conforming to standard NFX 41b002 (5% of NaCl at 6 < PH < 7.5 at 35° and 1 bar). For very specific atmospheres, special or adapted systems are available. Please consult Leroy-Somer.

LEROY-SOMER standard paint colour reference:

RAL 6000



# **B6** - Interference suppression

#### Airborne interference

#### Emission

For standard motors, the housing acts as an electromagnetic screening, reducing electromagnetic emissions measured at 0.25 metres from the motor to approximately 5 gauss ( $5 \times 10^{-4}$  T).

However, electromagnetic emissions may be noticeably reduced by a special construction of aluminium alloy end shields and a stainless steel shaft.

#### Immunity

The construction of motor housings (especially finned aluminium alloy frames) isolates external electromagnetic sources to the extent that any field penetrating the casing and magnetic circuit will be too weak to interfere with the operation of the motor.

#### Power supply interference

The use of electronic systems for starting, speed control or power supply can create harmonics on the supply lines which may interfere with the operation of machines. These phenomena are taken into account in determining the machine dimensions, which act as quenching chokes in this respect.

The IEC 61000 standard, currently in preparation, will define permissible rejection and immunity rates: only then will machines for general distribution (especially single-phase motors and commutator motors) have to be fitted with suppression systems.

Three-phase squirrel cage machines do not in themselves produce interference of this type. Mains connection equipment (contactors) may, however, need interference protection.

Application of Directive 89-336 modified by Directives 92-31 and 93-68 concerning electromagnetic compatibility (EMC).

#### a - for motors only

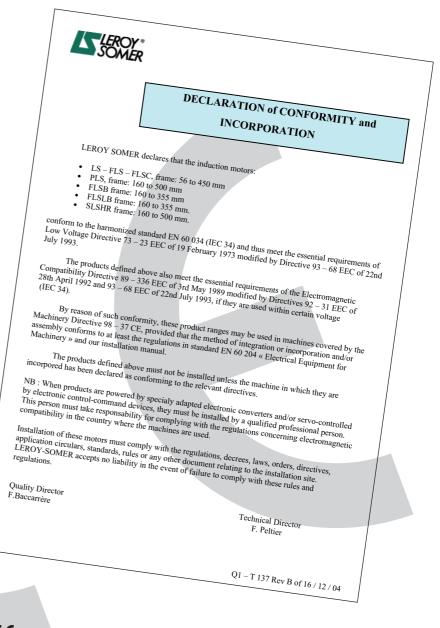
According to amendment 1 of IEC 60034-1, induction motors are not transmitters and do not produce interference (via carried or airborne signals) and therefore conform inherently to the essential requirements of the EMC directives.

## b - for motors supplied by inverters (at fixed or variable frequency)

In this case, the motor is only a subassembly of a device which the system builder must ensure conforms to the essential requirements of the EMC directives.

# Application of the Low Voltage Directive 73-23 EEC modified by Directive 93/68

All motors have been subject to this directive since 1 July 1997. The main requirements concern the protection of people, animals and property against risks caused by operation of the motors (see the commissioning and maintenance manual for precautions to be taken).



#### CE product marking

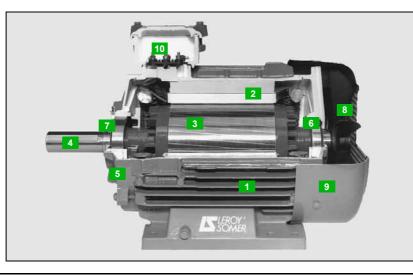
The fact that motors conform to the essential requirements of the Directives is shown by the **C** mark on their nameplates and/or packaging and documentation.



# C1 - Components

#### **C1.1 - DESCRIPTION OF STANDARD FLS CAST IRON MOTORS**

Component	Materials	Remarks
1 Finned housing	Cast iron	<ul> <li>with integral feet, or without feet</li> <li>4, 6 or 8 fixing holes for foot-mounted housings</li> <li>lifting rings for frame size ≥ 100</li> <li>earth terminal on foot or fin or terminal box base</li> </ul>
2 Stator	Insulated low-carbon magnetic steel laminations Insulated electroplated copper	<ul> <li>low carbon content guarantees long-term lamination pack stability</li> <li>welded packs</li> <li>semi-enclosed slots</li> <li>class F insulation</li> </ul>
3 Rotor	Insulated low-carbon magnetic steel laminations carbon Aluminium (A5L) or copper	<ul> <li>- inclined cage bars</li> <li>- rotor cage pressure die-cast in aluminium (or alloy for special applications) or soldered in copper</li> <li>- shrink-fitted to shaft, or keyed for soldered rotors</li> <li>- rotor balanced dynamically, level A, 1/2 key</li> </ul>
4 Shaft	Steel	<ul> <li>for frame size ≤ 132:</li> <li>shaft end fitted with screw and washer</li> <li>closed keyway</li> <li>for frame size ≥ 160:</li> <li>tapped hole</li> <li>open keyway</li> </ul>
5 End shields	Cast iron	
6 Bearings and lubrication		<ul> <li>- ball bearings C3 or C4 play</li> <li>- type ZZ "greased for life" up to frame size 132</li> <li>- semi-protected or open type from frame size 160 upwards, regreasable</li> <li>- bearings preloaded at NDE up to 315 S, preloaded at DE from size 315 M upwards</li> </ul>
7 Labyrinth seal Lipseals	Plastic or steel Synthetic rubber	- labyrinth seal at drive end for foot-mounted motors, frame size $\leq$ 132 - seal at drive end for foot and flange or flange-mounted motors, frame size $\leq$ 132 - lipseal at drive end and non drive end for frame sizes 160 to 225 MT inclusive - labyrinth seal at drive end and non drive end for frame sizes $\geq$ 355 LK - decompression grooves for 225 M to 355 LD
8 Fan	Composite material up to and including size 280. Metal from 315 ST upwards.	- 2 directions of rotation: straight blades
9 Fan cover	Pressed steel	<ul> <li>fitted, on request, with a drip cover for operation in vertical position, shaft end facing down.</li> </ul>
10 Terminal box	Cast iron body for all frame sizes. Sheet steel cover from size 80 to 132. Cast iron cover for larger sizes.	<ul> <li>IP 55</li> <li>fitted with a terminal block with 6 terminals up to 355 LD, 6 or 12 terminals thereafter</li> <li>ISO plastic up to 132, terminal box fitted with cable gland.</li> <li>sizes 160 to 450, cable gland baseplate without drilled holes (optional horn or cable gland).</li> <li>1 earth terminal in each terminal box</li> </ul>



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# C1 - Components

#### **C1.2 - DESCRIPTION OF THE FLSC CORROBLOC FINISH**

The CORROBLOC finish is a top coat for the FLS cast iron motor described in C2.1. In addition to the basic cast iron motor construction, its special finishes resist corrosion in particularly harsh environments, and these qualities are enhanced with age.

Component	Materials	Remarks
2 Stator 3 Rotor		- dielectric and anti-corrosion protection of the stator (coil end turns) and rotor
Nameplate	Stainless steel	- nameplate: indelible marking
Screws	Stainless steel	- captive screws for terminal box lid (frame size $\leq$ 132)
Terminal box	Body and cover in cast iron	
Cable gland	Brass	
External finish		- system IIIa as defined on page 23

#### **C1.3 - EXTENSION TO THE FLSC CORROBLOC RANGE**

Applications:

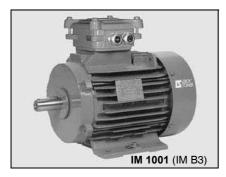
- IP 55 W damp protection (with the customer's agreement),
- IP 56 dust and damp protection, non-ventilated, for marine applications with intermittent duty,
- 500 hours resistance to saline mist,

- stainless steel.





# C2 - Mounting arrangements













The various mounting arrangements for machines are defined in IEC 60034-7. Below is an extract from the standard which shows equivalent terms in current use.

Code I	Code II
IM B 3	IM 1001
IM V 5	IM 1011
IM V 6	IM 1031
IM B 6	IM 1051
IM B 7	IM 1061
IM B 8	IM 1071
IM B 20	IM 1101
IM B 15	IM 1201
IM B 35	IM 2001
IM V 15	IM 2011
IM V 36	IM 2031
IM B 34	IM 2101
IM B 5	IM 3001
IM V 1	IM 3011
IM V 21	IM 3051
IM V 3	IM 3031
IM V 4	IM 3211
IM V 2	IM 3231
IM B 14	IM 3601
IM V 18	IM 3611
IM V 19	IM 3631
IM B 10	IM 4001
IM V 10	IM 4011
IM V 14	IM 4031
IM V 16	IM 4131
IM B 9	IM 9101
IM V 8	IM 9111
IM V 9	IM 9131
IM B 30	IM 9201
IM V 30	IM 9211
IM V 31	IM 9231

Codes I and II are interchangeable. It should however be noted that the above code list is not exhaustive and you should therefore refer to IEC 60034-7 for other designations. On the next page you will find the most common mounting arrangements with line drawings and an explanation of the standard symbols used.

#### Mounting options according to frame size

Some operating positions are prohibited for standard motors. Select the possible configurations for machine installation from the table below.

In the case of difficulty, please consult Leroy-Somer.

Frame size						Mounting	positions					
	IM 1001	IM 1051	IM 1061	IM 1071	IM 1011*	IM 1031	IM 3001	IM 3011*	IM 3031	IM 2001	IM 2011*	IM 2031
80 to 200	•	•	•	•	•	•	•	•	•	•	•	•
225 and 250	•	•	•	•	•	•	О	•	٠	•	•	•
280 and 315	•	0	0	О	0	0	О	•	•	•	•	О
355 to 450	•	0	0	0	0	0		•	О	•	٠	0

• : possible positions

O : please consult Leroy-Somer specifying the coupling method and the axial and radial loads if applicable.

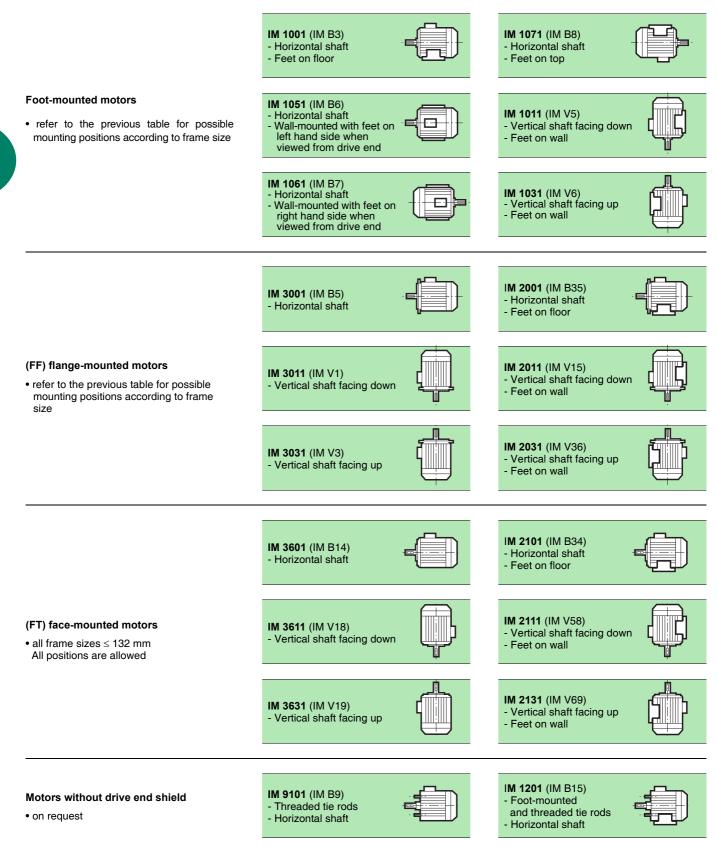
: positions not available

\* : the use of a drip cover is recommended for these mounting arrangements



# C2 - Mounting arrangements

Mountings and positions (IEC standard 60034-7)





## C3 - Bearings and lubrication

#### C3.1 - BEARINGS AND BEARING LIFE Definitions

#### Load ratings

#### - Basic static load C<sub>o</sub>:

This is the load for which permanent deformation at point of contact between a bearing race and the ball (or roller) with the heaviest load reaches 0.01% of the diameter of the ball (or roller).

#### - Basic dynamic load C:

This is the load (constant in intensity and direction) for which the nominal lifetime of the bearing will reach 1 million revolutions.

The static load rating  $C_{\circ}$  and dynamic load rating C are obtained for each bearing by following the method in ISO 281.

#### Lifetime

The lifetime of a bearing is the number of revolutions (or number of operating hours at a constant speed) that the bearing can accomplish before the first signs of fatigue (spalling) begin to appear on a ring, ball or roller.

#### - Nominal lifetime L10h

According to the ISO recommendations, the nominal lifetime is the length of time completed or exceeded by 90% of apparently identical bearings operating under the conditions specified by the manufacturer.

**Note:** The majority of bearings last much longer than the nominal lifetime; the average lifetime achieved or exceeded by 50% of bearings is around 5 times longer than the nominal lifetime.

#### Determination of nominal lifetime Constant load and speed of rotation

The nominal lifetime of a bearing expressed in operating hours  $L_{10h}$ , the basic dynamic load C expressed in daN and the applied loads (radial load  $F_r$  and axial load  $F_a$ ) are related by the following equation:

$$L_{10h} = \frac{1000000}{60 \cdot N} \cdot \left(\frac{C}{P}\right)$$

where N = speed of rotation (min-1)

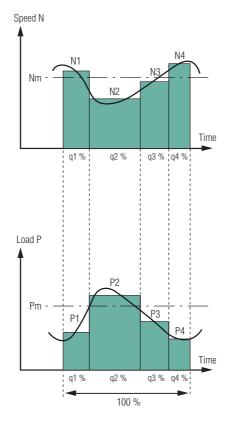
- P (P = X  $F_r$  + Y  $F_a$ ): dynamic load equivalent ( $F_r$ ,  $F_a$ , P in daN)
- p: an index which depends on the type of contact between the races and balls (or rollers)
  - p = 3 for ball bearings
  - p = 10/3 for roller bearings

The formulae that give Equivalent Dynamic Load (values of factors X and Y) for different types of bearing may be obtained from their respective manufacturers.

#### Variable load and speed of rotation

For bearings with periodically variable load and speed, the nominal lifetime is established using the equation:

$$\frac{L_{10h} = \frac{1000000}{60 \cdot N_{m}} \cdot \left(\frac{C}{P_{m}}\right)^{1}$$



Nm: average speed of rotation

$$N_m = N_1 \cdot \frac{q_1}{100} + N_2 \cdot \frac{q_2}{100} + \dots (min^{-1})$$

P<sub>m</sub>: average equivalent dynamic load

$$P_{m} = \sqrt{p} \sqrt{P_{1}^{1/p} \cdot \left(\frac{N_{1}}{N_{m}}\right) \cdot \frac{q_{1}}{100}} + P_{2}^{1/p} \cdot \left(\frac{N_{2}}{N_{m}}\right) \cdot \frac{q_{2}}{100}} + \dots (daN)$$

with  $q_1$ ,  $q_2$ , etc as a%

Nominal lifetime  $L_{10h}$  is applicable to bearings made of bearing steel and normal operating conditions (lubricating film present, no contamination, correctly fitted, etc).

Situations and data differing from these conditions will lead to either a reduction or an increase in lifetime compared to the nominal lifetime.

#### **Corrected nominal lifetime**

If the ISO recommendations (DIN ISO 281) are used, improvements to bearing steel, manufacturing processes and the effects of operating conditions may be integrated in the nominal lifetime calculation.

The theoretical pre-fatigue lifetime  $L_{\text{nah}}$  is thus calculated using the formula:

 $L_{nah} = a_1 a_2 a_3 L_{10h}$ 

with:

a1: failure probability factor

 $a_2$ : factor for the characteristics and tempering of the steel

 $a_3$ : factor for the operating conditions (lubricant quality, temperature, speed of rotation, etc)

Under normal operating conditions for FLS motors, the corrected nominal lifetime, calculated with a failure probability factor a1 = 1 ( $L_{10ah}$ ), is longer than the nominal lifetime  $L_{10h}$ .



# C3 - Bearings and lubrication

#### **C3.2 - TYPES OF BEARING AND STANDARD FITTING ARRANGEMENTS**

			Vertical shaft			
			Shaft facing down	Shaft facing up		
	Mounting arrangement	B3 / B6 / B7 / B8	V5	V6		
Foot-mounted motors	standard mounting	The DE bearing is: - located at DE for frame $\leq$ 132 - locked for 160 $\leq$ frame $\leq$ 315 S The NDE bearing is locked for frames 315 M to 450	The DE bearing is: - located at DE for frame $\leq$ 132 - locked for 160 $\leq$ frame $\leq$ 315 S The NDE bearing is locked for frames 315 M to 450	The DE bearing is: - located at DE for frame ≤ 90 - locked for 100 ≤ frame ≤ 315 S The NDE bearing is locked for frames 315 M to 450		
	on request	DE bearing locked for frames $\leq$ 132	DE bearing locked for frames $\leq$ 132	DE bearing locked for frames $\leq$ 90		
	Mounting arrangement	B5 / B35 / B14 / B34	V1 / V15 / V18 / V58	V3 / V36 / V19 / V69		
Foot-mounted motors (or foot and flange)	standard mounting	The DE bearing is locked for frames 80 to 315 S The NDE bearing is locked for frames 315 M to 450	The DE bearing is locked for frames 80 to 315 S The NDE bearing is locked for frames 315 M to 450	The DE bearing is locked for frames 80 to 315 S The NDE bearing is locked for frames 315 M to 450		

Important: When ordering, state correct mounting type and position (see section C1).

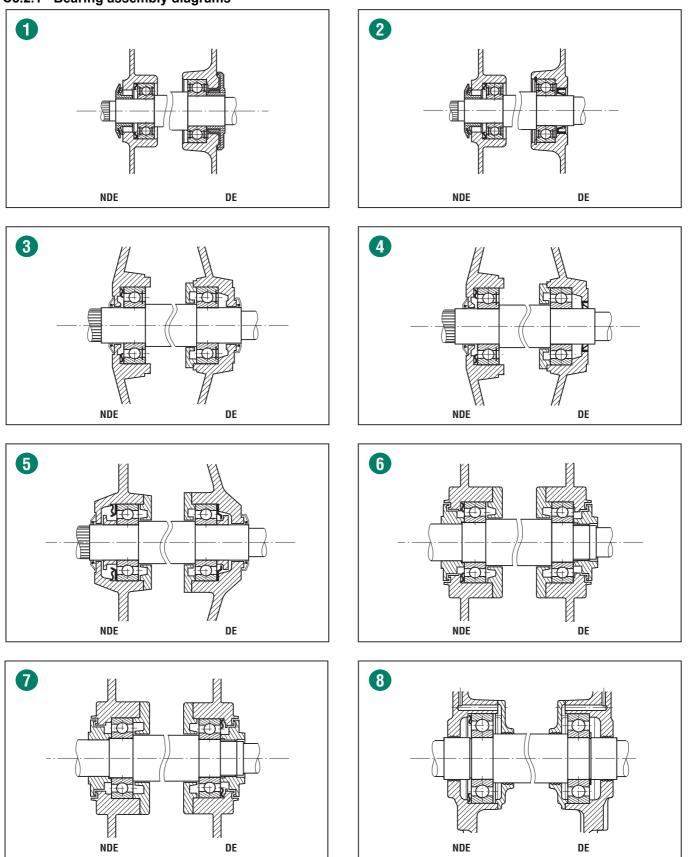
Motor			Standard fitting arrangement						
LEROY-SOMER			Non drive end		Assembly dia	agram reference			
Frame/Type	LEROY-SOMER designation	No. of poles	bearing (N.D.E.)	Drive end bearing (D.E.)	Foot-mounted motors	Flange-mounted (or foot and flange) motors			
80 L	FLS 80 L	2;4;6;8	6203 ZZ C3	6204 ZZ C3	0	2			
90 S	FLS 90 S	2;4;6;8	6204 ZZ C3	6205 ZZ C3	1	2			
90 L	FLS 90 L	2;4;6;8	6204 ZZ C3	6205 ZZ C3	0	2			
100 L	FLS 100 LK	2;4;6;8	6205 ZZ C3	6206 ZZ C3	1	2			
112 M	FLS 112 M	2;4;6;8	6205 ZZ C3	6206 ZZ C3	0	2			
132 S	FLS 132 S	2;4;6;8	6207 ZZ C3	6208 ZZ C3	1	2			
132 M	FLS 132 M	2;4;6;8	6207 ZZ C3	6308 ZZ C3	0	2			
160 M	FLS 160 M (A,B)	2;4;6;8	6210 Z C3	6309 Z C3	3	4			
160 L	FLS 160 L	2;4;6;8	6210 Z C3	6309 Z C3	3	4			
180 M	FLS 180 MR	2;4	6210 Z C3	6310 Z C3	3	4			
180 L	FLS 180 L	4;6;8	6212 Z C3	6310 Z C3	3	4			
200 L	FLS 200 L (A,B)	2;4;6;8	6313 C3	6313 C3	5	6			
225 S	FLS 225 ST	4;8	6313 C3	6313 C3	5	5			
225 M	FLS 225 MT	2	6313 C3	6313 C3	5	6			
225 M	FLS 225 M	4;6;8	6314 C3	6314 C3	8	8			
250 M	FLS 250 M	2;4;6;8	6314 C3	6314 C3	8	8			
280 S	FLS 280 S	2;4;6;8	6314 C3	6316 C3	8	8			
280 M	FLS 280 M	2;4;6;8	6314 C3	6316 C3	8	8			
315 S	FLS 315 ST	2	6317 C4	6317 C4	6	6			
315 S	FLS 315 ST	4;6;8	6318 C3	6318 C3	6	6			
315 M	FLS 315 M	2	6317 C4	6317 C4	0	0			
315 M	FLS 315 M	4;6;8	6320 C3	6320 C3	0	0			
315 L	FLS 315 L (A,B)	2	6317 C4	6317 C4	0	0			
315 L	FLS 315 L (A,B)	4;6;8	6320 C3	6320 C3	0	1			
355 L	FLS 355 L (A,B,C,D)	2	6317 C4	6317 C4	0	0			
355 L	FLS 355 L (A,B,C,D)	4;6;8	6322 C3	6322 C3	0	1			
355 LK	FLS 355 LK (A,B)	4;6;8	6324 C3	6324 C3	0	0			
400 L	FLS 400 LV (B)	4	6324 C3	6324 C3	0	7			
400 L	FLS 400 L (A,B)	4;6;8	6324 C3	6324 C3	0	0			
400 LK	FLS 400 LK (A,B)	4;6;8	6328 C3	6328 C3	0	0			
450 L	FLS 450 L (A,B)	4;6;8	6328 C3	6328 C3	0	0			
450 L	FLS 450 LV (A,B)	4	6328 C3	6328 C3	0	0			

Important: From the FLS 315 ST upwards, for 2-pole motors with a 60 Hz supply, specify the axial and radial loads during consultation.



# C3 - Bearings and lubrication

#### C3.2.1 - Bearing assembly diagrams





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C

C3 - Bearings and lubrication

C3.2.2 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

Horizontal motor

Nominal lifetime L<sub>10h</sub> of bearings: 25,000 hours

	Motor		oles DO min <sup>-1</sup>		oles 10 min <sup>-1</sup>		oles 10 min <sup>-1</sup>	8 p N = 75	oles O min <sup>-1</sup>
		>		>	<b>←</b>		<b>←</b>		
Frame size	Туре	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34
80	FLS 80	23	(61)*	37	(75)*	45	(83)*	55	(93)*
90	FLS 90 S/L	19	(69)*	35	(85)*	44	(94)*	55	(105)*
100	FLS 100 LK	32	(88)*	46	(102)*	63	(119)*	78	(134)*
112	FLS 112 M	32	(88)*	46	(102)*	63	(119)*	78	(134)*
132	FLS 132 S/M	86	(188)*	125	(227)*	159	(261)*	192	(294)*
160	FLS 160 M/MA/MB	163	195	224	256	272	304	299	331
160	FLS 160 L	154	186	210	242	253	285	282	314
180	FLS 180 MR	188	220	240	272	-	-	-	-
180	FLS 180 L	-	-	241	287	276	322	313	359
200	FLS 200 L/LA/LB	270	342	370	442	424	496	483	555
225	FLS 225 ST/MT	261	333	355	427	-	-	456	528
225	FLS 225 M	-	-	400	480	468	548	533	613
250	FLS 250 M	296	376	400	480	468	548	533	613
280	FLS 280 S	343	423	461	541	532	612	579	659
280	FLS 280 M	325	405	423	503	455	535	526	606
315	FLS 315 ST	492	332	461	621	546	706	570	730
315	FLS 315 M	486	326	746	546	905	705	963	763
315	FLS 315 LA	504	344	728	528	886	686	938	738
315	FLS 315 LB	487	327	733	533	847	647	890	690
355	FLS 355 LA	453	293	788	587	934	694	1006	766
355	FLS 355 LB	448	288	771	531	892	652	945	705
355	FLS 355 LC	443	285	751	512	-	-	-	-
355	FLS 355 LD	440	280	736	496	805	565	871	631
355	FLS 355 LKA	-	-	-	-	-	-	1038	758
355	FLS 355 LKB	-	-	862	582	923	643	1018	738
400	FLS 400 LA	-	-	873	593	941	661	1038	758
400	FLS 400 LB/LVB	-	-	862	582	923	643	1018	738
400	FLS 400 LKA	-	-	-	-	-	-	1264	910
400	FLS 400 LKB	-	-	-	-	1162	941	1237	883
450	FLS 450 LA/LVA	-	-	1061	707	1179	808	1264	910
450	FLS 450 LB/LVB	-	-	1041	687	1162	941	1237	883

()\* The axial loads shown above for IM B3 / B6 / B7 / B8 with frame size ≤ 132 are the permissible axial loads for locked DE bearings (non-standard assembly, special order).



C3 - Bearings and lubrication

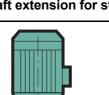
C3.2.2 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

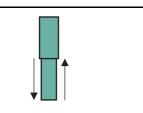
Vertical motor Shaft facing down

Nominal lifetime L<sub>10h</sub> of bearings: 25,000 hours

	Motor		oles DO min <sup>-1</sup>		oles DO min <sup>-1</sup>		oles 00 min <sup>-1</sup>	8 pc N = 75	oles O min <sup>-1</sup>
Frame size	Туре								1
		IM V5 IM V1 / V15 IM V18 / V58	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69	IM V5 IM V1 / V15 IM V18 / V69
80	FLS 80 L	22	(63)*	35	(79)*	42	(89)*	52	(99)*
90	FLS 90 S/L	17	(73)*	31	(91)*	41	(100)*	52	(111)*
100	FLS 100 LK	29	(93)*	41	(111)*	57	(129)*	72	(144)*
112	FLS 112 M	29	(93)*	41	(111)*	57	(129)*	72	(144)*
132	FLS 132 S/M	73	(207)*	110	(251)*	140	(291)*	176	(321)*
160	FLS 160 M/MA/MB	145	223	204	287	249	339	278	369
160	FLS 160 L	134	220	187	281	226	332	259	359
180	FLS 180 MR	164	257	214	320	-	-	-	-
180	FLS 180 L	-	-	208	342	240	384	276	426
200	FLS 200 L/LA/LB	230	402	324	517	374	581	432	646
225	FLS 225 ST/MT	218	402	303	515	-	-	401	634
225	FLS 225 M	-	-	324	600	382	689	449	753
250	FLS 250 M	238	465	324	600	382	689	449	753
280	FLS 280 S	265	545	362	699	491	790	463	869
280	FLS 280 M	281	507	307	701	347	761	389	869
315	FLS 315 ST	380	509	457	737	554	814	551	903
315	FLS 315 M	361	545	582	861	764	976	800	1084
315	FLS 315 LA	344	572	546	876	726	988	756	1091
315	FLS 315 LB	306	596	514	909	644	1018	681	1098
355	FLS 355 LA	244	648	512	1050	684	1175	721	1341
355	FLS 355 LB	222	667	475	1067	605	1199	618	1367
355	FLS 355 LC	195	692	425	1081	-	-	-	-
355	FLS 355 LD	175	707	391	1107	432	1259	494	1397
355	FLS 355 LKA	-	-	-	-	-		700	1510
355	FLS 355 LKB	-	-	612	1106	571	1372	624	1563
400	FLS 400 LA	-	-	672	1058	649	1315	700	1510
400	FLS 400 LB/LVB	-	-	612	1106	571	1372	624	1563
400	FLS 400 LKA	-		-		-		767	1953
400	FLS 400 LKB	-	-	-	-	671	1772	605	2088
450	FLS 450 LA/LVA	-	-	868	1247	791	1668	767	1953
450	FLS 450 LB/LVB	-	-	729	1366	671	1772	605	2088

()\* The axial loads shown above for IM V5 with frame size  $\leq$  132 are the permissible axial loads for locked DE bearings (non-standard assembly, special order).





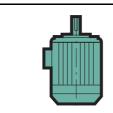


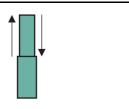
C3 - Bearings and lubrication

C3.2.2 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

Vertical motor Shaft facing up

Nominal lifetime L<sub>10h</sub> of bearings: 25,000 hours





	Motor	2 pc N = 300		4 pc N = 150		6 pc N = 100			oles O min <sup>-1</sup>
Frame size	Туре	$\downarrow$	1	$\downarrow$	1	$\downarrow$	1	$\downarrow$	1
3126	<i>"</i> "	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69
80	FLS 80 L	(60)*	25	(73)*	41	(80)*	51	(90)*	51
90	FLS 90 S/L	(67)*	23	(81)*	41	(91)*	50	(102)*	61
100	FLS 100 LK	85	37	97	55	113	73	128	88
112	FLS 112 M	85	37	97	55	113	73	128	88
132	FLS 132 S/M	175	105	212	149	242	189	278	219
160	FLS 160 M/MA/MB	177	191	236	255	281	307	310	337
160	FLS 160 L	166	188	219	249	258	300	291	327
180	FLS 180 MR	196	225	246	288	-	-	-	-
180	FLS 180 L	-	•	254	296	286	338	322	380
200	FLS 200 L/LA/LB	302	330	396	445	446	509	504	574
225	FLS 225 ST/MT	290	330	375	443	-	-	493	562
225	FLS 225 M	-	-	404	520	462	609	529	673
250	FLS 250 M	318	385	404	520	462	609	529	673
280	FLS 280 S	345	465	442	619	511	710	543	789
280	FLS 280 M	321	467	387	621	427	681	469	789
315	FLS 315 ST	380	509	457	737	554	814	551	903
315	FLS 315 M	361	545	582	861	764	976	800	1084
315	FLS 315 LA	344	572	546	876	726	988	756	1091
315	FLS 315 LB	306	596	514	909	644	1018	681	1098
355 to 4	50: consult Leroy-Somer befo	ore ordering							

()\* The axial loads shown above for IM V6 with frame size ≤ 90 are the permissible axial loads for locked DE bearings (non-standard assembly, special order).



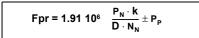
# C3 - Bearings and lubrication

# C3.2.3 - Permissible radial load on main shaft extension

In pulley and belt couplings, the drive shaft carrying the pulley is subjected to a radial force Fpr applied at a distance X (mm) from the shoulder of the shaft extension (length E).

## Radial force applied to drive shaft extension: Fpr

The radial force Fpr expressed in daN applied to the shaft extension is found by the formula.



where:

 $P_N$  = rated motor power (kW)

D = external diameter of the drive pulley (mm)

 $N_{\rm N}$  = rated speed of the motor (min<sup>-1</sup>)

k = factor depending on the type of transmission

 $P_P$  = weight of the pulley (daN)

The weight of the pulley is positive when it acts in the same direction as the tension force in the belt (and negative when it acts in the opposite direction).

Range of values for factor k(\*)

- toothed belts ..... k = 1 to 1.5
- V-belts ..... k = 2 to 2.5 - flat belts
- with tensioner ..... k = 2.5 to 3
- without tensioner ..... k = 3 to 4

(\*) A more accurate figure for factor k can be obtained from the transmission suppliers.

### • Permission radial force on the drive shaft extension

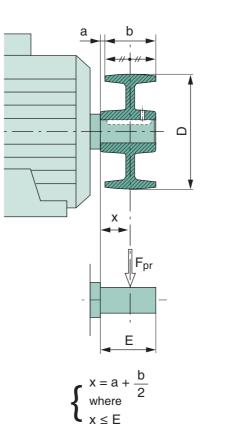
The charts on the following pages indicate, for each type of motor, the radial force FR at a distance X permissible on the drive end shaft extension, for a bearing life  $L_{10h}$  of 25,000 hours.

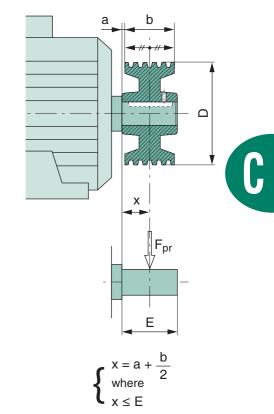
Note: For frame sizes  $\geq$  315 M, the selection charts are applicable for a motor installed with the shaft horizontal.

### • Change in bearing life depending on the radial load factor

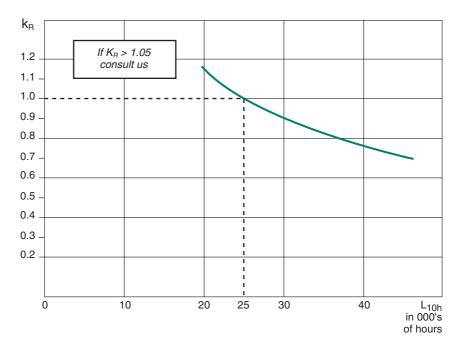
For a radial load Fpr (Fpr  $\neq$   $F_{\text{R}})$ , applied at distance X, the bearing life  $L_{10\text{h}}$  changes, at a first approximation, in the ratio  $k_{\text{R}}$ ,  $(k_{\text{R}}$  = Fpr /  $F_{\text{R}})$  as shown in the chart opposite, for standard assemblies.

If the load factor  $k_{\rm R}$  is greater than 1.05, you should consult our technical department, stating mounting position and direction of force before opting for a special fitting arrangement.





Change in bearing life L<sub>10h</sub> depending on the radial load factor k<sub>R</sub> for standard fitting arrangements.

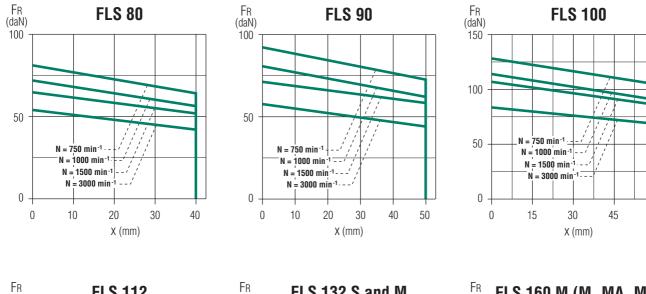


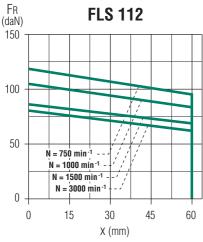


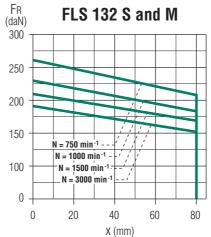
# C3 - Bearings and lubrication

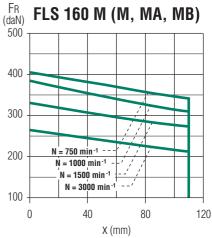
#### C3.2.4 - Standard fitting arrangement

Permissible radial load on main shaft extension with a bearing life  $L_{10h}$  of 25,000 hours.

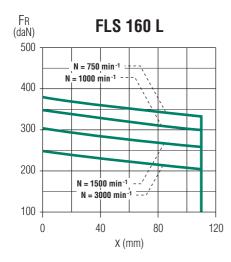


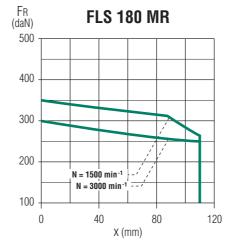


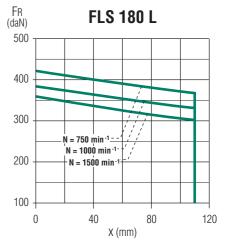




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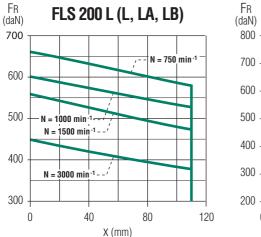


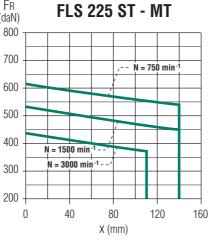


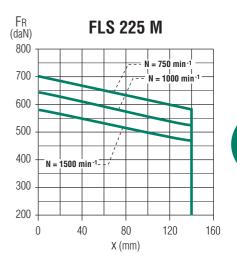
# C3 - Bearings and lubrication

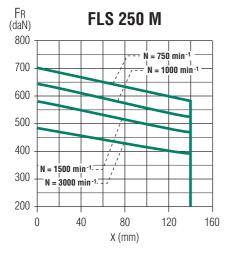
#### C3.2.4 - Standard fitting arrangement

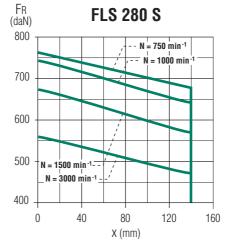
Permissible radial load on main shaft extension with a bearing life  $L_{10h}$  of 25,000 hours.

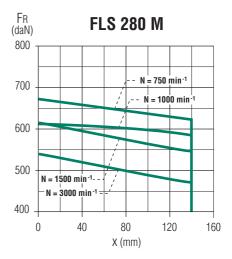


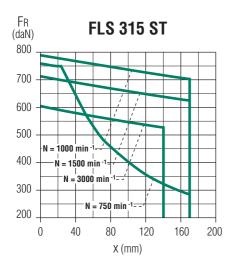


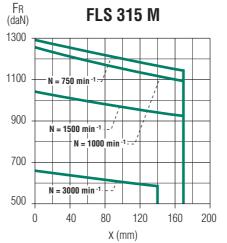




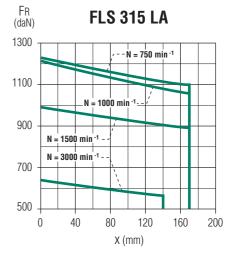








LEROY\*

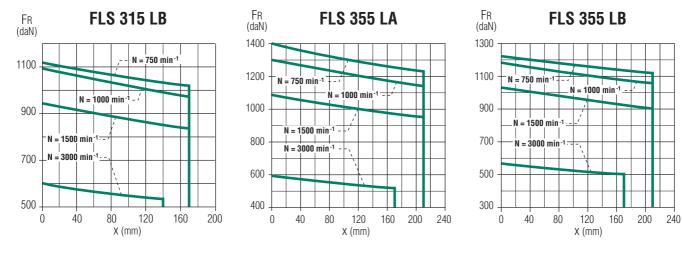


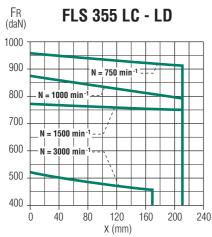


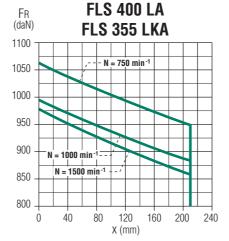
# C3 - Bearings and lubrication

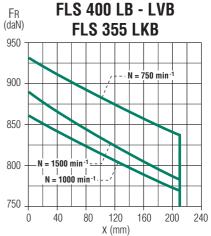
#### C3.2.4 - Standard fitting arrangement

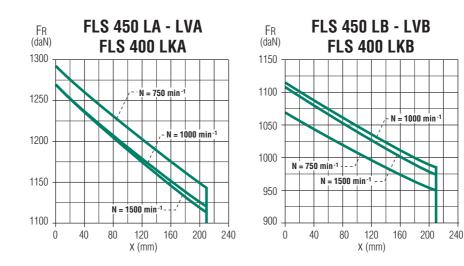
Permissible radial load on main shaft extension with a bearing life  $L_{10h}$  of 25,000 hours.













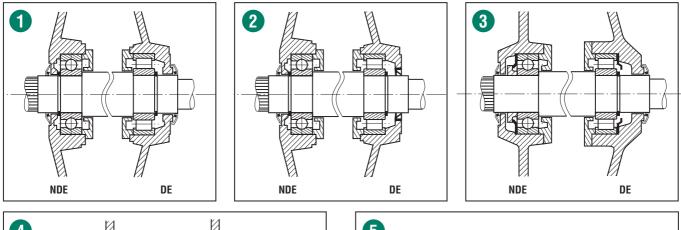
# C3 - Bearings and lubrication

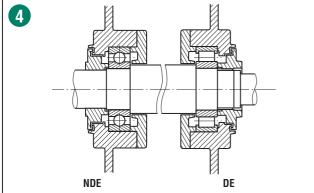
### C3.3 - TYPES AND SPECIAL FITTING ARRANGEMENTS FOR DE ROLLER BEARINGS

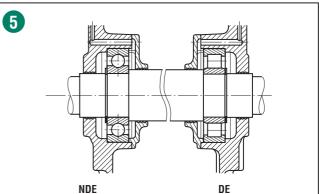
М	lotor		Standard fitting arrangement				
		No. of poles	Non drive end		Assembly diagram reference		
Frame size	LEROY-SOMER designation	·	bearing (N.D.E.)	Drive end bearing (D.E.)	Foot-mounted motors	Flange-mounted (or foot and flange) motors	
160 M	FLS 160 M/MA/MB	4;6;8	6210 Z C3	NU 309	0	2	
160 L	FLS 160 L	4;6;8	6210 Z C3	NU 309	1	2	
180 M	FLS 180 MR	4	6210 Z C3	NU 310	1	2	
180 L	FLS 180 L	4;6;8	6212 Z C3	NU 310	1	2	
200 L	FLS 200 L/LA/LB	4;6;8	6313 C3	NU 313	3	3	
225 S	FLS 225 ST	4;8	6313 C3	NU 313	3	3	
225 M	FLS 225 M	4;6;8	6314 C3	NU 314	5	5	
250 M	FLS 250 M	4;6;8	6314 C3	NU 314	5	5	
280 S	FLS 280 S	4;6;8	6314 C3	NU 316	5	5	
280 M	FLS 280 M	4;6;8	6314 C3	NU 316	5	5	
315 S	FLS 315 ST	4;6;8	6318 C3	NU 318	4	4	
315 M	FLS 315 M	4;6;8	6320 C3	NU 320	4	4	
315 L	FLS 315 L	4;6;8	6320 C3	NU 320	4	4	
355 L*	FLS 355 LA/LB/LC/LD	4;6;8	6322 C3	NU 322	4	4	
355 L*	FLS 355 LKA/LKB	4;6;8	6324 C3	NU 324	4	4	
400 L*	FLS 400 LA/LB	4;6;8	6324 C3	NU 324	4	4	
400 L*	FLS 400 LKA/LKB	4;6;8	6328 C3	NU 328	4	4	
450 L*	FLS 450 LA/LB/LVA/LVB	4;6;8	6328 C3	NU 328	4	4	

\* in the vertical position, the axial and radial force values must be specified.

### C3.3.1 - Bearing assembly diagrams







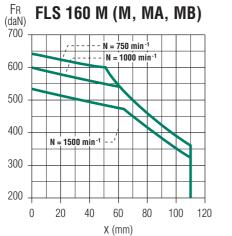


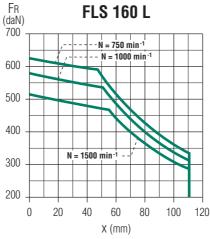
39

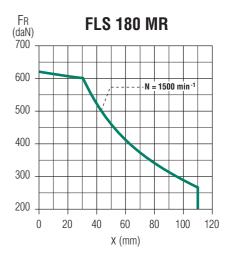
# C3 - Bearings and lubrication

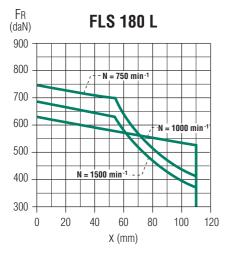
#### C3.3.2 - Special fitting arrangements

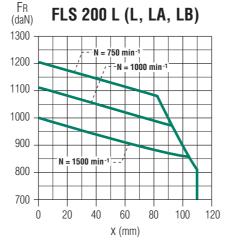
Permissible radial load on main shaft extension with a bearing life  $L_{10h}$  of 25,000 hours.

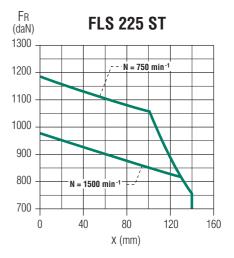


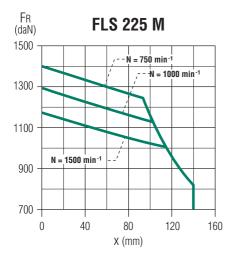


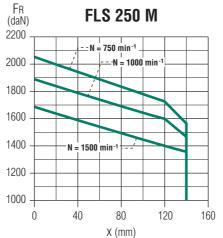


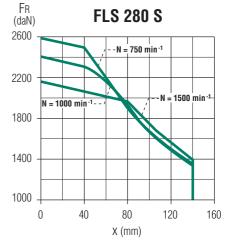












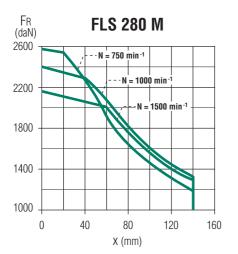


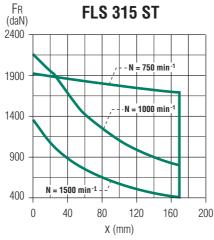
# C3 - Bearings and lubrication

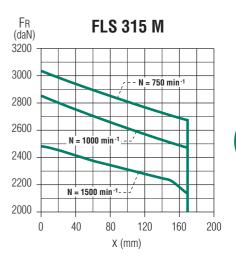
**FLS 315 ST** 

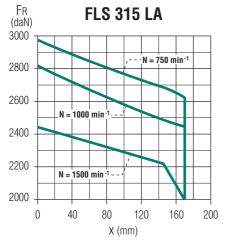
#### C3.3.2 - Special fitting arrangements

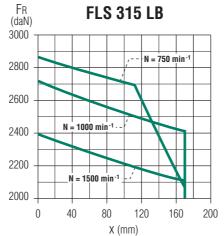
Permissible radial load on main shaft extension with a bearing life L<sub>10b</sub> of 25,000 hours.

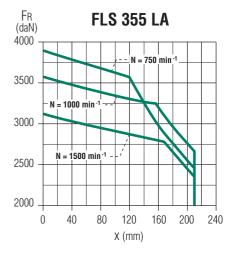


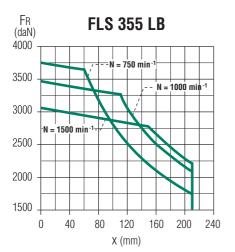


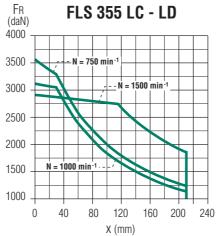


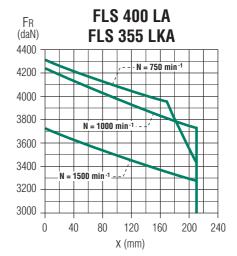










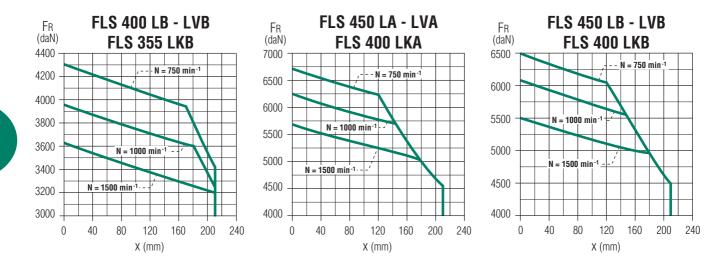




# C3 - Bearings and lubrication

#### C3.3.2 - Special fitting arrangements

Permissible radial load on main shaft extension with a bearing life  $L_{10h}$  of 25,000 hours.





## C3 - Bearings and lubrication

#### C3.4 - LUBRICATION AND MAINTENANCE OF BEARINGS Role of the lubricant

The principal role of the lubricant is to avoid direct contact between the metal parts in motion: balls or rollers, slip-rings, cages, etc. It also protects the bearing against wear and corrosion.

The quantity of lubricant needed by a bearing is normally quite small. There should be enough to provide good lubrication without undesirable overheating. As well as lubrication itself and the operating temperature, the amount of lubricant should be judged by considerations such as sealing and heat dissipation.

The lubricating power of a grease or an oil lessens with time owing to mechanical constraints and straightforward ageing. Used or contaminated lubricants should therefore be replaced or topped up with new lubricant at regular intervals.

Bearings can be lubricated with grease, oil or, in certain cases, with a solid lubricant.

#### C3.4.1 - Lubrication with grease

A lubricating grease can be defined as a product of semi-fluid consistency obtained by the dispersion of a thickening agent in a lubricating fluid and which may contain several additives to give it particular properties.

Composition of a grease
Base oil: 85 to 97%
Thickener: 3 to 15%
Additives: 0 to 12%

#### The base oil lubricates

The oil making up the grease **is of prime importance**. It is the oil that lubricates the moving parts by coating them with a protective film which prevents direct contact. The thickness of the lubricating film is directly linked to the viscosity of the oil, and the viscosity itself depends on temperature. The two main types used to make grease are mineral oils and synthetic oils. Mineral oils are suitable for normal applications in a range of temperatures from -30° to +150°C. Synthetic oils have the advantage of being effective in severe conditions (extreme variations of temperature, harsh chemical environments, etc).

# The thickener gives the grease consistency

The more thickener a grease contains, the 'harder' it will be. Grease consistency varies with the temperature. In falling temperatures, the grease hardens progressively, and the opposite happens when temperatures rise. The consistency of a grease can be quantified using the NLGI (National Lubricating Grease Institute) classification. There are 9 NLGI grades, from 000 for the softest greases up to 6 for the hardest. Consistency is expressed by the depth to which a cone may be driven into a grease maintained at 25°C.

If we only consider the chemical nature of the thickener, lubricating greases fall into three major categories:

• conventional greases with a metallic soap base (calcium, sodium, aluminium, lithium). Lithium soaps have several advantages over other metallic soaps: a high melting point (180° to 200°), good mechanical stability and good water resistant properties.

• greases with a complex soap base The main advantage of this type of soap is a very high melting point (over 250°C).

• soapless greases. The thickener is an inorganic compound, such as clay. Their main property is the absence of a melting point, which makes them practically non-liquefying.

# Additives improve some properties of greases

Additives fall into two types, depending on whether or not they are soluble in the base oil.

The most common insoluble additives graphite, molybdenum disulphide, talc, mica, etc, improve the friction characteristics between metal surfaces. They are therefore used in applications where heavy pressure occurs.

The soluble additives are the same as those used in lubricating oils: antioxidants, antirust agents, etc.

#### C3.4.2 - Grease life

The lifetime of a lubricating grease depends on:

- the characteristics of the grease (type of soap and base oil, etc)

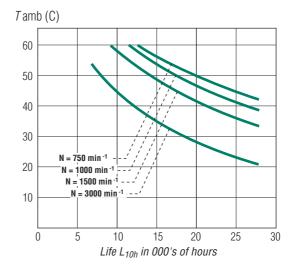
- service stress (type and size of bearing, speed of rotation, operating temperature, etc)

- contamination

# C3.4.2.1 - Permanently greased bearings

For motors from 80 frame to 132 frame, the type and size of the bearings make for long grease life and therefore lubrication for the lifetime of the machine. The grease life  $L_{10h}$  according to speed of rotation and ambient temperature is shown on the chart opposite.

#### • Grease life $L_{10h}$ in 000's of hours, for frames sizes $\leq$ 132.





# C3 - Bearings and lubrication

# C3.4.2.2 - Bearings with grease nipples

The chart opposite shows the regreasing intervals, depending on the type of motor, for standard bearing assemblies of frame size  $\geq 160$  fitted with grease nipples, operating at an ambient temperature of 40°C on a horizontal shaft machine.

**Note:** the quality and quantity of grease and the regreasing interval are shown on the machine nameplate.

The chart opposite is valid for FLS motors lubricated with ESSO UNIREX N3 grease, which is used as standard, as well as KLUBER BQ72672 grease for 2-pole versions only of the 315 ST/ M/L and 355 L.

#### C3.4.2.3 - Special assembly

For special assemblies (motors fitted with DE roller bearings or other types), machines of frame size  $\geq$  160 have bearings with grease nipples. Instructions for bearing maintenance are given on the nameplates on these machines.

		3600*	3000	1800	1500	1200	1000	900	750	Qty. of grease cm <sup>3</sup>
160 M/L	DE	4 000	5 200	10 000	12 000	16 000	19 000	21 500	26 000	13
	NDE	3 500	4 600	9 000	11 000	15 000	18 000	20 000	24 000	10
180 MR	DE	3 500	4 600	9 000	11 000					15
	NDE	3 500	4 600	9 000	11 000					10
180 L	DE			9 000	11 000	15 000	18 000	20 000	24 000	15
	NDE			7 700	9 700	13 000	16 000	18 000	22 000	12
200 L		2 200	3 200	7 000	9 000	12 000	15 000	17 000	21 000	23
225 ST				7 000	9 000			17 000	21 000	23
225 MT		2 200	3 200							23
225 M				6 500	8 300	11 000	14 000	16 000	20 000	26
250 M		1 800	2 800	6 500	8 300	11 000	14 000	16 000	20 000	26
280	DE	1 200	2 000	5 500	7 200	10 000	12 500	14 000	18 000	33
	NDE	1 800	2 800	6 500	8 300	11 000	14 000	16 000	20 000	26
315 ST 2P		800	1 700							37
315 ST 4P 8	k +			4 600	6 200	8 600	11 000	13 000	16 000	40
315 M/L 2P		800	1 700							37
315 M/L 4P	& +			3 800	5 400	7 600	10 000	11 500	14 500	50
355 L 2P		800	1 700							37
355 L 4P &	+			3 000	4 500	6 600	9 000	10 500	13 500	60
355 LK/400	L			2 300	3 700	6 000	8 000	10 000	12 000	72
400 LK/450	L			1 000	2 300	4 000	6 000	8 000	10 000	93

 Regreasing intervals according to frame size and speed of rotation (for standard bearing assemblies).

(standard values: for maintenance purposes, refer to the values on the machine nameplates).

**Important:** From the FLS 315 ST upwards, for 2-pole motors with a 60 Hz supply, specify the axial and radial loads during consultation.

\* see chapter D2.2.3 / page 60



#### **3-phase TEFV induction motors FLS** cast iron Construction FLS motors are of standard C4 - Cooling configuration IC 411 New designation for the IC (International IC 4 A 1 Α 1 Cooling) coded cooling method in the IEC Circulation mode for secondary fluid (1: self-circulating) 60034-6 standard. Secondary fluid (A : air)

Coolant

The standard allows for two designations (general formula and simplified formula) as shown in the example opposite.

 Circulation method for primary fluid (1: self-circulating) Primary fluid (A: air)

Circuit layout (4: machine surface-cooled)

Note: the letter A may be omitted if this will not lead to confusion. This contracted formula becomes the simplified formula. Simplified form: IC 411.

#### **Circuit layout**

Characteris- tic number	Designation	Description
<b>O</b> (1)	Free circulation	The coolant enters and leaves the machine <i>freely</i> . It is taken from and returned to the fluid round the machine.
<b>1</b> (1)	Machine with an intake pipe	The coolant is taken up elsewhere than from the fluid round the machine, brought into the machine through an <i>intake pipe</i> and emptied into the fluid round the machine.
<b>2</b> (1)	Machine with an outlet pipe	The coolant is taken up from the fluid round the machine, brought away from the machine by an <i>outlet pipe</i> and does not go back into the fluid round the machine.
<b>3</b> (1)	Machine with two pipes (intake and outlet)	The coolant is taken up elsewhere than from the fluid round the machine, brought to the machine through an <i>intake pipe</i> , then taken away from the machine through an <i>outlet pipe</i> and does not go back into the fluid round the machine.
4	Surface cooled machine using the fluid round the machine	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (the one surrounding the machine) through the machine casing. The casing surface is either smooth or finned to improve heat transmission.
5(2)	Built-in heat exchanger (using the surrounding environment)	The primary coolant circulates in a <i>closed</i> circuit, transferring its heat to a secondary coolant (the one surrounding the machine) in an integral heat exchanger inside the machine.
6(2)	Machine-mounted heat exchanger (using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (the one surrounding the machine) in a heat exchanger that forms an independent unit, mounted on the machine.
<b>7</b> (2)	Built-in heat exchanger (not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (which is not the one round the machine) in an integral heat exchanger inside the machine.
<b>8</b> (2)	Machine-mounted heat exchanger (not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (which is not the one round the machine) in a heat exchanger that forms an independent unit, mounted on the machine.
<b>9</b> (2)(3)	Separate heat exchanger (using/not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to the secondary fluid in a heat exchanger that forms an independent unit, away from the machine.

#### **Characteris-**Type of fluid tic letter Α Air F Freon Н Hydrogen Ν Nitrogen С Carbon dioxide W Water U Oil S Any other fluid (must be identified separately) Y The fluid has not yet been selected (used temporarily)

#### Method of circulation

Characteris- tic number	Designation	Description
0	Free circulation	The circulation of the coolant is due only to differences in temperature. Ventilation caused by the rotor is negligible.
1	Self-circulating	The circulation of the coolant depends on the rotational speed of the main machine, and is caused by the action of the rotor alone, or a device mounted directly on it.
2, 3, 4		Not yet defined.
<b>5</b> (4)	Built-in, independent device	The coolant is circulated by a built-in device which is powered independently of the rotational speed of the main machine.
<b>6</b> (4)	Independent device mounted on the machine	The coolant is circulated by a device mounted on the machine which is powered independently of the rotational speed of the main machine.
<b>7</b> (4)	Entirely separate independent device or using the pressure of the coolant circulation system	The coolant is circulated by a separate electrical or mechanical device, independent and not mounted on the machine, or by the pressure in the coolant circulation system.
<b>8</b> (4)	Relative displacement	The circulation of the coolant is produced by the relative movement between the machine and the coolant, either by displacement of the machine in relation to the coolant, or by the flow of the surrounding coolant.
9	Any other device	The coolant is circulated using a method other than those defined above: it must be described in full.

(1) Filters or labyrinths for dust removal or noise protection can be fitted inside the casing or in the ducting. The first designation numbers 0 to 3 also apply to machines in which the coolant is taken up at the outlet of a watercooler designed to lower the temperature of the ambient air or recirculated through a watercooler so as not to increase the ambient temperature.

(2) The nature of the heat exchanger elements is not specified (smooth or finned tubes, corrugated surfaces, etc).

(3) A separate heat exchanger can be installed near to or at a distance from the machine. A secondary gas coolant may or may not be the surrounding medium.

(4) Use of such a device does not exclude the ventilating action of the rotor or the existence of an additional fan mounted directly on the rotor.



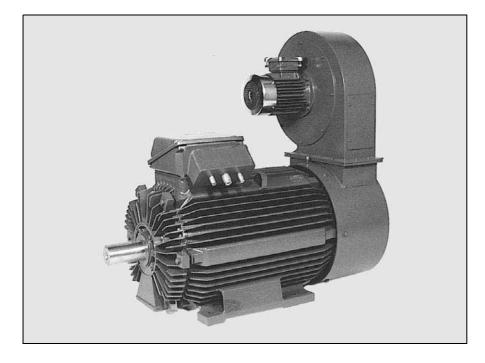
# C4 - Cooling

### C4.1 - STANDARD CODES

C

IC 410	Enclosed machine, surface-cooled by natural convection and radiation. No external fan.	
IC 411	Enclosed machine. Smooth or finned ventilated casing. External shaft-mounted fan.	
IC 416 A*	Enclosed machine. Smooth or finned enclosed casing. External motorized axial (A) fan supplied with the machine.	
IC 416 R*	Enclosed machine. Smooth or finned enclosed casing. External motorized radial (R) fan supplied with the machine.	
IC 418	Enclosed machine. Smooth or finned casing. No external fan. Ventilation provided by air flow coming from the driven system.	

\* Features not within manufacturer's standard range.



# Application of cooling systems to the LEROY-SOMER range

Frame size	IC 410	IC 411	IC 416 A	IC 416 R
80	О	•		
90 to 450	О	•	О	О

: standard construction

**O** : possible (ask for estimate)

□ : not possible

Another cooling system may be fitted as an option: complete immersion of the motor in oil (ask for estimate).



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# C4 - Cooling

### **C4.2 - VENTILATION**

#### C4.2.1 - Motor ventilation

In compliance with IEC 60034-6, the motors in this catalogue are cooled using method IC 411, ie. "surface-cooled machine using the ambient air circulating round the machine".

Cooling is achieved by a fan mounted at the NDE of the motor, inside a fan cover which acts as a safety guard. The fan draws the air through the grille in the cover and sends it along the housing fins, giving an identical heat balance in either direction of rotation.

#### Note: Obstruction - even accidental - of the fan cover grille (grille clogged or placed against a wall) has an adverse effect on the motor cooling process.

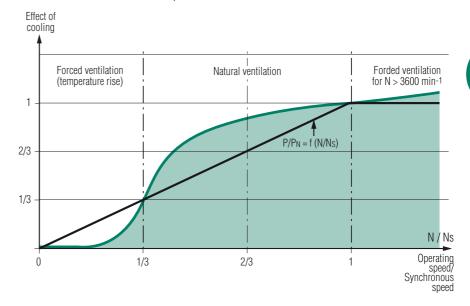
We recommend a minimum distance of 1/3 of the frame size between the end of the cover and any possible obstacle (wall, machine, etc).

#### Cooling of variable speed motors

Special precautions need to be taken when standard induction motors are being used with variable speed, powered by an inverter or voltage controller.

In prolonged operation at low speed, cooling efficiency is lost. It is therefore advisable to install forced ventilation that will produce a constant flow independent of the motor speed.

In prolonged operation at high speed, the fan may make excessive noise. It is again advisable to install a forced ventilation system.



#### C4.2.2 - Non-ventilated applications in continuous operation

Motors can be supplied without fans. Dimensions will depend on the application.

#### a) IC 418 cooling system

If they are placed in the air flow from a fan, these motors are capable of achieving their power rating if the speed of the air between the housing fins and the overall flow rate of the air between the fins comply with the data in the table opposite.

	2 p	oles	4 p	oles	6 poles and above	
Frame size	flow rate m <sup>3</sup> /h	speed m/s	flow rate m <sup>3</sup> /h	speed m/s	flow rate m <sup>3</sup> /h	speed m/s
80	120	7.5	60	4	40	2.5
90	200	11.5	75	5.5	60	3.5
100	300	15	130	7.5	95	5
112	460	18	200	9	140	6
132	570	21	300	10.5	220	7
160	1000	21	600	12.5	420	9
180	1200	21	900	16	600	10
200	1800	23	1200	16	750	10
225	2000	24	1500	18	1700	13
250	3000	25	2600	20	1700	13
280	3000	25	2600	20	2000	15
315	5000	25	2600	20	2000	15
355	5200	25	2800	20	2200	15
400	5500	25	3000	20	2400	15
450	6000	25	3200	20	2600	15

These air flows are valid for normal working conditions as described in section B2.1.



# C4 - Cooling

#### a) IC 410 cooling system

Used for general applications without cooling, these motors will provide the output powers given in the table below (if this is the case, their internal design is suited to the power provided, for an ambient temperature of  $40^{\circ}$ C and a temperature rise corresponding to insulation class F).

#### Non-ventilated three-phase induction motors - 50 Hz - IC 410 (temperature rise class F)

Power kW	No. of poles 2 poles	No. of poles 4 poles	No. of poles 6 poles	No. of poles 8 poles
0.18	-	-	FLS 80 L	FLS 90 L
0.25	- -	FLS 80 L	FLS 80 L	FLS 90 L
0.37	FLS 80 L	FLS 80 L	FLS 90 L	FLS 100 LK
0.55	FLS 80 L	FLS 90 S	FLS 90 L	FLS 100 LK
0.75	FLS 80 L	FLS 90 L	FLS 100 LK	FLS 112 M
0.9	FLS 90 L	FLS 90 L	-	-
1.1	FLS 90 L	FLS 100 LK	FLS 112 M	FLS 132 S
1.5	FLS 100 LK	FLS 112 M	FLS 112 M	FLS 132 M
1.85	FLS 112 M	FLS 112 M	FLS 132 M	FLS 160 MB
2.2	FLS 112 M	FLS 112 M	FLS 132 M	FLS 160 L
3	FLS 132 S	FLS 132 M	FLS 160 L	FLS 180 L
3.7	-	-	FLS 160 L	FLS 180 L
4	FLS 132 M	FLS 132 M	FLS 180 L	FLS 200 L
5.5	FLS 160 L	FLS 180 MR	FLS 200 LA	FLS 225 ST
7.5	FLS 180 MR	FLS 180 L	FLS 225 M	FLS 225 M
11	FLS 200 L	FLS 200 L	FLS 250 L	FLS 280 S
15	FLS 225 MT	FLS 225 M	FLS 280 S	FLS 280 M
18.5	FLS 250 M	FLS 250 M	FLS 280 M	FLS 315 ST
22	FLS 280 S	FLS 280 S	FLS 315 ST	FLS 315 M
30	FLS 280 M	FLS 280 M	FLS 315 M	FLS 315 LA
37	FLS 315 ST	FLS 315 ST	FLS 315 LA	FLS 315 LB
45	FLS 315 M	FLS 315 M	FLS 315 LB	FLS 355 LA
55	FLS 315 LA	FLS 315 LA	FLS 355 LA	FLS 355 LB
75	FLS 355 LA	FLS 355 LA	FLS 355 LB	FLS 400 LA
90	FLS 355 LB	FLS 355 LB	FLS 355 LD	FLS 400 LB
110	FLS 355 LD	FLS 355 LD	FLS 400 LA	FLS 450 LA
132	FLS 355 LD	FLS 355 LD	FLS 400 LB	FLS 450 LB
160	-	FLS 400 LB	FLS 450 LB	-
200	-	FLS 450 LB	-	-

Dimensions: see pages 99 to 105

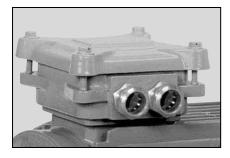


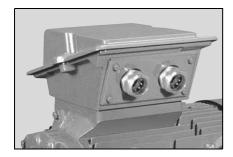
# C5 - Mains connection

#### C5.1 - TERMINAL BOX

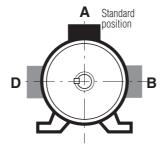
Placed as standard on the top of the motor near the drive end, the terminal box has IP 55 protection and is fitted with a cable gland (see table in C5.2).

The standard position of the cable gland is on the right, seen from the drive end but, owing to the symmetrical construction of the box, it can usually be placed in any of the 4 directions (see table opposite).

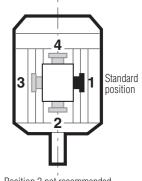




 Positions of the terminal box in relation to the drive end (motor in IM 1001 position)



 Positions of the cable gland in relation to the drive end



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Position 2 not recommended (not possible on standard FF flange-mounted motor)

Terminal	box position	А	В	D
FLS	80 to 132	•	-	-
FLS 160 to 225 MT		•	-	-
FLS 2	25 M to 450	•	•*	•*
• : standard	<ul> <li>: fixed-price op</li> </ul>	otion O: to estin	nate only - : no	t available

N.B. : The FLS 355 LK, 400 and 450 are fitted with an auxiliary terminal box on the non drive end, which must remain in the axis of the main terminal box.

\* except the FLS 315 ST

Cable gland position	1	2	3	4
Foot-mounted motor				
FLS 80 to 355 L	•	•	•	•
FLS 355 LK to 450	•	-	•	-
FT face-mounted motor				
FLS 80 to 132	٠	О	•	•
FF flange-mounted motor				
FLS 80 to 355 L	•	О	•	•
FLS 355 LK to 450	•	-	•	-

• : standard • : possible by simply removing the terminal box

**O** : ask for estimate - : not available

#### C5.1.1 - Flying leads

According to specification, motors can be supplied with flying leads or multicore cables. Please state cable characteristics (type and supplier, cross-section, length, number of conductors), connection method (on stator coil end turns, or on a separate panel), and the cable gland position required.



# C5 - Mains connection

#### C5.2 - TABLE OF TERMINAL BOXES AND CABLE GLANDS FOR RATED SUPPLY VOLTAGE OF 360 to 480V (according to EN 50262)

Frame size	Single-sp	eed motor	Two-spe	Cable gland for accessories:		
Frame SIZE	D.O.L. starting	Y∆ starting	2 windings	1 winding	PTO / PTF / etc	
80	ISO 20	-	2 x ISO 20	ISO 20	ISO 16	
90	ISO 20	-	2 x ISO 20	ISO 20	ISO 16	
100 LK	ISO 20	ISO 20	2 x ISO 20	ISO 20	ISO 16	
112 / 132 S	ISO 20	ISO 20	2 x ISO 20	ISO 20	ISO 16	
132 M	ISO 25	ISO 25	2 x ISO 25	ISO 25	ISO 16	
160 / 180 MR	Motors supplie	ISO 16				
180	Motors supplie	ed with an undrilled cable gland	mounting plate, without nozzle o	or cable gland <sup>1</sup>	ISO 16	
200	Motors supplie	ed with an undrilled cable gland	mounting plate, without nozzle o	or cable gland <sup>1</sup>	ISO 16	
225 ST/MT	Motors supplie	ISO 16				
225 M / 250 / 280	Motors supplie	ISO 16				
315 to 355 LD	Motors supplie	Motors supplied with an undrilled cable gland mounting plate, without nozzle or cable gland <sup>1</sup>				
355 LK to 450	Motors supplie	ed with an undrilled cable gland	mounting plate, without nozzle c	or cable gland <sup>1</sup>	ISO 16	

- standard cable gland material: polyamide 6/6.

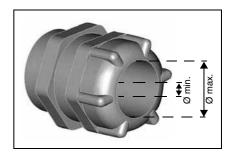
- on request, special brass or stainless steel cable glands can be fitted.

1. From frame size 160, the cable gland mounting plates are supplied without cable glands or drill holes. In order to receive them with drill holes and fitted with cable glands if required, you should specify the number of cables, their diameter and the type of cable gland required on your order.

#### Tightening capacity of cable glands

(NFC 68 311 and 312 standards)

Type of cable gland	Min. cable Ø - Max. cable Ø (mm)				
Type of cable gland	Polyamide cable gland	Brass cable gland			
ISO 16	6 - 10	5.5 - 9.5			
ISO 20	10 - 15	8.5 - 13			
ISO 25	13 - 19	12 - 17			
ISO 32	17 - 25	15 - 22			
ISO 40	24 - 32	19.5 - 28			





# C5 - Mains connection

#### C5.3 - TERMINAL BLOCKS -DIRECTION OF ROTATION

The motors are fitted with a block of six terminals complying with standard NFC 51 120, with the terminal markings complying with IEC 60034-8 (or NFEN 60034-8).

N.B. : Motors of frame size 355 LK, 400 and 450 are fitted with twelve M 14 terminals linked in pairs. The wiring diagram therefore remains the same.

When the motor is running in U1, V1, W1 or 1U, 1V, 1W from a direct mains supply L1, L2, L3, it turns clockwise when seen from the drive shaft end.

If any two of the phases are changed over, the motor will run in an anti-clockwise direction (make sure that the motor has been designed to run in both directions).

Motor type	Terminals
FLS 80 to 112 M	M5
FLS 132 S to 160 L	M6
FLS 180 MR	M6
FLS 180 L	M8
FLS 200	M8
FLS 225 ST-MT	M8
FLS 225 M	M10
FLS 250	M10

If the motor is fitted with thermal protection or space heaters, these are connected and labelled in the main terminal box up to the 355 LD, and in an auxiliary box from the 355 LK to the 450.

Motor type	Terminals
FLS 280	M12
FLS 315	M12
FLS 355 L	M12
FLS 355 LK	M14
FLS 400 L	M14
FLS 400 LK	M14
FLS 450 L	M14

Tightening torque for the nuts on the terminal blocks  $\checkmark$ 

Terminal	M4	M5	M6	M8	M10	M12	M14
Torque N.m	2	3.2	5	10	20	35	50

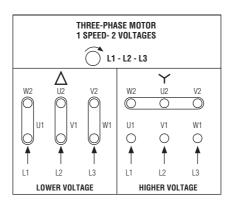
#### **C5.4 - WIRING DIAGRAMS**

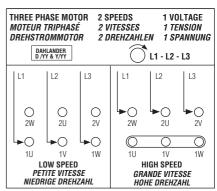
All motors are supplied with a wiring diagram in the terminal box.

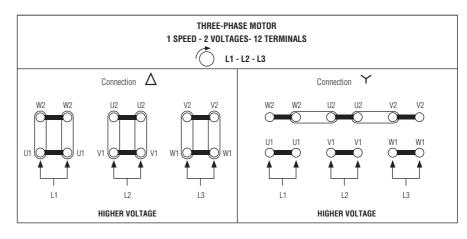
The diagrams normally used are shown opposite.

On the following pages are outline diagrams with internal and external connections.

N.B. : Motors of frame size 355 LK, 400 and 450 are fitted with twelve M 14 terminals linked in pairs. The wiring diagram therefore remains the same.







#### **C5.5 - EARTH TERMINALS**

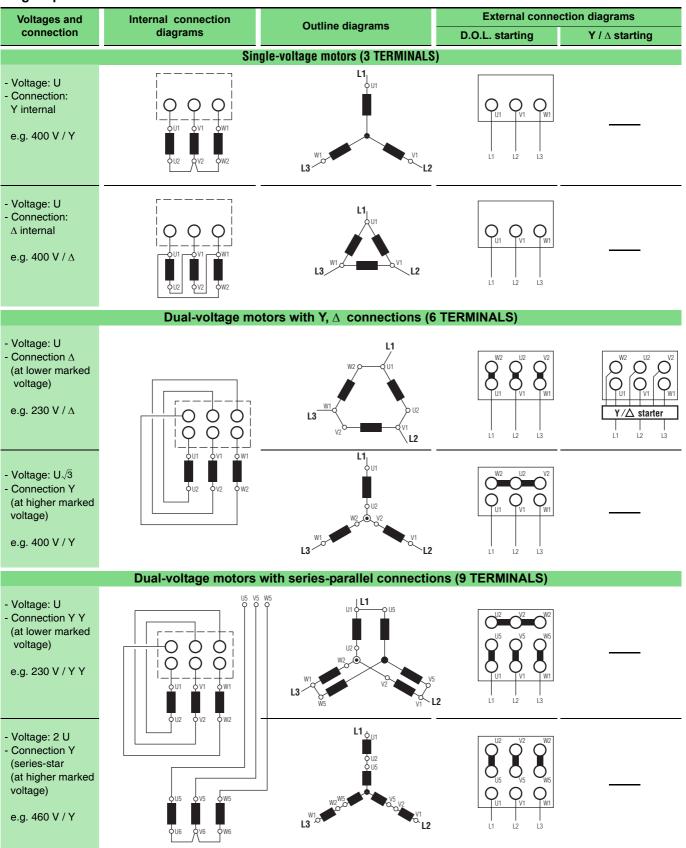
One is located inside the terminal box and the other on one of the feet or one of the cooling fins.

A threaded stud with a hexagonal nut is used to connect cables with cross-sections at least as large as the cross-section of the phase conductors. It is indicated by the sign:  $\perp$  in the terminal box moulding and on the foot or fin.



# C6 - Motor connections

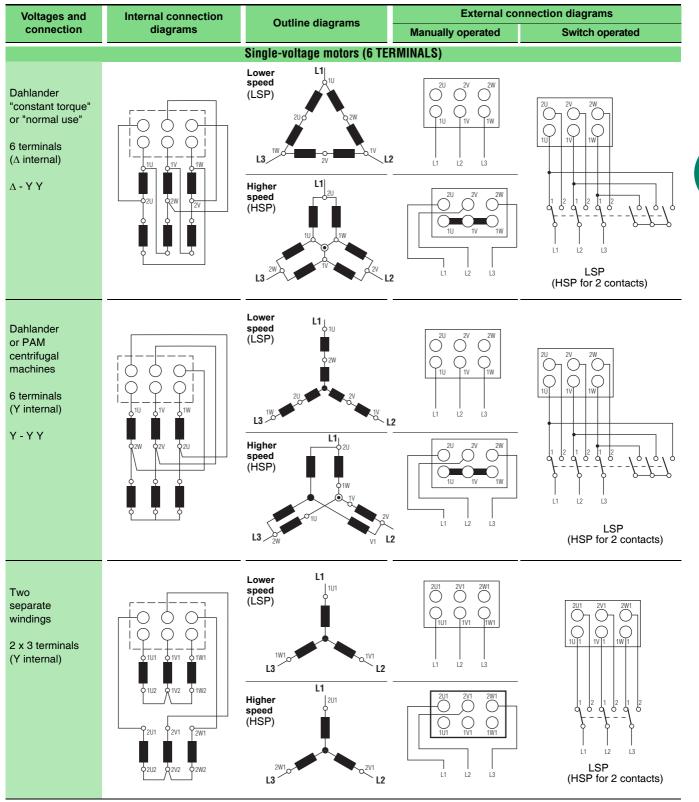




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# C6 - Motor connections

#### **Two-speed motors**



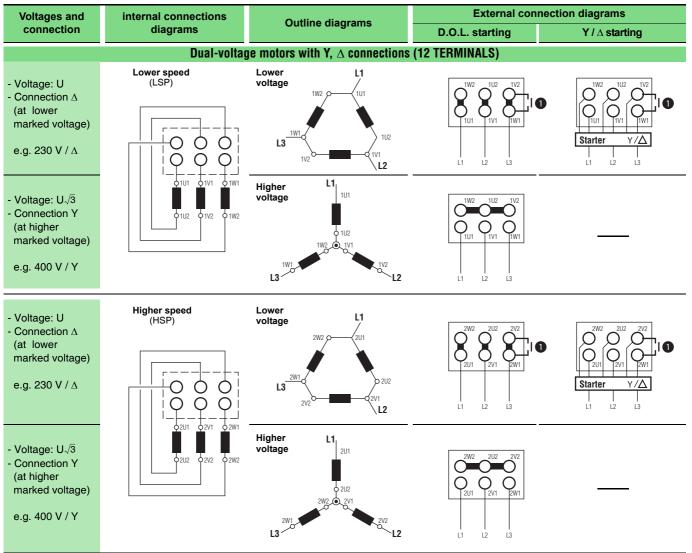
Note: the standardized markings appear on the cables coming from the stator windings.



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# C6 - Motor connections

#### **Two-speed motors**



It is advisable to open the unused circuit (for the speed not in use) to avoid induced currents.

 ${\pmb 0}$  : safety switch open when machine runs at the second speed.



### D1 - Duty cycle - Definitions

Typical duty cycles (according to IEC 60034-1)

#### The typical duty cycles are described below: 1 - Continuous duty - Type S1

Operation at constant load of sufficient duration for thermal equilibrium to be reached (see figure 1).

#### 2 - Short-time duty - Type S2

Operation at constant load during a given time, less than that required for thermal equilibrium to be reached, followed by a rest and de-energized period of sufficient duration to re-establish machine temperatures within 2 K of the coolant (see figure 2).

#### 3 - Intermittent periodic duty - Type S3

A sequence of identical duty cycles, each consisting of a period of operation at constant load and a rest and de-energized period (see figure 3). Here, the cycle is such that the starting current does not significantly affect the temperature rise (see figure 3).

#### 4 - Intermittent periodic duty with starting - Type S4

A sequence of identical duty cycles, each consisting of a significant starting period, a period of operation at constant load and a rest and de-energized period (see figure 4).

#### 5 - Intermittent periodic duty with electrical braking - Type S5

A sequence of periodic duty cycles, each consisting of a starting period, a period of operation at constant load, a period of rapid electrical braking and a rest and de-energized period (see figure 5).

#### 6 - Periodic continuous duty with intermittent load - Type S6

A sequence of identical duty cycles, each consisting of a period of operation at constant load and a period of operation at no load. There is no rest and de-energized period (see figure 6).

#### 7 - Periodic continuous duty with electrical braking - Type S7

A sequence of identical duty cycles, each consisting of a starting period, a period of operation at constant load and a period of electrical braking. There is no rest and de-energized period (see figure 7).

# 8 - Periodic continuous duty with related changes of load and speed - Type S8

A sequence of identical duty cycles, each consisting of a period of operation at constant load corresponding to a predetermined rotation speed, followed by one or more periods of operation at other constant loads corresponding to different rotation speeds (in induction motors, this can be done by changing the number of poles). There is no rest and de-energized period (see figure 8).

#### 9 - Duty with non-periodic variations in load and speed - Type S9

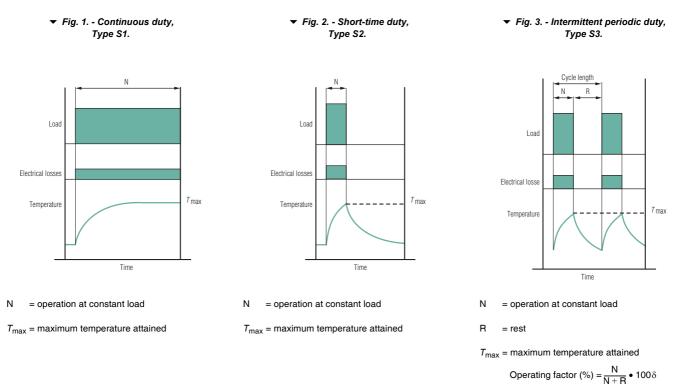
This is a duty in which the load and speed generally vary non-periodically within the permissible operating range. This duty frequently includes applied overloads which may be much higher than the full load or loads (see figure 9).

Note - For this type of duty, the appropriate full load values must be used as the basis for calculating overload.

#### 10 - Operation at discrete constant loads - Type S10

This duty consists of a maximum of 4 discrete load values (or equivalent loads), each value being applied for sufficient time for the machine to reach thermal equilibrium. The minimum load during a load cycle may be zero (no-load operation or rest and de-energized period) (see figure 10).

Note: In section D4.6, there is a method for specifying machines in intermittent duty.

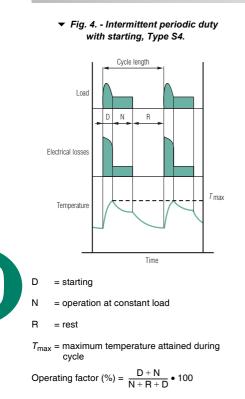




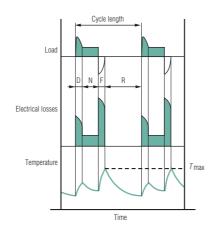
# D1 - Duty cycle - Definitions

▼ Fig. 5. - Intermittent periodic duty

with electrical braking, Type S5.



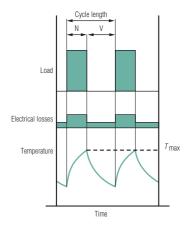
▼ Fig. 7. - Periodic continuous duty with electrical braking, Type S7.



- D = starting
- = operation at constant load Ν
- = electrical braking F
- R = rest

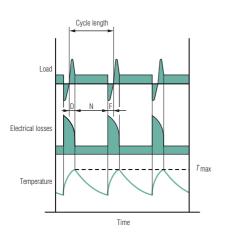
 $T_{max}$  = maximum temperature attained during

cycle Operating factor (%) =  $\frac{D + N + F}{D + N + F + R} \bullet 100$  ▼ Fig. 6. - Periodic continuous duty with intermittent load, Type S6.



- = operation at constant load Ν
- ν = no-load operation
- $T_{max}$  = maximum temperature attained during cvcle

Operating factor (%) =  $\frac{N}{N+V} \bullet 100$ 



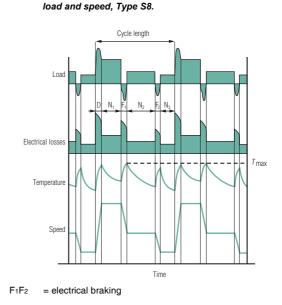
D = starting

Ν = operation at constant load

F = electrical braking

 $T_{max}$  = maximum temperature attained during cycle

Operating factor = 1



▼ Fig. 8. - Periodic continuous duty with related changes of

D = starting

N1N2N3 = operation at constant loads.

T<sub>max</sub> = maximum temperature attained during cycle

Operating factor =

 $D + N_1$ 100 % D + N1 + F1 + N2 + F2 + N3 F1 + N2 100 %  $D + N_1 + F_1 + N_2 + F_2 + N_3$ F2 + N3



# D1 - Duty cycle - Definitions

 Fig. 9. - Duty with non-periodic variations in load and speed, Type S9.

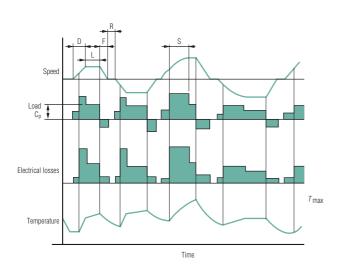
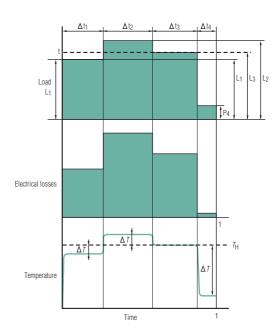


 Fig. 10 - Duty at discrete constant loads, Type S10.



- D = starting
- L = operation at variable loads
- F = electrical braking
- R = rest
- S = operation at overload
- C<sub>p</sub> = full load
- $T_{\text{max}}$  = maximum temperature attained.

- L = load
- N = power rating for duty type S1
- $p = p / \frac{L}{N} = reduced load$
- t = time

t

- T<sub>p</sub> = total cycle time
  - = discrete period within a cycle
- $\label{eq:lambda} \begin{array}{ll} \Delta t_i & = t_i \ / \ T_p = \mbox{relative duration of period} \\ & \mbox{within a cycle} \end{array}$
- Pu = electrical losses
- H<sub>N</sub> = temperature at power rating for duty type S1
- $\Delta H_i$  = increase or decrease in temperature rise at the ith period of a cycle

Power is determined according to duty cycle. See section D4.6.



# D2 - Supply voltage

# D2.1 - REGULATIONS AND STANDARDS

The statement by the electricity consultative committee dated 25th June 1982, and the 6th edition (1983) of publication No. 38 of the International Electrotechnical Committee (IEC) have laid down time scales for the harmonisation of standard voltages in Europe. Since 1998, voltages at the point of delivery have to be maintained between the following extreme values:

Single-phase current: 207 to 244 V

• Three-phase current: 358 to 423 V The IEC 60038 standard gives the

European reference voltage as 230/400 V three-phase and 230 V single-phase, with a tolerance of +6% to -10% until 2003 and ±10% from then on.

- The tolerances usually permitted for power supply sources are indicated below:
- Maximum line drop between customer delivery point and customer usage point: 4%.

• Variation in frequency around nominal frequency:

- continuous state : ±1%
- transient state : ±2%

• Three-phase mains phase-balance error: - zero-sequence component and/or negative phase sequence component compared to positive phase sequence component: < 2%

- Harmonics:
- relative harmonic content: <10%
- individual harmonic voltages:
- to be established
- Surges and transient power cuts: to be established

# The motors in this catalogue are designed for use on the European power supply of 230/400 V $\pm$ 10% - 50 Hz.

This means that the same motor

- can operate on the following existing supplies: 220/380 V  $\pm 5\%$
- 230/400 V ±5% and ±10%
- 240/415 V ± 5%

and is therefore suitable for a large number of countries worldwide where for example it is possible to extend them to some 60 Hz supplies:

- 265/460 V ± 10%

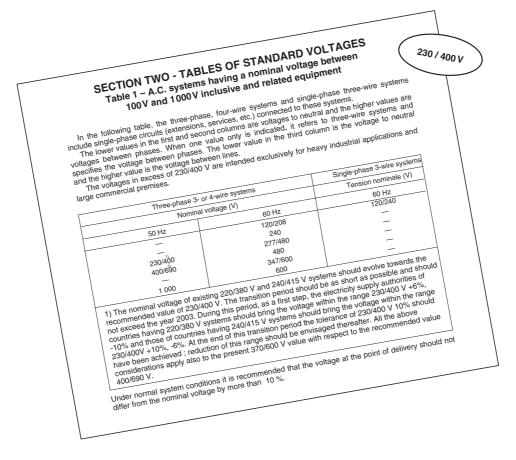
From 2008, 380 and 415 V - 50 Hz voltage supplies must be eliminated.







# D2 - Supply voltage



#### D2.2 - EFFECTS ON MOTOR PERFORMANCE

#### D2.2.1 - Voltage range

The characteristics of motors will of course vary with a corresponding variation in voltage of  $\pm 10\%$  around the rated value.

An approximation of these variations is given in the table opposite (precise values for each motor can be supplied on request).

	Voltage variation as a %						
	UN-10%	UN-5%	UN	Un+5%	Un+10%		
Torque curve	0.81	0.90	1	1.10	1.21		
Slip	1.23	1.11	1	0.91	0.83		
Rated current	1.10	1.05	1	0.98	0.98		
Rated efficiency	0.97	0.98	1	1.00	0.98		
Rated power factor (Cos $\phi$ )	1.03	1.02	1	0.97	0.94		
Starting current	0.90	0.95	1	1.05	1.10		
Nominal temperature rise	1.18	1.05*	1	1*	1.10		
P (Watt) no-load	0.85	0.92	1	1.12	1.25		
Q (reactive V A) no-load	0.81	0.9	1	1.1	1.21		

\* According to standard IEC 60034-1, the additional temperature rise must not exceed 10 K within ±5% of Un.



# D2 - Supply voltage

# D2.2.2 - Simultaneous variation of voltage and frequency

Within the tolerances defined in IEC guide 106, machine input and performance are unaffected if the variations are of the same polarity and the voltage/frequency ratio U/f remains constant.

If this is not the case, variations in performance are significant and require the machine specification to be changed.

# D2.2.3 - Use of 400V - 50 Hz motors on 460V - 60 Hz supplies

For a rated power at 60 Hz 15 to 20% greater than the rated power at 50 Hz (see section E), the main characteristics are modified according to the following variations, which necessitate replating of the motor:

- Efficiency increases by 0.5 - 3%

- Power factor increases by 0.5 3%
- -Rated current decreases by 0 5%
- $-I_D / I_N$  increases by around 10%

# D2.2.4 - Motors powered by a 500V - 50 Hz supply

Motors powered by this supply and Y or  $\Delta$  connected are a special type of construction

#### D2.2.5 - Phase voltage imbalance

The phase imbalance for voltage is calculated as follows:

% voltage imbalance = 100 x	maximum difference in volta compared to average voltage value
	average voltage value

The effect on motor performance is summarized in the table opposite.

If this imbalance is known before the motor is purchased, it is advisable, in order to

### D2.2.6 - Phase current imbalance

Voltage imbalances induce current imbalances. Natural lack of symmetry due to manufacture also induces current imbalances.

The chart opposite shows the ratios in which the negative phase component is equal to 5% (and 3%) of the positive phase components in three-phase current supplies without zero components (neutral absent or not connected).

Inside the curve, the negative phase component is lower than 5% (and 3%).

Variation in main motor parameters (approx.) within the limits defined in IEC Guide 106.

U <sub>/f</sub>	Pu	М	N	<b>Cos</b> φ	Efficiency
Constant	Pu <mark>ť</mark> f	М	$N\frac{f'}{f}$	cos φ unchanged	Efficiency unchanged
Variable	$Pu\frac{f'}{f}\left(\frac{u'}{u}\right)^2$	$M \left( \frac{u'/u}{f/f'} \right)^2$	N <mark>f</mark>	Depends of satu of ma	uration

M = minimum and maximum values of starting torque.

-Slip and rated torque  $M_N,\,M_D\,/\,M_N,$ 

 $M_M / M_N$  remain more or less constant.

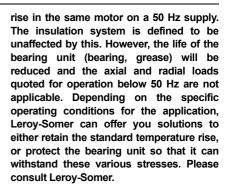
#### VERY IMPORTANT NOTE:

The motors defined in this catalogue which can be used with a 60 Hz supply, will NOT CONFORM with CSA or UL standards. To conform with these standards, a different type of construction is needed. FLS motors rated > 110 kW can be powered by a 460V / 60 Hz supply. In these conditions, the temperature rise in the stator winding may be 15 to 20% higher than the temperature

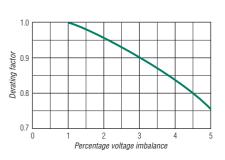
and a quotation should be obtained from Leroy-Somer. Their characteristics with regard to speed, efficiency, cos  $\phi$ , M<sub>D</sub> / M<sub>N</sub> and I<sub>D</sub> / I<sub>N</sub> are almost unchanged. Only the

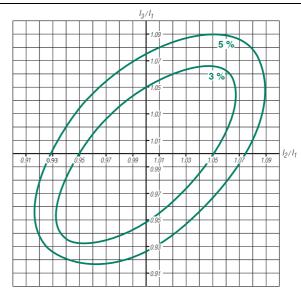
establish the type of motor required, to apply the derating specified in standard IEC 60892, illustrated on the graph opposite.

imbalance	0	2	3.5	5
Stator current	100	101	104	107.5
% increase in losses	0	4	12.5	25
Temperature rise	1	1.05	1.14	1.28



current varies in the voltage ratio for a given power. Exact values will be supplied with the quotation.







### D3 - Insulation class - Temperature rise and thermal reserve

#### Insulation class

The machines in this catalogue have been designed with a class  ${\sf F}$  insulation system for the windings.

Class F allows for temperature rises of 105 K (measured by the resistance variation method) and maximum temperatures at the hot spots in the machine of 155  $^{\circ}$ C (Ref. IEC 60085 and IEC 60034-1).

Complete impregnation with tropicalized varnish of thermal class 180 °C gives protection against attacks from the environment, such as: 90% relative humidity, interference, etc.

For special constructions, the winding is class H and impregnated with special varnishes which enable it to operate in conditions of high temperatures with relative air humidity of up to 100%.

Temperature rise ( $\Delta T^*$ ) and maximum temperatures at hot spots ( $T_{max}$ ) for insulation classes (IEC 60034 - 1).

	∆ <b>7</b> *	T <sub>max</sub>
Class B	80 K	130°C
Class F	105 K	155°C
Class H	125 K	180°C

 $^{\ast}$  Measured using the winding resistance variation method.

The insulation of the windings is monitored in two ways:

a - Dielectric inspection which involves checking the leakage current, at an applied voltage of (2U + 1000) V, in conditions complying with standard IEC 60034-1 (systematic test).

b - Monitoring the insulation resistance between the windings and between the windings and the earth (sampling test) at a D.C. voltage of 500V or 1000V.

# Temperature rise and thermal reserve

LEROY-SOMER motors are built to have a maximum winding temperature rise of 80 K under normal operating conditions (ambient temperature 40 °C, altitude below 1000 m, rated voltage and frequency, rated load).

Running at the voltage limit ( $\pm$  10% of U<sub>N</sub>) will induce overheating of less than 15 K.

In IEC 60034-1 and 60034-2, temperature rise ( $\Delta\theta$ ) is calculated using the winding resistance variation method, with the formula:

$$\Delta T = \frac{R_2 - R_1}{R_1} (235 + T_1) + (T_1 - T_2)$$

 $R_1$  : cold resistance measured at ambient temperature  $T_1$ 

 ${\rm R}_2$  : stabilized hot resistance measured at ambient temperature  ${\rm T}_2$ 

235 : coefficient for a copper winding (for an aluminium winding, the coefficient is 225)

The result is a thermal reserve linked to the following factors:

• a difference of 25 K between the nominal temperature rise (Un, fn, Pn) and the permissible temperature rise (105 K) for class F insulation.

• a difference of over 20 K at the voltage limits (Un  $\pm$  10%) between the actual temperature rise and the permissible temperature rise.

• see chapter D2.2.3 / page 60.



D



## D4 - Power - Torque - Efficiency - Power Factor (Cos $\phi$ )

#### **D4.1 - DEFINITIONS**

The output power (Pu) at the motor shaft is linked to the torque (M) by the equation:

 $Pu = M.\omega$ where Pu is in W, M is in N.m,  $\omega$  is in rad/s and where  $\boldsymbol{\omega}$  is expressed as a function of the speed of rotation in min<sup>-1</sup> by the equation:

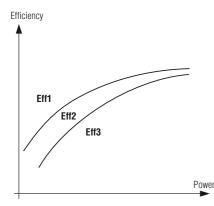
 $\omega = 2\pi N/60$ 

The active power (P) drawn from the mains is expressed as a function of the apparent power

#### **D4.2 - EFFICIENCY**

In accordance with the agreements signed at the RIO and BUENOS AIRES INTERNATIONAL CONFERENCES, the generation of motors with new aluminium or cast iron frame has been designed to improve efficiency by reducing atmospheric pollution (carbon dioxide).

The improvement in efficiency of low voltage industrial motors (representing around 50% of installed power in industry) has had a large impact on energy consumption.



3 levels of efficiency Eff. 1-2-3 have been defined in a European agreement for 2 and 4-pole motors from 1.1 to 90 kW and this catalogue presents the reference range of FLS(C) Eff 2 motors.

Level Eff 3 in version FLS(C) has not been manufactured for some years now. The Eff 1 level range is available on request.

The European recommendation for measuring efficiency recommends testing using the separate losses method (in accordance with IEC 60034-2) on motors not fitted with bearing seals.

(S) and the reactive power (Q) by the equation:

$$S = \sqrt{P^2 + Q^2}$$

(S in VA, P in W and Q in VAR)

The power P is linked to the output power Pu by the equation:

F

The output power Pu at the motor shaft is expressed as a function of the phase-tophase mains voltage (U in Volts), of the line current absorbed (I in Amps) by the equation:

$$Pu = U.I. \sqrt{3} \cdot \cos \varphi \cdot \eta$$

where  $\cos \varphi$  is the power factor found from the ratio:

 $\cos \varphi = \frac{P}{S}$ 

$$P = \frac{Pu}{\eta}$$

where  $\eta$  is the efficiency of the machine.

The advantages of improvement in efficiency:

Motor characteristics	Effects on the motor	Customer benefits
Increase in efficiency and in power factor.	Increase in specific output power.	Lower operating costs. Longer service life (x2 or 3). Better return on investment.
Noise reduction.		Improved working conditions.
Vibration reduction.		Quiet operation and longer service life of driven controls.
Temperature reduction.	Longer service life of fragile components (insulation system components, greased bearings).	Reduction in operating incidents and reduced maintenance costs.
	Increase in the capacity of instantaneous or extended overloads.	Wider field of applications (voltages, altitude, ambient temperature, etc).

#### D4.3 - INFLUENCE OF LOAD ON $\eta$ AND POWER FACTOR COS $\phi$ See the selection data in section E.

Overrating motors in a number of applications causes them to operate at about 3/4 load, resulting in optimum motor efficiency.



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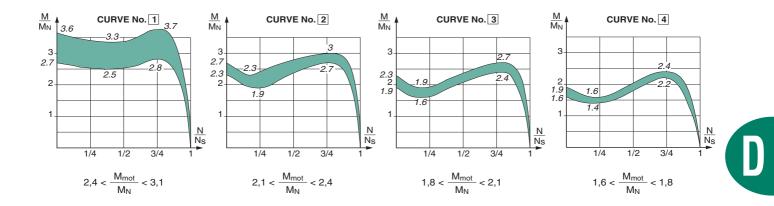
# D4 - Power - Torque - Efficiency - Power Factor (Cos $\phi$ )

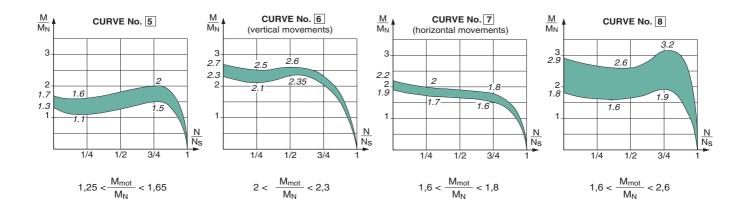
#### **D4.4 - TORQUE-SPEED CHARACTERISTICS**

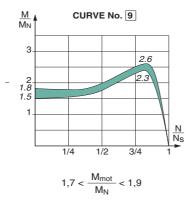
Below are torque/speed curves that correspond to a range of typical cases (different sizes of motor, no. of poles, etc).  $M_{mot}$  is the average starting torque of the motor.

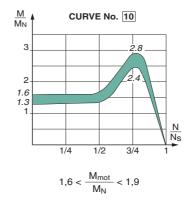
To find the accelerating torque, subtract the average load resistive torque from the average starting torque of the motor.

The curve numbers refer back to the electromagnetic characteristic selection tables in section E.











# D4 - Power - Torque - Efficiency - Power Factor (Cos φ)

#### D4.5 - CALCULATION OF ACCELERATING TORQUE AND **STARTING TIME**

Acceleration time can be calculated using a simplified formula:

$$t_{d}=\frac{\pi}{30}~\frac{N\cdot J_{N}}{M_{a}}$$
 , where:

 $t_d$  : is the acceleration time in seconds  $J_N$  = moment of inertia in kg.m<sup>2</sup> of the motor plus the load corrected, if necessary, to the speed of the shaft that develops the torque M<sub>a</sub> N: speed to be achieved in min-1

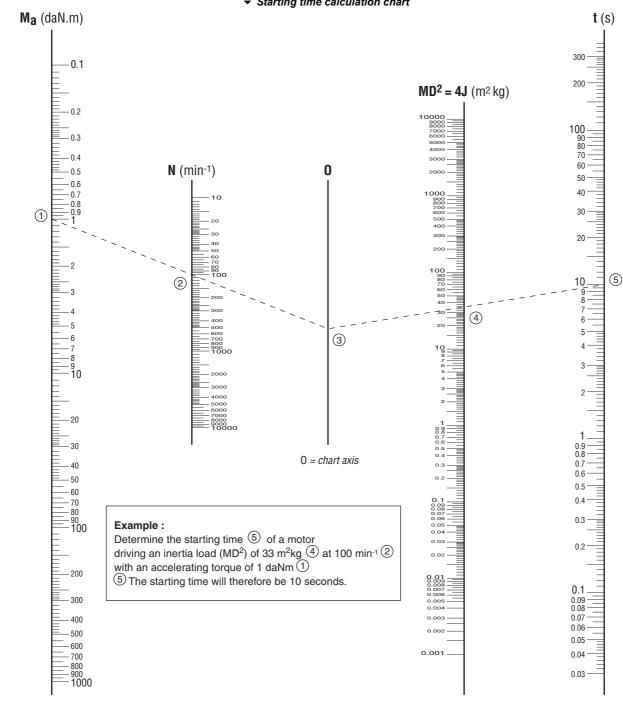
 $M_a$  or  $M_{acc}$  = the average accelerating torque in N.m (average torque developed by the motor during starting, reduced by the average resistive torque during the same period). In general, for centrifugal machines, a very good approximation can be written as follows:

$$M_{a} = \frac{M_{D} + 2M_{A} + 2M_{M} + M_{N}}{6} - M$$

The chart below may also be used:

Here again is the formula by which the moment of inertia of the driven machine turning at speed N' is equalized with the speed N of the motor.

$$\mathbf{J}_{\mathbf{N}} = \mathbf{J}_{\mathbf{N}'} \cdot \left(\frac{\mathbf{N}'}{\mathbf{N}}\right)^2$$



LEROY\* SOMER

Starting time calculation chart



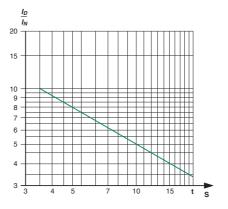
# D4 - Power - Torque - Efficiency - Power Factor (Cos φ)

# Permissible starting times and locked rotor time

The starting times calculated by using the chart on the previous page must remain within the limits opposite on condition that the number of starts per hour is 6 or less.

Three successive cold starts and two consecutive warm starts are allowed.

Permissible motor starting time for each motor in relation to the ratio  $I_D / I_N$  for 6 cold starts/hour.



The table below gives locked rotor times at full voltage (e.g. incident on the transmission) for the motor when warm and when cold (ambient temperature: 40 °C):

	2 p	oles	4 p	oles	6 p	oles	8 p	oles
Туре	t (cold) s	t (warm) s						
FLS 80	8	3	12	6	16	8	18	9
FLS 90	6	3	9	5	18	9	30	11
FLS 100	5	2.5	8	4	20	7	30	11
FLS 112	5	2.5	5	2.5	11	5	25	9
FLS 132	5	2.5	5	2.5	9	4	20	5
FLS 160 M	11	2	14	3	23	4.5	34	7
FLS 160 L	8	2	9	2	17	3.5	31	6
FLS 180 MR	6	1	12	2.5	-	-	-	-
FLS 180 L	-	-	13	2.5	7	1.5	33	6
FLS 200	14	3	15	3	14	2.5	42	8
FLS 225	12	2.5	16	3	20	4	25	5
FLS 250	21	7	15	5	23	7.5	23	7.5
FLS 280	15	5	12	4	16	5.5	23	7.5
FLS 315 ST	20	4	24	5	12	2.5	10	2
FLS 315 M	20	4	12	2.5	17	3.5	15	3
FLS 315 L	30	6	12	2.5	17	3.5	15	3
FLS 355 LA/LB	25	5	12	2.5	15	3	17	3.5
FLS 355 LC/LD	20	4	15	3	15	3	20	4
FLS 355 LK	-	-	30	6	20	4	20	4
FLS 400	-	-	30	6	20	4	20	4
FLS 450	-	-	30	6	20	4	20	4



## D4 - Power - Torque - Efficiency - Power Factor (Cos $\phi$ )

#### D4.6 - RATED POWER Pn IN **RELATION TO DUTY CYCLE** D4.6.1 - General rules for standard motors

 $P_{n} = \sqrt{\frac{n \times t_{d} \times \left[I_{D} / I_{n} \times P\right]^{2} + (3600 - n \times t_{d})P_{u}^{2} \times fdm}{2}}$ 3600

Iterative calculation where:

- starting time of motor with t<sub>d</sub>(s) power P(w)
- number of (equivalent) starts n per hour
- OF operating factor (decimal)
- I<sub>D</sub>/I<sub>n</sub> starting current of motor with
- power P P<sub>u</sub> (w) output power of motor during the
- duty cycle using OF (in decimal), operating factor P (w) rated power of motor
- selected for the calculation

Note: n and OF are defined in section

D4.6.2 Sp = specification

	•	
S1	OF = 1; n ≤ 6	
S2		; n = 1 length of operation determined by Sp
S3	OF according to Sp;	n ~ 0 (temperature rise not affected by starting)
S4	OF according to Sp	; n according to Sp; t <sub>d</sub> , P <sub>u</sub> , P according to Sp (replace n with 4n in the above formula)
S5	OF according to Sp	; n = n starts + 3 n brakings = 4 n; $t_d$ , $P_u$ , P acc. to Sp (replace n with 4n in the above formula)
S6	$\mathbf{P} = \sqrt{\frac{\Sigma(\mathbf{P}_i^2 \cdot \mathbf{t}_i)}{\Sigma \mathbf{t}_i}}$	
S7	same formula as S5	but OF = 1
S8	at high speed, same at low speed, same f	
S9	S8 duty formula after cycle with OF on eac	complete description of h speed
S10	same formula as S6	

In addition, see the warning regarding precautions to be taken. Variations in voltage and/or frequency greater than standard should also be taken into account. The application should also be taken into account (general at constant torque, centrifugal at quadratic torque, etc).

#### D4.6.2 - Determination of the power in intermittent duty cycles for adapted motors

#### rms power in intermittent duty

This is the rated power absorbed by the driven machine, usually defined by the manufacturer.

If the power absorbed by the machine varies during a cycle, the rms power P is calculated using the equation:

$$P = \sqrt{\frac{\sum_{1}^{n}(P_{i}^{2} \cdot t_{i})}{\sum_{1}^{n}t_{i}}} = \sqrt{\frac{P_{1}^{2} \cdot t_{1} + P_{2}^{2} \cdot t_{2} \dots + P_{n}^{2} \cdot t_{n}}{t_{1} + t_{2} + \dots + t_{n}}}$$

if, during the working time the absorbed power is:

P<sub>1</sub> for period t<sub>1</sub>

P<sub>2</sub> for period t<sub>2</sub>

P<sub>n</sub> for period t<sub>n</sub>

Power values lower than 0.5 P<sub>N</sub> are replaced by 0.5 P<sub>N</sub>in the calculation of rms power P (no-load operation is a special case).

Additionally, it is also necessary to check that for a particular motor of power P<sub>N</sub>:

· the actual starting time is at most equal to 5 seconds

· the maximum output of the cycle does not exceed twice the rated output power P

· there is still sufficient accelerating torque during the starting period

#### Load factor (LF)

Expressed as a percentage, this is the ratio of the period of operating time with a load during the cycle to the total duration of the cycle where the motor is energized.

#### **Operating factor (OF)**

Expressed as a percentage, this is the ratio of the motor power-up time during the cycle to the total cycle time, provided that the total cycle time is less than 10 minutes.

#### Starting class

Class:  $n = n_D + k.n_F + k'.n_i$ 

n<sub>D</sub> is the number of complete starts per hour n<sub>F</sub> is the number of times electrical braking is applied per hour

"Electrical braking" means any braking directly involving the stator winding or the rotor winding:

· Regenerative braking (with frequency controller, multipole motor, etc)

Reverse-current braking (the most commonly used)

• D.C. injection braking

ni is the number of impulses (incomplete starts up to one-third of maximum speed) per hour.

k and k' are constants determined as follows:

	k	k'
Cage induction motors	3	0.5

Reversing the direction of rotation involves braking (usually electrical) and starting.

- Braking with LEROY-SOMER electromechanical brakes, as with any other brakes that are independent of the motor, does not constitute electrical braking in the sense described above.

**Calculating derating** Input criteria (load)

- rms power during the cycle = P Moment of inertia corrected to speed of motor = Je

- Operating factor = OF
- Class of starts per hour = n

- Resistive torque during starting = Mr

- Selection in catalogue
- Motor power rating P<sub>N</sub>
- Starting current  $I_d$ ,  $cos\phi_D$
- Moment of inertia of rotor J<sub>r</sub>
- Average starting torque Mmot
- Efficiency at  $P_N(\eta_{PN})$  and at  $P(\eta_P)$

#### Calculations

- Starting time:

$$t_{d} = \frac{\pi}{30} \cdot N \cdot \frac{(J_{e} + J_{r})}{M_{max} - M_{r}}$$

 $\overline{M_{mot}} - M_r$ - Cumulative starting time per hour: nxt<sub>d</sub>

Energy to be dissipated per hour during starts = sum of the energy dissipated in the rotor (= inertia acceleration energy) and the energy dissipated in the stator during the cumulative starting time per hour:

$$E_{d} = \frac{1}{2}(J_{e} + J_{r})\left(\frac{\pi \cdot N}{30}\right)^{2} \times n + n \times t_{d}\sqrt{3}UI_{d}\cos\phi_{d}$$

- Energy to be dissipated during operation  $E_f = P. (1 - \eta_P) . (fdmx3600 - nxt_d)$ 

Energy that the motor can dissipate at rated power with the Operating Factor for Intermittent Duty.

 $E_m = (OF) 3600 \cdot P_N \cdot (1 - \eta_{PN})$ 

(The heat dissipated when the motor is at rest can be ignored).

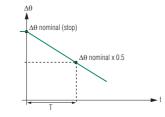
Dimensioning is correct if the following relationship is verified =

$$E_m \ge E_d + E_f$$

If the sum of  $E_d + E_f$  is lower than 0.75  $E_m$ check whether a motor with the next lowest power would be more suitable.

#### D4.6.3 Equivalent thermal constant

The equivalent thermal constant enables the machine cooling time to be predetermined.



Thermal constant =  $\frac{T}{In2}$  = 1.44 T

Cooling curve  $\Delta \theta = f(t)$ 

where  $\Delta \theta$ = temperature rise in S1 duty T = time required for nominal

- temperature rise to reach half its value
- t = time
- In = natural logarithm

#### D4.6.4 - Transient overload after operating in type S1 duty cycle

At rated voltage and frequency, the motors can withstand an overload of:

- 1.20 for an OF = 50 % 1.40 for an OF = 10%
- However, it is necessary to ensure that the maximum torque is much greater than 1.5

times the rated torque corresponding to the overload.



# D5 - Speed of rotation

#### D5.1 - SINGLE FIXED SPEED MOTOR

The great majority of applications only require a single fixed speed. If this applies to you, you should opt for a 1500 min<sup>-1</sup> or possibly 3000 min<sup>-1</sup> motor (50 Hz supply) which are the ones most frequently used. However, even with fixed speeds there are

two types of application which fall outside the standard speed range of 750 to 3000 min<sup>-1</sup>.

#### D5.1.1 - High-speed motor

High-speed motors, operating at speeds of over 3000 min<sup>-1</sup>, obtained by using supplies with fixed frequencies other than 50 Hz, for example 100, 200 or 400 Hz: the motor will run at a synchronous speed N such that:

$$N = \frac{120}{p} \cdot f$$

(N is in min<sup>-1</sup>; f is the frequency of the supply in Hz; p is the number of motor poles). Motors of this type have to be specially designed, taking into account the following important points:

- the wave form of the high frequency supply (type of harmonics and total harmonic distortion)

 increased magnetic losses in relation to frequency

- mechanical properties of rotors

- bearing properties, lubrication, lifetime, temperature rises

- ventilation, noise levels, vibrations

- starting current, motor torque, load inertia It should also be noted that high speed applications are limited to smaller machines: the higher the speed, the smaller the machine must be.

#### D5.1.2 - Low-speed motor

Low-speed motors, running at under 750 min<sup>-1</sup>. Low speeds are obtained either by using a supply with a fixed frequency of under 50 Hz, or by using more than 8 poles with a 50 Hz supply. Motors of this type also have to be specially designed to deal with the problems involved in this type of application, such as:

- resistive torgue and driven inertia and in the manufacture:

ventilation

The most widely used fixed frequency (50 Hz) low speeds are 500 min<sup>-1</sup> (12-pole motor) and 375 min<sup>-1</sup> (16-pole motor).

#### **D5.2 - MULTIPLE FIXED SPEEDS** MOTOR

Some applications require operation at two or three fixed speeds. These can be obtained by changing the poles in a multispeed motor. There are a large number of solutions, but we shall only look at the following:

#### D5.2.1 Motor with single winding

Motors with a single winding (Dahlander connection [speed ratio: 2:1]) or PAM (any speed ratio):

Internal connection of stator windings is used for specific applications:

Dahlander Y - Y or  $\Delta$  -  $\Delta$ centrifugal { Damana PAM - Y applications other applications - Dahlander  $\Delta$  - Y

In general, these motors are designed for D.O.L. starting from the mains supply and are single-voltage.

The most common speed ratios are: - 3000 / 1500 min<sup>-1</sup> (2 / 4 poles) -1500 / 750 min<sup>-1</sup> (4 / 8 poles)

#### D5.2.2 - Motor with separate windings

Motors with two separate windings. Different starts are obtained depending on the winding connections on the terminal block: 2 x 3 terminals: Direct-On-Line (D.O.L.) starting

2 x 6 terminals: Y /  $\Delta$  starting possible.

In the first case, these motors will be singlevoltage; in the second, they may be either dual-voltage or  $Y / \Delta$  starting single-voltage motors

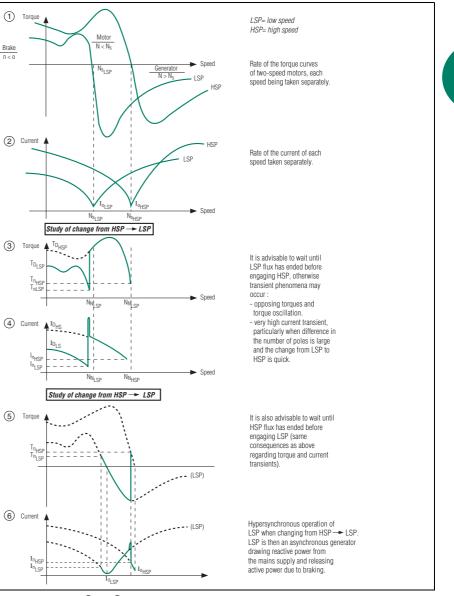
The most common speed ratios are:

-1000 / 750 min<sup>-1</sup> (6 / 8 poles)

-1500 / 1000 min<sup>-1</sup> (4 / 6 poles)

#### D5.2.3 - Behaviour of two-speed motors

Each speed of a multi-speed motor behaves like a complete motor (curves ① and ②) with operation as a brake, a motor and an asynchronous generator, depending on the quadrant.



The above curves 3 to 6 explain how the torques and currents develop when the motor changes from low speed to high speed and vice versa.

Note: The greater the difference between the number of poles, the more likelihood of: - significant current peak at LSP - long braking time and risk of temperature rise at LSP - high level of hypersynchronous noise Some of these phenomena can be aggravated if the driven inertia is high. The rated power is determined according to the criteria in section D4.6.1 for each of the two speeds (see type S8 duty). Manufacturers' recommendations should be followed regarding devices for connecting to the mains supply and protection, using equipment which has already been examined and for which the problems of transient current peaks have been resolved.



# D5 - Speed of rotation

#### D5.2.4 - Operating rules

A few common-sense rules need to be applied to get the best out of a two-speed motor:

- Avoid large differences in the number of poles (for example 2/12p, 2/16p, 4/20p, etc): the torque drop at high speed occurs at a speed greater than the synchronous speed at low speed. The motor may start to "crawl" and never reach its higher speed rating.

- It is better to start the motor at the lower speed: this effectively eliminates the high speed torque drop, thus reducing the starting time. It will also limit current surge. - As well as taking the precaution advised in the previous paragraph, current surge can be limited using the advice given in section D8 on "starting". Do bear in mind, though, that not all two-speed motors can be started using the suggested types of starting.

- An important precaution for motors with two separate windings, if the normal connection is a delta, is to "open" the delta for the speed not in use to avoid inducing circulating currents which can create opposing torques and harmful temperature rises.

#### D5.2.5 - Two-speed motors with connected windings

For ventilation applications, we manufacture two-speed motors by connecting the windings on a single-speed motor:

- High speed by delta connection at full voltage.

Low speed by star connection at full voltage.

The second speed is obtained because the motor is seriously desaturated (voltage divided by 1.732 at the phase terminals) and the rotor is experiencing a great deal of slip: as a result, there is a significant rotor temperature rise - since all the Joule losses due to the slip are dissipated in it - and risks of significant overheating - by conduction in the windings if essential derating precautions have not been taken.

In fact, equilibrium is achieved for both speed and temperature rise by means of the following principles:

- The power varies in the same way as the speed power three.

- The slip varies as a function of the output and the temperature rise.

The choice of alloy for the rotor squirrel cage depends on the required output speeds.

When the power absorbed by the fan varies for reasons not related to the selected operating principle - for example, dirt on the fan blades, temperature of the air flow, variation of power supply frequency or voltage, etc. - the temperature rise in the rotor varies and allows speed equilibrium to regained without making any be adjustments (unless the variations exceed the maximum motor torque in the relevant connection).

The immediate consequence of these random conditions is to define the motor according to its load (driven inertia, power, speeds, etc) and to optimize the choice using real tests. The number of poles chosen for these applications should be four poles or more, and the power rating less than 7.5 kW with 4 poles. We do not offer actual motor ranges, but will undertake development work in a technical partnership.

#### D5.2.6 - Special cases

Motors with more than two speeds have to be specially designed, as, in the majority of cases, the precise nature of the load must be specified.

#### D5.3 - VARIABLE SPEEDS

Improvements in manufacturing processes have led to the introduction of variable speed control.

Two different procedures can be

used on motors:

- slip variation at fixed frequency

supply frequency variation

#### D5.3.1 - Slip variation at fixed frequency

On a motor of a given build, slip other than the rated slip can be obtained by either increasing the load or decreasing the supply voltage.

As an increase in slip is accompanied by increased rotor losses, special rotors have now been designed for use in motors for very specific applications.

The most common application is the hightorque motor with a high-resistance rotor, used with variable voltage, providing constant torque within a specified range of speeds.

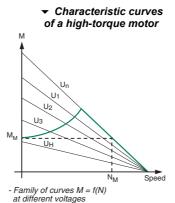
These motors have to be specially designed.

The family of curves below shows the variation in motor torque in relation to the supply voltage UN > U1 > U2, etc.

The green curve shows the maximum torque available in relation to speed for a maximum temperature rise for the insulation class in Type S1 duty (normally with forced ventilation).

The dotted curve shows the maximum constant torque available in Type S1 duty in the speed range 0 to NM.

The available powers and torques of these motors in Type S1 duty are much lower than those of standard motors of the same type.

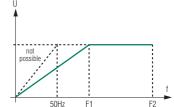


Maximum use in S1 type duty  $M_M$  maximum constant torque from 0 to  $N_M$ in S1 type duty

#### D5.3.2 - Frequency variation

In induction motors, variations of speed within a wide range are obtained using a power supply with variable frequency and voltage.

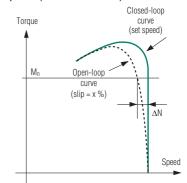
As a general rule, the frequency inverter delivers a proportional voltage and frequency up to a value  $F_1$ , which depends on the manufacturer and/or the user, and a fixed voltage up to a maximum frequency value of  $F_2$ . In these conditions, the motor output is proportional to the frequency up to the value  $F_1$  ( $F_1$  = frequency where the U/f ratio changes), and then constant up to the value FF<sub>2</sub>.



In practice, certain adjustments have to be made. At low frequency, to maintain significant torque, the inverter provides greater saturation of the motor (and thus a higher U value); the value of F1 is itself made variable so as to widen the range of use at constant torque (or at proportional power).

In addition, forced ventilation enhances motor cooling at low speeds and reduces noises levels at high speeds.

In applications where accurate speed regulation is required, the variable speed drive can be used with closed-loop feedback by fitting a speed detector (D.C. tacho, A.C. tacho or encoder) which will send a signal to the inverter to change its U/ f ratio and so regulate the speed at the level required (see curve below).



Using induction motors at high speeds (over about 4000pmin<sup>-1</sup>) can be risky. The cage may be damaged, bearing life impaired, as well as vibration and high-frequency saturation leading to heavy losses and significant temperature rises, etc. An indepth mechanical and electrical design exercise is needed for all high-power machines required to operate at speeds of over 4000 min-1 (see the table of mechanical speed limits at the end of this section).



D5 - Speed of rotation

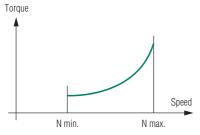
High-speed motors often need to be adapted to suit their application, and this work may include:

- fitting a speed detector
- (D.C. tacho, A.C. tacho or encoder)
- fitting forced ventilation
- fitting a brake or decelerator

#### Applications and choice of solutions There are three main types of load:

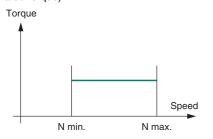
#### a - Centrifugal machines

The output torque varies as the square of the speed. The torque required for acceleration is low (about 20% of rated torque).



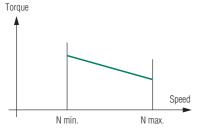
#### **b** - Constant torque applications

The output torque remains constant throughout the speed range. The torque required for acceleration may be high, depending on the machine (higher than the rated torque).



#### c - Constant power applications

The output torque decreases as the speed increases. The torque required for acceleration is at most equal to the rated torque.



These applications involve a choice of motor-drives based on the following criteria: - Centrifugal machines: torque or power at the maximum operating speed.

- Applications with constant torque: range of operating speeds and output torques.

- Applications with constant power: range of operating speeds and torque at the minimum operating speed.

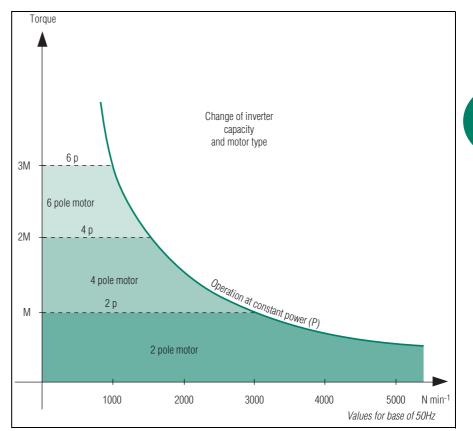
#### Choice of inverter/motor combination

The curve below expresses the output torque of a 2, 4 or 6 pole motor supplied by a drive with power P where  $F_1$  is 50 Hz (point at which U/f ratio changes).

For a frequency inverter with power  $P_N$  operating at a constant power P within a determined range of speeds, it is possible to optimize the choice of the motor and its number of poles to give a maximum amount of torque.

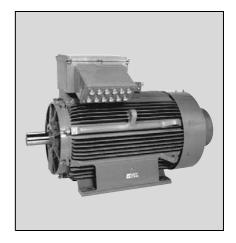
*Example 1:* the UMV - 3.5 T inverter (drive) can supply the following motors: FLS 90 L - 2 p - 2.2 kW - 7.5 N.m FLS 100 LK - 4 p - 2.2 kW - 15 N.m

FLS 112 M - 6 p - 2.2 kW - 22.5 N.m











# D5 - Speed of rotation

# Extreme operating conditions and other points

#### **Transient overloads**

Drives are designed to withstand transient overload peaks of 180% or overloads of 150% for 60 seconds (maximum once every ten minutes). If the overload is greater, the system will automatically shut down.

#### Starting torque and current

The specific U/f ratio (with Boost for frequencies lower than 25 Hz) means that the torque available when the motor is switched on can be adjusted to a value higher than the rated value.

#### Adjusting the switching frequency

This optimizes motor noise levels by adapting the wave form to the specific type of use.

#### **Electrical protection**

The system all have integrated features to protect them against:

- overload (over-current)
- under-voltage and over-voltage
- short-circuit
- earth fault

*Note:* All the above faults are shown on an LCD screen, as are settings, speed and current ranges, etc.

## Mechanical speed limits for standard motors when the frequency is varied

With increasingly extensive frequency ranges, frequency inverters can, in theory, control a motor at a higher speed than its rated speed. However, the bearings and type of balancing of the standard rotor dictate a maximum mechanical speed which cannot be exceeded without endangering the service life of the motor.

The table opposite shows this critical speed for standard horizontal and vertical motors (for the 315 M and above, consult us for the vertical position).

Above these limits, please consult Leroy -Somer.

These speed limit values are given for motors coupled directly to the load (with no radial load).

The formula for calculating the greasing interval I'g at frequency f' is on average:

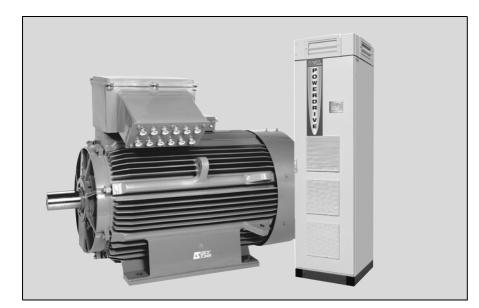
$$I'g = \frac{25 \times Ig}{f'}$$

 $I_{\alpha}$  = greasing interval

(as indicated in section C3.4.2.2)

Туре	2 poles	4 poles	6 poles
FLS 80	13000	13000	13000
FLS 90	10000	10000	10000
FLS 100	9000	9000	9000
FLS 112	9000	9000	9000
FLS 132	8000	8000	8000
FLS 160	5000	5000	5000
FLS 180	5000	5000	5000
FLS 200	4000	4000	4000
FLS 225 ST/MT	4000	4000	-
FLS 225 M	3600	3600	3600
FLS 250	3600	3600	3600
FLS 280	3600	3000	3000
FLS 315 ST	3600	3000	3000
FLS 315 M/L	3600	2500	2500
FLS 355 L	3600	2000	2000
FLS 355 LK	-	1800	1800
FLS 400	-	1800	1800
FLS 400 LK	-	1800	1800
FLS 450	-	1800	1800

For 2-pole motors rated above 110 kW at 60 Hz, refer to section D2.2.3, page 60.



#### Choice of motor

There are two possibilities:

#### a - The frequency inverter is not supplied by LEROY-SOMER

All the motors in this catalogue can be used with a frequency inverter. Depending on the application, motors will need to be derated by around 10% to maintain all the characteristics described in this catalogue.

To avoid changes in frame size due to derating within the standard range, LEROY-SOMER has developed a range of adapted motors with standardized dimensions. What is more, the improved efficiency of this range means that the motors can be used with an electronic drive without derating.

## b - The frequency inverter is supplied by LEROY-SOMER

LEROY-SOMER has developed a range of optimized motors together with a range of frequency inverters.

As these two ranges have been specifically designed for use in combination, excellent performance is guaranteed.

There is a special catalogue devoted to this product line.



### D6 - Noise and vibration

#### D6.1 - MOTOR NOISE LEVELS D6.1.1 - Noise emitted by rotating machines

In a compressible medium, the mechanical vibrations of an elastic body create pressure waves which are characterized by their amplitude and frequency. The pressure waves constitute an audible noise if they have a frequency of between 16 and 16000 Hz.

Noise is measured by a microphone linked to a frequency analyser. Measurements are taken in an anechoic chamber on machines at no-load, and a sound pressure level Lp or a sound power level Lw can then be established. Measurement can also be carried out in situ on machines which may be on-load, using an acoustic intensity meter which can differentiate between sound sources and identify the sound emissions from the machine.

The concept of noise is linked to hearing. The auditory sensation is determined by integrating weighted frequency components with isosonic curves (giving a sensation of constant sound level) according to their intensity. The weighting is carried out on sound meters using filters whose bandwidth takes into account, to a certain extent, the physiology of the human ear:

**Filter A:** used for low and medium noise levels. High attenuation, narrow bandwidth. **Filter B:** used for very high noise levels. Wide bandwidth.

**Filter C:** very low attenuation over the whole of the audible frequency range.

Filter A is used most frequently for sound levels emitted by rotating machinery. It is this filter which has been used to establish the standardized characteristics. A few basic definitions:

The unit of reference is the bel, and the sub-multiple decibel dB is used here.

Sound pressure level in dB

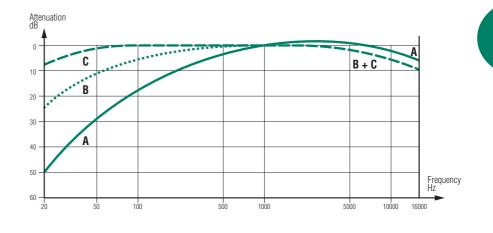
$$L_p = 20 \log_{10} \left( \frac{P}{P_0} \right)$$
 where  $p_0 = 2.10^{-5} Pa$ 

Sound power level in dB

 $L_{W} = 10 \log_{10} \left( \frac{P}{P_{o}} \right)$  where  $p_{0} = 10^{-12} W$ 

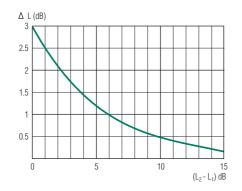
#### Sound intensity level in dB

 $L_{W} = 10 \log_{10} \left( \frac{I}{I_{o}} \right)$  where  $I_{0} = 10^{-12} \text{ W/m}^{2}$ 



#### **Correction of measurements**

For differences of less than 10 dB between 2 sound sources or where there is background noise, corrections can be made by addition or subtraction using the rules below.

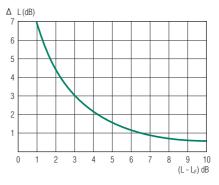


#### Addition of levels

If L<sub>1</sub> and L<sub>2</sub> are the separately measured levels (L<sub>2</sub>  $\ge$  L<sub>1</sub>), the resulting sound level L<sub>R</sub> will be obtained by the formula: L<sub>B</sub> = L<sub>2</sub> +  $\Delta$ L

 $L_{\rm R} = L_2 + \Delta L$ 

 $\Delta L$  is found by using the curve above  $\clubsuit$ 



#### Subtraction of levels\*

This is most commonly used to eliminate background noise from measurements taken in a "noisy" environment.

If L is the measured level and  $L_F$  the background noise level, the actual sound level  $L_R$  will be obtained by the calculation:

$$L_R = L - \Delta L$$
  
is found by using the curve above  $\blacktriangle$ 

\*This method is the one normally used for measuring sound power and pressure levels. It is also an integral part of sound intensity measurement.



ΛL

### D6 - Noise and vibration

Under IEC 60034-9, the guaranteed values are given for a machine operating at no-load under normal supply conditions (IEC 60034-1), in the actual operating position, or sometimes in the

direction of rotation as specified in the design. This being the case, standardized sound

power level limits are shown for the values

obtained for the machines described in this

catalogue. (Measurements were taken in conformity with standard ISO 1680).

#### Weighted sound level [dB(A)] of motors (with a 50 Hz supply) in position IM 1001

Expressed as sound power level (Lw) according to the standard, the level of sound is also shown as sound pressure level (Lp) in the table below:

		2 poles	3		4 poles	;		6 pole	6		8 poles	5
Motor type	IEC 60034-9	FLS	FLS	IEC 60034-9	FLS	FLS	IEC 60034-9	FLS	FLS	IEC 60034-9	FLS	FLS
	Power L	νA	Pressure LpA	Power Lv	vA	Pressure LpA	Power L	νA	Pressure LpA	Power L	vA	Pressure LpA
FLS 80 L	81	67	68	-	53	44	-	49	40	-	49	40
FLS 90 S	81	73	64	71	59	50	-	54	45	-	54	45
FLS 90 L	81	73	64	71	59	50	71	54	45	-	54	45
FLS 100 LK	86	75	66	76	61	52	71	57	48	71	51	46
FLS 112 M/MR	86	78	69	76	61	52	71	57	48	71	58	49
FLS 132 S	91	81	72	76	68	59	76	64	55	71	63	54
FLS 132 M	91	81	72	81	68	59	76	64	55	76	63	54
FLS 160 M	91	84	74	81	73	63	80	66	56	76	66	56
FLS 160 L	94	84	74	88	73	63	80	66	56	80	66	56
FLS 180 MR	96	85	75	88	73	63	-	-	-	-	-	-
FLS 180 L	-	-	-	88	75	64	84	74	63	80	72	62
FLS 200 L	96	86	76	91	76	66	84	76	65	84	73	62
FLS 225 ST	-	-	-	91	79	66	-	-	-	84	75	62
FLS 225 M/MT	98	87	76	94	79	68	87	83	72	84	76	65
FLS 250 M	98	88	77	94	79	68	87	83	72	89	76	66
FLS 280 S	100	88	77	97	79	68	90	83	72	89	76	65
FLS 280 M	100	88	77	97	79	68	90	83	72	89	76	65
FLS 315 ST	100	89	77	97	82	70	94	87	75	89	86	75
FLS 315 M/LA	103	96	84	101	85	73	94	88	78	92	90	78
FLS 315 LB	103	96	84	101	85	73	98	88	78	92	90	78
FLS 355 LA/LB/LC	107	96	84	105	92	80	98	90	78	92	90	78
FLS 355 LD	107	96	84	105	92	80	101	90	78	92	90	78
FLS 355 LKA	-	-	-	-	-	-	-	-	-	98	90	78
FLS 355 LKB	-	-	-	105	94	82	101	90	78	98	90	78
FLS 400 LA/LB	-	-	-	105	94	82	101	90	78	98	90	78
FLS 400 LVB	-	-	-	108	97	85	-	-	-	-	-	-
FLS 400 LKA/LKB	-	-	-	-	-	-	105	93	80	98	90	78
FLS 450 LA/LB	-	-	-	108	95	82	105	93	80	98	90	78
FLS 450 LVA/LVB	-	-	-	111	97	85	-	-	-	-	-	-

The maximum tolerance for these values is + 3 dB(A).

In compliance with standards IEC 60034-9 and NFEN ISO 4871, uncertainty on machine installations is established using the formula:

 $L_p = L + k$ 

where 1.5 < k < 6 dB depending on whether laboratory or control measurements are being used.

## D6.1.2 - Noise levels for machines at full load

Sound power levels, when at full load, are usually higher than those when at no-load. The maximum increase at full load to be

added to the declared values at no-load is between 2 and 8 dB(A). (Addition to standard IEC 60034.9).



D6 - Noise and vibrations

**TS** The FLS machines in this catalogue have level A in standard configuration

#### D6.2 - VIBRATION LEVELS -BALANCING

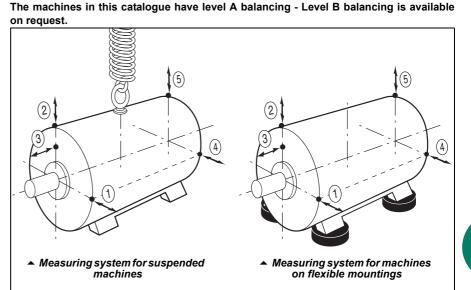
Inaccuracies due to construction (magnetic, mechanical and air-flow) lead to sinusoidal (or pseudo sinusoidal) vibrations over a wide range of frequencies. Other sources of vibration can also affect motor operation: such as poor mounting, incorrect drive coupling, end shield misalignment, etc.

We shall first of all look at the vibrations emitted at the operating frequency, corresponding to an unbalanced load whose amplitude swamps all other frequencies and on which the dynamic balancing of the mass in rotation has a decisive effect.

Under standard ISO 8821, rotating machines can be balanced with or without a key or with a half-key on the shaft extension.

Standard ISO 8821 requires the balancing method to be marked on the shaft extension as follows:

- half-key balancing: letter H
- full key balancing: letter F
- no-key balancing: letter N



The measurement points quoted in the standards are the ones indicated in the drawings above.

At each point, the results should be lower than those given in the tables below for each balancing class and only the highest value is to be taken as the "vibration level".

#### **Measured parameters**

The vibration speed can be chosen as the variable to be measured. This is the speed at which the machine moves either side of its static position. It is measured in mm/s.

As the vibratory movements are complex and non-harmonic, it is the quadratic average (rms value) of the speed of vibration which is used to express the vibration level.

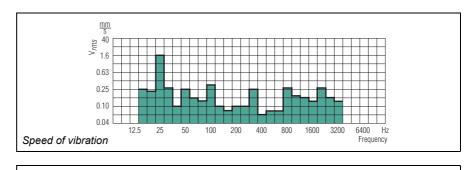
Other variables that could also be measured are the vibratory displacement amplitude (in  $\mu$ m) or vibratory acceleration (in m/s<sup>2</sup>).

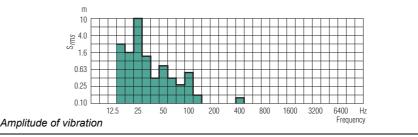
If the vibratory displacement is measured against frequency, the measured value decreases with the frequency: high-frequency vibrations are not taken into account.

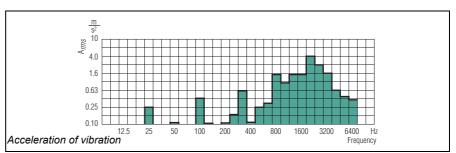
If the vibratory acceleration is measured, the measured value increases with the frequency: low-frequency vibrations (unbalanced loads) cannot be measured.

The rms speed of vibration is the variable chosen by the standards.

However, if preferred, the table of vibration amplitudes may still be used (for measuring sinusoidal and similar vibrations).









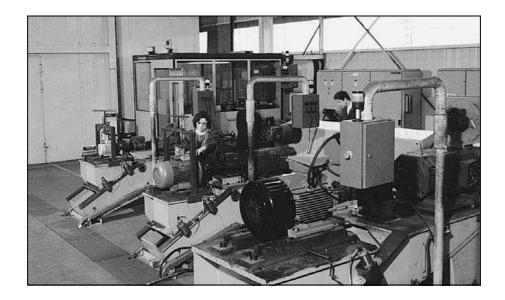
## D6 - Noise and vibration

MAXIMUM VIBRATION MAGNITUDE LIMITS, FOR DISPLACEMENT, SPEED AND ACCELERATION IN RMS VALUES FOR FRAME SIZE H (IEC 60034-14)

	Frame size <i>H</i> (mm)								
Vibration level	56 < <i>H</i> ≤ 132			132 < <i>H</i> ≤ 280			H > 280		
	Displa- cement µm	Speed mm/s	Accelera- tion m/s <sup>2</sup>	Displa- cement µm	Speed mm/s	Accelera- tion m/s <sup>2</sup>	Displa- cement µm	Speed mm/s	Accelera- tion m/s <sup>2</sup>
Α	25	1.6	2.5	35	2.2	3.5	45	2.8	4.4
В	11	0.7	1.1	18	1.1	1.7	29	1.8	2.8

F F s

For large machines and special requirements with regard to vibration, balancing can be carried out *in situ* (finished assembly). Prior consultation is essential, as the machine dimensions may be modified by the addition to the drive ends of the balancing disks required in this situation.





#### **D7.1 - THERMAL PROTECTION**

Motors are protected by a manual or automatic overcurrent relay, placed between the isolating switch and the motor. This relay may in turn be protected by fuses. These protection devices provide total protection of the motor against non-transient overloads. If a shorter reaction time is required, or if you want to detect transient overloads, or to monitor temperature rises at "hot spots" in the motor or at strategic points in the installation for maintenance purposes,

**D7** - Performance

it would be advisable to install heat sensors placed at sensitive points. The various types are shown in the table below, with a description of each. It must be emphasized that sensors cannot be used to carry out direct adjustments to the motor operating cycles.

#### Built-in indirect thermal protection

Туре	Symbol	Operating principle	Operating curve	Cut-off (A)	Protection provided	Number of devices
Normally closed thermostat (closed when de-energized)	РТО	bimetallic strip, indirectly heated, with normally closed (NC) contact		2.5 A at 250 V with cos φ 0.4	general surveillance for non-transient overloads	2 or 3 in series
Normally open thermostat (open when de-energized)	PTF	bimetallic strip, indirectly heated, with normally open (NO) contact		2.5 A at 250 V with cos φ 0.4	general surveillance for non-transient overloads	2 or 3 in parallel
Positive temperature coefficient thermistor	PTC	Variable non-linear resistor with indirect heating		0	general surveillance for transient overloads	3 in series
Thermocouples	T (T < 150 °C) Copper Constantan K (T < 1000 °C) Copper Copper-Nickel	Peltier effect		0	continuous surveillance at hot spots	1 per hot spot
Platinum resistance thermometer	PT 100	Variable linear resistor with indirect heating	R	0	high accuracy continuous surveillance at key hot spots	1 per hot spot

- NRT: nominal running temperature

- The NRTs are chosen according to the position of the sensor in the motor and the temperature rise class.

#### Fitting thermal protection

- PTO or PTF, in the control circuits

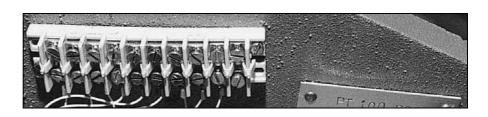
- PTC, with relay, in the control circuits - PT 100 or thermocouples, with reading equipment or recorder, in the control board of the installation for continuous surveillance.

#### Alarm and early warning

All protective equipment may be backed up by another type of protection (with different NRTs). The first device will then act as an "early warning" (light or sound signals given without shutting down the power circuits), and the second device will be the actual alarm (shutting down the power circuits).

#### Built-in direct thermal protection

For low rated currents, bimetallic strip-type protection may be used. The line current passes through the strip, which shuts down or restores the supply circuit as necessary. The design of this type of protection allows for manual or automatic reset.





### D7 - Performance

## D7.2 - POWER FACTOR (COS $\boldsymbol{\phi}$ ) CORRECTION

To help improve current supply in the power lines, electricity supply distributors now ask their customers to have loads with a power factor ( $\cos \phi$ ) as near as possible to 1 or at least higher than 0.93.

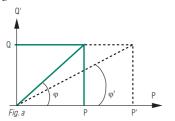
To create the magnetic field, induction motors absorb reactive power (Q) and introduce a power factor which may be quite different from the one recommended by electricity supply distributors.

There are, however, several ways of correcting the power factor:

#### a/ by changing the active power

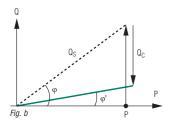
- increase active energy consumption (space heaters, lighting, etc)

- use synchronous machines (cos  $\phi$  = 1). Fig. a



#### b/ by changing the reactive power

- provide capacitive reactive compensation for the generally inductive reactive drop in the installation (power lines and induction motors). *Fig. b* 



The need for power factor correction is not linked to faults in design or manufacture. Instead of the two procedures outlined above, it may be easier to use the chart opposite to calculate the compensating reactive power.

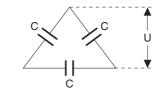
### Calculating the reactive power compensation

$$Q = \frac{Pu}{\eta}(tg\phi - tg\phi')$$

where Pu active output power n motor efficiency

tg  $\phi$  and tg  $\phi'$  phase angle error before and after connection

#### Connection of capacitors



The capacitor values are given by the following formula (in three-phase):

 $\mathsf{Q}=\mathsf{U}^2\,\mathsf{C}\omega\bullet\sqrt{3}$ 

U voltage of the mains with an angular velocity of the phases:

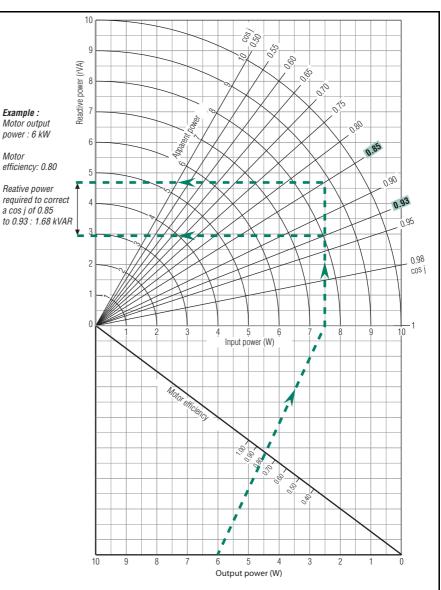
 $\omega \; (\; \omega = 2 \; \pi \bullet f)$ 

#### **IMPORTANT:**

The use of capacitors on motor terminals can cause certain problems:

- in hypersynchronous braking, the motor operates as a self-excited generator and high peak voltages will occur across the mains connected terminals

- in the event of micro-cuts, reactive energy is released which will excite the motor. When the supply is restored, high transient voltages may occur.



For increased accuracy when using the chart, multiply the horizontal scale and the vertical scale by the same factor. The result should be divided by the same factor.

 Chart for finding the reactive power required for power factor improvement.



### D7 - Performance

## D7.3 - MOTORS OPERATING IN PARALLEL

### Motors connected to the same mechanical shaft

A mechanical shaft can be operated by two or more separate motors:

a) If the motors are of the same type, the total power consumption on the line is equally distributed between the motors (to within the different slip variations).

b) If the motors are of different types, the power is distributed according to the steady speed of the whole unit. So, a small motor with high slip, placed on the same line as a large motor with minimal slip, will run at more or less the same speed as the large motor and therefore only provide a small proportion of the rated power.

# Motors coupled to independent shafts which must rotate at the same speed:

#### electrical shaft

To avoid deformation problems in large machines (gantry cranes, for example), separately sited mechanical shafts have to be synchronized to rotate at the same speed, whatever their loads.

We can then draw the follow diagram, called an electrical shaft:

 $1 - \bigoplus_{M1} - \bigoplus_{S1} 2 - \bigoplus_{S2} - \bigoplus_{M2}$ 

1 - 2 : mechanical shafts to be synchronized

*M1 - M2: drive motors, normally cage induction motors, providing the average torque on each line.* 

S1 - S2: synchronizing slipring motors, coupled to the drive motors M1 and M2, whose rotor circuits are linked phase-tophase. These motors have the dimensions required for providing the synchronization power defined in the application specification.

Note: There is a simplified version of this diagram, in which motors M1 and M2 are absent and motors S1 and S2 carry out both functions. In this case both rotors output into a single rheostat for minimum slip operation, which will enable any desynchronization (out-of-step) to be detected and the necessary speed compensation to be made.

For a given power, machine dimensions will have to be large enough to be able to supply sufficient motor and synchronization torque, and minimize losses due to rotor slip.

#### Motors in parallel on the same supply controlled by a single switch Example: drying tunnel with several fans.

As manufacturing inaccuracies in the

windings can occur, it is best to check the order of the motor and line phases before starting, and not to use motors with different internal connections so as to avoid circulating currents which might destroy complete installations.

All equipotential neutral connections must be excluded.





### D8 - Starting methods for cage induction motors

The two essential parameters for starting cage induction motors are:

- starting torque
- starting current

These two parameters and the resistive torque determine the starting time.

These three characteristics arise from the construction of cage induction motors. Depending on the driven load, it may be necessary to adjust these values to avoid torque impulse on the load or current surges in the supply. There are essentially five different types of supply, which are:

- D.O.L. starting
- star/delta starting
- soft starting with auto-transformer
- soft starting with resistors
- electronic starting

The tables on the next few pages give the electrical outline diagrams, the effect on the characteristic curves, and a comparison of the respective advantages of each mode.

## D8.1 - MOTORS WITH ASSOCIATED ELECTRONICS

"Electronic" starting modes control the voltage at the motor terminals throughout the entire starting phase, giving very gradual smooth starting:

#### "Unistart" electronic soft starter

This electronic starter enables three-phase induction motors to be started smoothly by controlling their acceleration.

#### Characteristics:

- P < 2.2 kW 380V-415V 50/60 Hz
- P < 1.5 kW 230V 50/60 Hz
- Ramp from 0.5 to 10 s
- Starting torque adjustable from 0 to 100%.

#### • "Digistart" electronic soft starter

- 10 models from 9 to 500 kW
- Supply: 220 to 690 V 50/60 Hz

#### - Advantages:

- Protects both itself and the motor over the whole power range.
- Can be used on all motors without derating
- Fault signalling
- Simple digital programming
- · Keypad or remote control

#### Hyper control

Hyper Control is an electronic system which is placed between the multi-speed motor and the low-speed power supply contactor, and is used to manage torque when changing from one speed to another.

#### 6 power ratings

RATINGS	HC.1.22.400	HC.3.22.400	HC.4.8.9.400	
Low-speed motor power	0.06 to 3.9 kW			
Three-phase mains supply voltage		400 V +10% -10%		

RATINGS	HC.1.22.230	HC.3.22.230	HC.4.8.9.230	
Low-speed motor power	0.035 to 2.25 kW			
Three-phase mains supply voltage		230 V +10% -10%		

Mains frequency	50 / 60 Hz ±5%		
Protection	IP 20		
Housing in composite material			

#### D8.2 - VARIABLE SPEED MOTOR • Starting on variable speed drive

One of the advantages of variable speed drives is that loads can be started without a current surge on the mains supply, since starting is always performed with no voltage or frequency at the motor terminals.



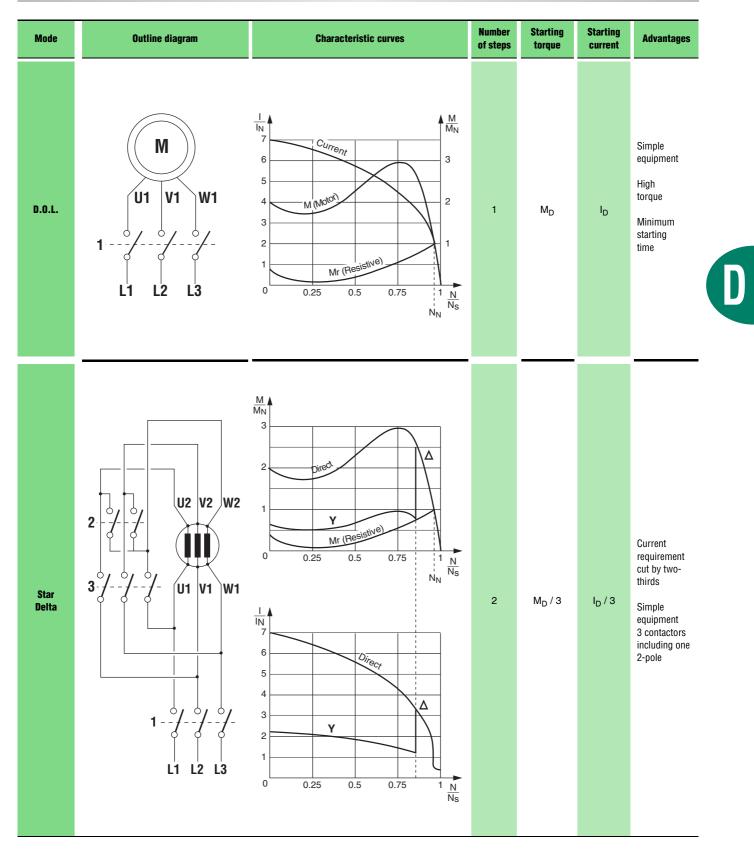
UNISTART



DIGISTART

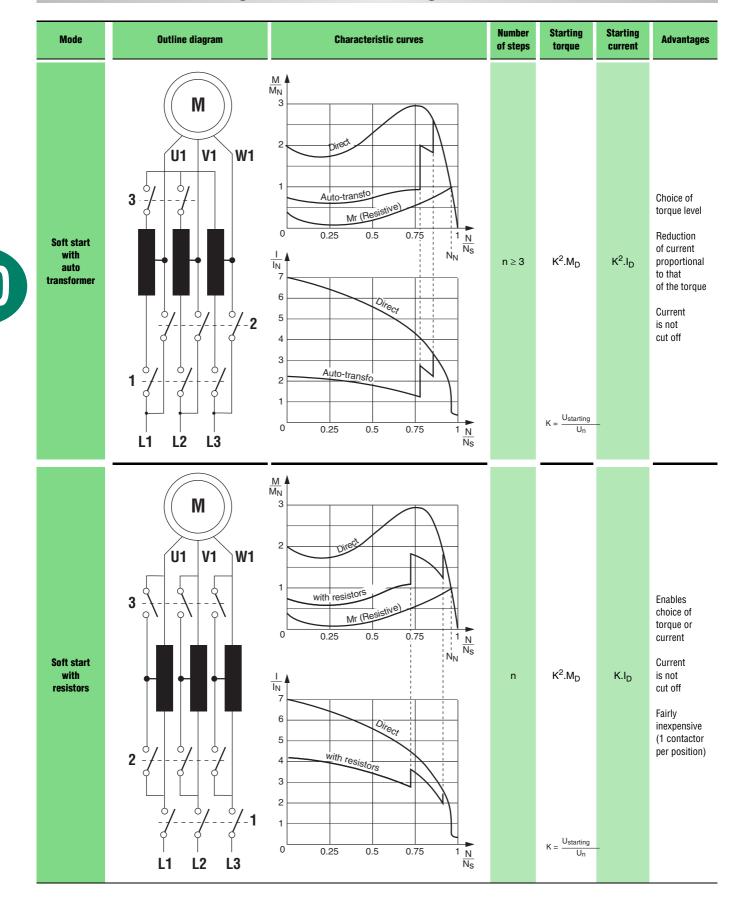


## D8 - Starting methods for cage induction motors



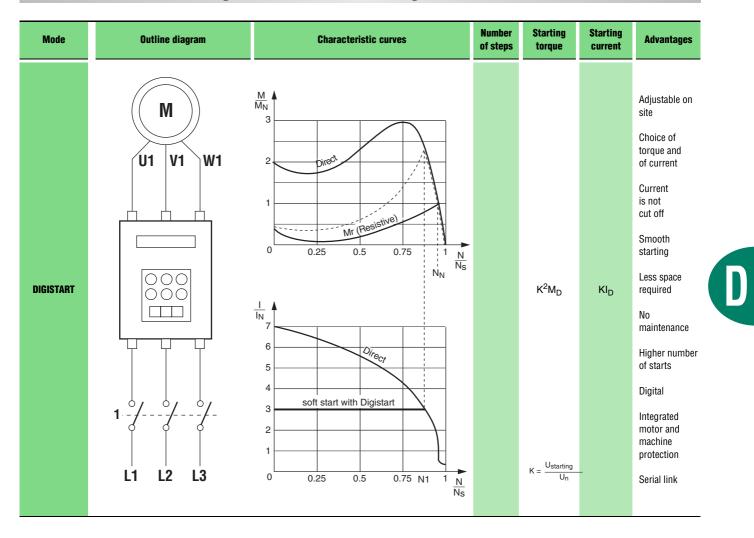


## D8 - Starting methods for cage induction motors





## D8 - Starting methods for cage induction motors





### D9 - Braking methods

#### **General information**

The braking torque is equal to the torque produced by the motor increased by the resistive torque of the driven machine.

$$C_f = C_m + C_r$$

C<sub>f</sub>= braking torque

 $C_m$ = motor torque  $C_r$ = resistive torque

Braking time, i.e. the time required for an induction motor to change from speed N to stop, is calculated by the formula:

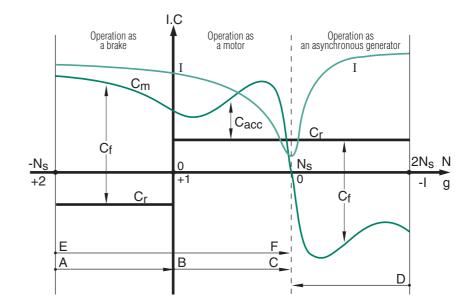
$$\mathbf{T_f} = \frac{\boldsymbol{\Pi} \cdot \mathbf{J} \cdot \mathbf{N}}{\mathbf{30} \cdot \mathbf{C_f}(\mathbf{av})}$$

T<sub>f</sub> (in s) = braking time

J (in kgm<sup>2</sup>) = moment of inertia

N (in min<sup>-1</sup>) = speed of rotation

 $C_{f}$  (av) (in N.m) = average braking torque during the time period



Curves I = f(N),  $C_m = f(N)$ ,  $C_r = f(N)$ , in the motor starting and braking zones.

I = current absorbed	g = slip
C = torque value	N <sub>s</sub> = synchronous speed
C <sub>f</sub> = braking torque	AB = reverse-current braking
C <sub>r</sub> = resistive torque	BC = starting, acceleration
C <sub>m</sub> = motor torque	DC = braking as asynchronous generator
N = speed of rotation	EF = <i>reverse</i>

#### **Reverse-current braking**

This method of braking is obtained by reversing two of the phases.

In general, an isolator disconnects the motor from the supply at the time the speed changes to N=0.

In cage induction motors, the average braking torque is generally greater than the starting torque.

Braking torque varies in different types of machine, as it depends on the rotor cage construction.

This method of braking involves a large amount of absorbed current, more or less constant and slightly higher than the starting current.

Thermal stresses during braking are three times higher than during acceleration.

Accurate calculations are required for repetitive braking.

Note: The direction of rotation of a motor is changed by reverse-current braking and restarting.

Thermically, one reversal is the equivalent of 4 starts. Care must therefore be taken when choosing a machine.

#### D.C. injection braking

Operating stability can be a problem when reverse-current braking is used, due to the flattening out of the braking torque curve in the speed interval  $(O, -N_S)$ .

There is no such problem with D.C. injection braking: this can be used on both cage induction and slipring motors.

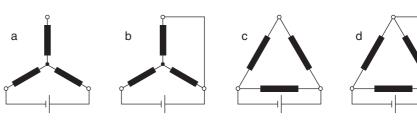
With this braking method, the induction motor is connected to the mains and braking occurs when the A.C. voltage is cut off and D.C. voltage is applied to the stator.

There are four different ways of connecting the windings up to direct current.

The D.C. applied to the stator is usually supplied by a rectifier plugged into the mains.

Thermal stresses are approximately three times lower than for reverse-current braking.

The shape of the braking torque curve in the speed interval  $(0, - N_S)$  is similar to that of the curve Cm = f (N) and is obtained by changing the abscissa variable to N<sub>f</sub> = N<sub>S</sub> - N.



Motor winding connections for direct current



D9 - Braking methods

The braking current is calculated using the formula:

$$\mathbf{I_f} = \mathbf{k1_i} \times \mathbf{I_d}_{\sqrt{\frac{\mathbf{C_f} - \mathbf{C_{fe}}}{\mathbf{k_2} \cdot \mathbf{Cd}}}}$$

The values of k1 for each of the four connections are:

k1 <sub>a</sub> = 1.225	k1 <sub>c</sub> = 2.12
k1 <sub>b</sub> = 1.41	k1 <sub>d</sub> = 2.45

The braking torque can be found by the formula:

$$\mathbf{C}_{\mathbf{f}} = \frac{\boldsymbol{\Pi} \cdot \mathbf{J} \cdot \mathbf{N}}{\mathbf{30} \cdot \mathbf{T}_{\mathbf{f}}}$$

In the formulae above:

l <sub>f</sub> (in A)	= direct current for braking
l <sub>d</sub> (in A)	= starting current in the phase
	= $\frac{1}{\sqrt{3}}$ I <sub>d</sub> given in catalogue (for $\Delta$ connection)
C <sub>f</sub> (in N.m)	= average braking torque in the interval (N <sub>s</sub> , N)
C <sub>fe</sub> (in N.m)	= external braking torque
$C_d$ (in N.m)	= starting torque
J (en kgm <sup>2</sup> )	= total moment of inertia on the drive shaft
N (in min <sup>-1</sup> )	= speed of rotation
T <sub>f</sub> (in s)	= braking time
k1 <sub>i</sub>	= numerical factors
	for connections a, b, c and d (see diagram)
k2	= numerical factors taking into account the average braking torque

The direct current to be applied to the windings is calculated by:

(k2 = 1.7)

 $U_{f} = k3_{i} \cdot k4 \cdot I_{f} \cdot R_{1}$ 

k3 values for the four diagrams are as follows:

- $k_{a}^{2} = 2$
- k3<sub>b</sub> = 1.5

 $k_{c}^{2} = 0.66$ 

- k3<sub>d</sub> = 0.5
- $U_f$  (in V) = voltage for braking

I<sub>f</sub> (in A) = direct current for braking

 $R_1$  (en Ω) = stator phase resistance at 20° C

- k3<sub>i</sub> = numerical factors for connections a, b, c and d (see diagrams)
- k4 = numerical factor taking into account the temperature rise of the motor (k4 = 1.3)

#### **Regenerative braking**

This is the braking method applied to multispeed motors when changing down to lower speeds. This procedure cannot be used to stop the motor.

Thermal stresses are approximately equal to those occurring when motors with Dahlander connections are started at the lower rated speed (speed ratio 1 : 2).

With the motor at the lower speed, working as a generator, it develops very high braking torque in the speed interval ( $2N_s$ ,  $N_s$ ).

The maximum braking torque is slightly higher than the starting torque of the motor at the lower speed.

#### **Mechanical braking**

Electromechanical brakes (D.C. or A.C field excitation) can be fitted at the rear of the motor.

For further details, see our "Brake motors" catalogue.



D



### D10 - Operation as an asynchronous generator

#### D10.1 - GENERAL

The motor operates as an asynchronous generator each time the load becomes a driving load and the rotor speed exceeds the synchronous speed ( $N_s$ ).

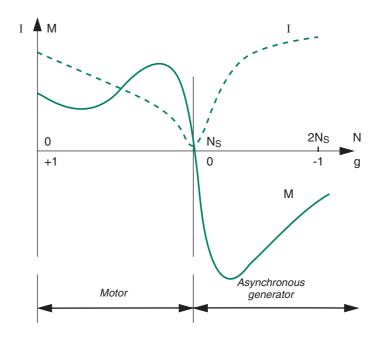
This can be induced either voluntarily, as in the case of electric power stations (water or wind power, etc) or involuntarily, caused by factors linked to the application (downward movement of crane hooks or blocks, inclined conveyors, etc).

#### D10.2 - OPERATING CHARACTERISTICS

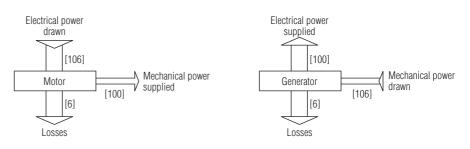
The diagram opposite shows the various operations of an asynchronous machine in relation to its slip (g) or its speed (N).

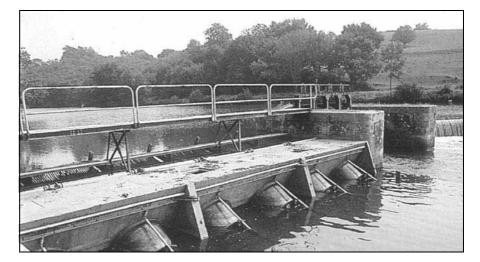
**Example:** let us consider an induction motor of 45 kW, 4 poles, 50 Hz at 400V. As a rough estimate, its characteristics as an asynchronous generator can be deduced from its rated characteristics as a motor, by applying the rules of symmetry. If more precise values are required, the manufacturer should be consulted.

In practice, it can be checked that the same machine, operating as a motor and as a generator with the same slip, has approximately the same losses in both cases, and therefore virtually the same efficiency. It can be deduced from this that the rated electrical power supplied by the asynchronous generator will be virtually the same as the motor output power.



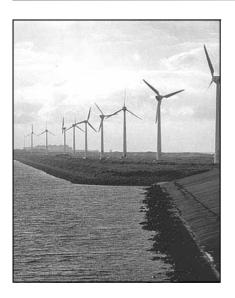
Characteristics	Motor	GA
Synchronous speed (min <sup>-1</sup> )	1500	1500
Rated speed (min <sup>-1</sup> )	1465	1535
Rated torque (m.N)	+ 287	- 287
Rated current at 400V (A)	87 A (absorbed)	87 A (supplied)







#### D10 - Operation as an asynchronous generator



## D10.3 - CONNECTION TO A POWERFUL MAINS SUPPLY

It is assumed that the machine stator is connected to a powerful electrical mains supply (usually the national grid), ie. a mains supply provided by a generator which regulates the power to at least twice that of the asynchronous generator.

Under these conditions, the mains supply imposes its own voltage and frequency on the asynchronous generator. Furthermore, it supplies it automatically with the reactive energy necessary for all its operating conditions.

#### D10.3.1 - Connection -Disconnection

Before connecting the asynchronous generator to the mains supply, it is necessary to ensure that the direction of phase rotation of the asynchronous generator and the mains supply are in the same order.

• To connect an asynchronous generator to the mains supply, it should be accelerated gradually until it reaches its synchronous speed Ns. At this speed, the machine torque is zero and the current is minimal.

This is an important advantage of asynchronous generators: as the rotor is not polarised until the stator is powered up, it is not necessary to synchronise the mains supply and the machine when they are connected. However, there is a phenomenon affecting the connection of asynchronous generators which, in some cases, can be a nuisance: the rotor of the asynchronous generator, although not energized, still has some residual magnetism.

On connection, when the magnetic flux created by the mains supply and that caused by the residual magnetism of the rotor are not in phase, the stator experiences a very brief current peak (one or two half-waves), combined with an instantaneous overtorque of the same duration.

It is advisable to use connecting stator resistances to limit this phenomenon.

• Disconnecting the asynchronous generator from the mains supply does not pose any particular problem.

As soon as the machine is disconnected, it becomes electrically inert since it is no longer energized by the mains supply. It no longer brakes the driving machine, which should therefore be stopped to avoid reaching overspeed.

### D10.3.1.1 - Reactive power compensation

To limit the current in the lines and the transformer, the asynchronous generator can be compensated by restoring the power factor of the installation to the unit, using a bank of capacitors.

In this case, the capacitors are only inserted at the terminals of the asynchronous generator once it has been connected, to avoid self-energization of the machine due to the residual magnetism during speed pick-up. For a 3-phase low voltage asynchronous generator, 3-phase or singlephase capacitors in delta connection are used.

### D10.3.1.2 - Electrical protection and safety

There are two protection and safety categories:

- those which relate to the mains

- those which relate to the set and its generator

The major mains protection devices monitor:

- maximum-minimum voltage

- maximum-minimum frequency

- minimum power or energy feedback (operating as a motor)

- generator connection fault
- The protection devices for the set are:
- stop on detection of racing start
- lubrication faults

- thermal magnetic protection of the generator, usually with probes in the winding.

## D10.4 - POWER SUPPLY FOR AN ISOLATED NETWORK

This concerns the supply of a consuming network which does not have another generator of sufficient power to impose its voltage and frequency on the asynchronous generator.

## D10.4.1 - Reactive power compensation

In the most common case, reactive energy must be supplied:

- to the asynchronous generator
- to the user loads which consume it

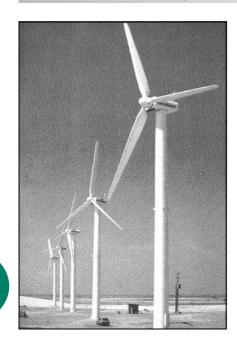
To supply both of these consumption types with reactive energy, use a reactive energy source of suitable power connected in parallel on the circuit. This is usually a bank of capacitors with one or more stages which may be fixed, manually adjusted (using notches) or automatically adjusted. Synchronous capacitors are now rarely used.

**Example:** in an isolated network with power consumption of 50 kW where  $\cos \phi = 0.9$  (and  $\tan \phi = 0.49$ ), supplied by an asynchronous generator with  $\cos \phi$  of 0.8 at 50 kW (and  $\tan \phi = 0.75$ ), it is necessary to use a bank of capacitors which supplies:

(50 x 0.49) + (50 x 0.75) = 62 kvar



#### D10 - Operation as an asynchronous generator



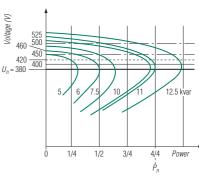
#### D10.4.2 - Characteristic curves

At rated frequency, an asynchronous generator supplies a voltage which depends on the active power supplied and the value of the energization capacitors.

For each asynchronous generator, it is possible to plot a network of curves such as those shown below.

In conclusion, to maintain a constant voltage, the reactive power must be adapted to the active power required.

Adjusting the load and the capacitors does not present any special difficulties. The table below shows how these parameters should be modified.



Example of a13 kW and 6-pole machine

#### Direction of adjustment for load and capacitors

Prot	olem	Action
Frequency	Voltage	Action
Too high	Too high	Increase the active load or reduce the speed or mechanical power
Too high	Too low	Increase the capacitor bank capacity
Too low	Too high	Decrease the capacitor bank capacity
Too low	Too low	Reduce the active load or increase the speed

#### D10.4.3 - Regulation

When the power consumed by the user or the power supplied by the driving machine vary but the frequency and voltage are to be maintained within narrow limits, a regulation device must be provided. This device is designed to maintain the correct electrical characteristics by adjusting one or more parameters:

- active power supplied (driving machine)

- active power consumed (loads on the circuit in use)

- reactive power supplied (usually capacitors).

#### D10.4.4 - Control and protection

The installation comprises an electrical measuring, control and protection enclosure.

The only special devices are:

- time delay on connection of the load circuit to avoid de-energization of the machine on starting

- control of the energization capacitors, manually or automatically as required

The rest of the electrical equipment is completely standard.

#### D10.5 - PERFORMANCE OF MOTORS USED AS AG

- Preference should be given to 4 - 6 or 8pole versions for power ratings above 5.5 kW depending on the speeds of the driven machines.

- For small generators (P  $\leq$  4 kW), the most common application uses 2 poles.

- For standard motors, the no-load voltages of asynchronous generators are very high and the voltage drop for the rated power is around 15% (power ratings below the rated power should not be used).

- Remember that asynchronous generators consume the reactive power required for their energization and supply active power to the mains (isolated or non-isolated) and that the reactive power of the loads should be compensated.



## E1 - Selection data: single-speed

2 poles - 3000 min <sup>-1</sup>	90 - 91
4 poles - 1500 min <sup>-1</sup>	92 - 93
6 poles - 1000 min <sup>-1</sup>	94 - 95
8 poles - 750 min <sup>-1</sup>	96 - 97

### E2 - Selection data: two-speed

Centrifugal applications	98
General applications	99



For dimensions, see section **F** page 99



### E1 - Selection data: single-speed



```
IP 55
CI. F - ∆T 80 K
400 V
```

Can be used at 400 V  $\pm 10\%$  in the conditions defined on page 61



#### MAINS SUPPLY ${\rm \Delta}$ 230 / Y 400 V or ${\rm \Delta}$ 400 V $\qquad$ 50 Hz

at	Power at 50 Hz	Rated speed	Rated torque	Rated current	l	Power facto	or		Efficiency		I <sub>d</sub> ∕I <sub>n</sub>	C <sub>d</sub> ∕C <sub>n</sub>	C <sub>m</sub> ∕C <sub>n</sub>	Apparent power	Torque curve	Moment of inertia	Weight
Туре	kW	min <sup>-1</sup>	N.m	А	50 %	75 %	100 %	50 %	75 %	100 %				kVA	N°	kg.m <sup>2</sup>	kg
FLS 80 L	0.75	2840	2.5	1.6	0.76	0.80	0.86	73	77.4	76.9	5.9	2.4	2.2	1.1	1	0.0007	15
FLS 80 L	1.1	2837	3.7	2.4	0.65	0.77	0.84	76.6	78.5	79.5	5.6	2.7	2.4	1.6	6	0.0009	18
FLS 90 S	1.5	2870	5	3.3	0.64	0.75	0.81	79	81	82	7.3	3	3.1	2.3	5	0.0014	21
FLS 90 L	2.2	2862	7.5	4.3	0.71	0.82	0.88	82.5	84.2	84.5	8.1	3.7	3.5	3	5	0.0021	26
FLS 100 LK	3	2925	10	5.5	0.85	0.89	0.91	83	84	86	8.4	2.4	3	3.8	4	0.0069	42
FLS 112 M	4	2940	13.6	7.5	0.81	0.87	0.89	84	86	86.5	8.7	2.9	3.3	5.2	1	0.0084	48
FLS 132 S	5.5	2940	18.7	10.6	0.79	0.84	0.86	84	85.5	87	7.6	2.3	2.9	7.4	2	0.0168	67
FLS 132 S	7.5	2950	25	14.1	0.81	0.85	0.87	87	88	88	8.9	2.6	3.4	9.8	4	0.0236	70
FLS 160 MA	11	2935	35.8	20	0.82	0.86	0.88	85.3	87.3	88.4	8.6	2.8	3.2	14.1	2	0.037	97
FLS 160 MB	15	2935	48.8	27	0.82	0.86	0.88	87	89.1	89.7	8.6	2.8	3.2	19	2	0.043	108
FLS 160 L	18.5	2940	60	33	0.84	0.88	0.90	88.1	90.2	90.8	8.4	2.7	3.1	22.6	2	0.057	126
FLS 180 MR	22	2940	71	39	0.83	0.87	0.89	88.3	90.4	91	8.5	2.8	3.1	27.2	2	0.065	135
FLS 200 LA	30	2950	97	51	0.85	0.90	0.91	90.2	91.9	92.4	7.7	2.4	2.8	35.7	3	0.13	245
FLS 200 LB*	37	2959	120	63	0.84	0.89	0.9	91.3	93	93.5	8.3	3	3.4	44.4	8	0.16	265
FLS 225 MT*	45	2958	145	78	0.83	0.88	0.89	91.6	93.3	93.8	8.3	2.8	3.2	54	8	0.19	290
FLS 250 M*	55	2966	177	94	0.81	0.87	0.89	92.2	94	94.6	7.9	2.5	3.5	65	8	0.44	405
FLS 280 S*	75	2965	241	127	0.82	0.88	0.90	93	94.2	94.6	8	2.7	3.8	88	8	0.47	505
FLS 280 M*	90	2962	290	149	0.83	0.89	0.91	91.6	95.1	95.5	7.7	2.6	3.7	104	8	0.53	560
FLS 315 ST	110	2975	356	178	0.89	0.92	0.93	95	95.7	95.8	8.2	2.8	3.3	123	8	1.08	850
FLS 315 M	132	2962	427	221	0.86	0.89	0.90	93.8	95.4	96	7.5	1.8	2.7	153	9	1.71	1000
FLS 315 LA	160	2969	517	272	0.82	0.87	0.89	92.8	94.9	95.5	7.5	2	3	188	9	1.71	1050
FLS 315 LB	200	2967	647	342	0.81	0.86	0.88	93.9	95.4	96	7.7	2.3	3.4	237	8	1.99	1150
FLS 355 LA	250	2978	808	424	0.84	0.88	0.89	94	95.2	95.6	7.2	2.1	2.6	294	3	3.39	1400
FLS 355 LB	275	2980	881	464	0.84	0.88	0.89	95	96	96.2	8.4	2.3	2.9	322	10	3.39	1500
FLS 355 LB •	315	2976	1016	525	0.85	0.89	0.90	94.9	95.9	96.2	7.2	1.8	2.5	364	10	3.39	1500
FLS 355 LC	330	2980	1057	560	0.81	0.86	0.88	95.4	96.3	96.6	7.9	1.9	2.6	388	3	3.39	1915
FLS 355 LC	355	2979	1137	588	0.83	0.88	0.90	95.6	96.5	96.8	8.2	2.3	3.1	407	3	4.03	1915
FLS 355 LD •	400	2977	1284	673	0.82	0.87	0.89	95.2	96.1	96.4	7.8	2	2.7	466	3	4.03	1915

\* Motors (EFF1)

• Class F temperature rise

For power ratings above 400 kW, please consult Leroy-Somer.

\* Torque curve

section D4.4 - page 63

section D6.1 - page 71



## E1 - Selection data: single-speed

Voltage and f	requency	MAINS	S SUPPI	_Y 380 V	50 Hz	MAIN	S SUPP	LY 415 V	50 Hz			PPLY 4 om 440V to		60 Hz
	Power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	kW	min <sup>-1</sup>	A		%	min <sup>-1</sup>	A		%	kW	min <sup>-1</sup>	A		%
FLS 80 L	0.75	2802	1.8	0.85	74.5	2846	1.8	0.78	74.1	0.9	3420	1.8	0.83	76.3
FLS 80 L	1.1	2819	2.4	0.89	77.1	2859	2.4	0.84	75.5	1.3	3442	2.4	0.88	78.8
LS 90 S	1.5	2853	3.2	0.87	81	2885	3	0.82	84	1.8	3485	3.1	0.87	83
LS 90 L	2.2	2880	4.8	0.84	83	2904	4.6	0.81	82.5	2.7	3490	4.6	0.88	84.5
LS 100 LK	3	2910	5.8	0.93	84	2930	5.5	0.9	84	3.6	3510	5.8	0.92	84
FLS 112 M	4	2925	7.9	0.91	85	2945	7.5	0.88	84.5	4.8	3530	7.8	0.91	85
FLS 132 S	5.5	2930	10.9	0.9	85.5	2940	10.3	0.87	85.4	6.6	3525	10.9	0.90	84.6
LS 132 S	7.5	2935	14.2	0.92	87.5	2955	13.4	0.89	87.8	9	3530	14.2	0.91	87.4
FLS 160 MA	11	2929	21	0.89	88.2	2939	20	0.87	88.4	13.2	3535	21	0.88	88.1
LS 160 MB	15	2929	29	0.89	89.5	2939	27	0.87	89.7	18	3535	29	0.88	89.4
LS 160 L	18.5	2933	34	0.91	90.6	2944	32	0.89	90.8	22	3540	34	0.90	90.5
FLS 180 MR	22	2933	41	0.90	90.8	2944	38	0.88	91	25	3533	39	0.90	90.5
LS 200 LA	30	2946	54	0.92	92.3	2967	50	0.90	93	34.5	3546	51	0.92	92.1
FLS 200 LB	37	2955	65	0.92	93.6	2963	62	0.89	93.9	42.5	3555	62	0.92	93.4
FLS 225 MT	45	2946	81	0.9	93.7	2956	75	0.89	93.7	52	3546	78	0.90	93.5
FLS 250 M	55	2962	98	0.90	94.5	2970	91	0.89	94.6	63	3562	93	0.90	94.3
FLS 280 S	75	2966	134	0.90	94.5	2967	124	0.89	94.6	86	3566	127	0.90	94.3
FLS 280 M	90	2953	158	0.91	95.3	2967	146	0.90	95.5	103	3567	151	0.90	95.3
FLS 315 ST	110	2971	188	0.93	95.7	2976	172	0.93	95.7	126	3571	178	0.93	95.5
FLS 315 M	132	2957	230	0.91	96	2963	213	0.90	96	132	3557	190	0.91	95.8
LS 315 LA	160	2963	283	0.90	95.3	2972	265	0.88	95.3	160	3563	235	0.90	95.1
LS 315 LB	200	2956	358	0.89	95.3	2968	338	0.86	95.6	200	3556	297	0.89	95.1
LS 355 LA	250	2974	442	0.90	95.4	2978	409	0.89	95.5	250	3574	366	0.90	95.2
LS 355 LB	275	2973	482	0.90	96.3	2980	451	0.88	96.5	275	3576	400	0.90	96.2
LS 355 LB •	315	2970	552	0.90	96.3	2976	516	0.88	96.5	315	3571	462	0.89	96.1
LS 355 LC	330	2980	590	0.88	96.6	2980	561	0.85	96.2	330	3576	493	0.88	95.6
FLS 355 LC	355	2978	619	0.90	96.8	2983	589	0.87	96.4	355	3578	517	0.90	95.8
FLS 355 LD •	400	2976	709	0.89	96.3	2981	647	0.89	96.6	400	3576	598	0.88	95.5

• Class F temperature rise

For power ratings above 400 kW, please consult Leroy-Somer.



### E1 - Selection data: single-speed



IP 55 CI. F - ∆T 80 K 400 V

Can be used at 400 V  $\pm 10\%$  in the conditions defined on page 61



#### MAINS SUPPLY $\triangle$ 230 / Y 400 V or $\triangle$ 400 V 50 Hz

	Power at 50 Hz	Rated speed	Rated torque	Rated current		Power facto	r		Efficiency		I <sub>d</sub> / I <sub>n</sub>	C <sub>d</sub> / C <sub>n</sub>	C <sub>m</sub> ∕C <sub>n</sub>	Apparent power	Torque curve	Moment of inertia	Weight
Туре	kW	min <sup>-1</sup>	N.m	Α	50 %	75 %	100 %	50 %	75 %	100 %				kVA	N°	kg.m <sup>2</sup>	kg
FLS 80 L	0.55	1410	3.7	1.6	0.56	0.69	0.74	65	69.4	69.2	4.4	2.1	2.3	1.1	3	0.0013	15
FLS 80 L	0.75	1425	5	2	0.58	0.70	0.75	70	73	72.5	5.7	3	2.8	1.4	1	0.0024	17
FLS 90 S	1.1	1429	7.5	2.5	0.68	0.77	0.83	76	78.4	78	4.9	1.6	2	1.7	5	0.0026	19
FLS 90 L	1.5	1428	10	3.3	0.62	0.74	0.82	77	79.4	79.5	5.3	1.8	2.3	2.3	4	0.0032	21
FLS 90 L	1.8	1438	12.3	4	0.63	0.75	0.82	79	80.8	80.1	5.9	2.1	3.2	2.7	2	0.0037	23
FLS 100 LK	2.2	1457	15	4.6	0.67	0.77	0.83	82.2	84.4	83.8	6.3	1.9	2.4	3.2	3	0.0077	41
FLS 100 LK	3	1454	20	6.2	0.64	0.76	0.82	83.4	84.9	84.7	6.5	2.1	2.6	4.3	2	0.0094	44
FLS 112 M	4	1462	27.5	8.4	0.62	0.74	0.81	82.2	84.9	85.1	7.4	2.5	2.9	5.8	2	0.012	48
FLS 132 S	5.5	1467	37	10.9	0.66	0.78	0.84	86	87.1	87	8	2.7	3.7	7.7	1	0.0154	65
FLS 132 M	7.5	1450	50	14.3	0.75	0.82	0.87	85.5	87.2	87	7.3	1.9	2.9	10.5	2	0.0192	70
FLS 132 M	9	1449	61	16.8	0.72	0.84	0.88	86.5	88.4	87.7	7.6	2.8	2.9	11.6	2	0.023	75
FLS 160 M	11	1455	72.2	21	0.72	0.81	0.86	87	88.4	88.5	7.8	2.6	3.3	15	2	0.06	103
FLS 160 L	15	1455	98.5	28	0.72	0.81	0.86	88	89.4	89.5	7.8	2.6	3.3	20	2	0.079	120
FLS 180 MR	18.5	1465	120.5	35	0.72	0.81	0.86	88.5	89.9	90	7.8	2.6	3.3	24	2	0.095	135
FLS 180 L	22	1465	143	41	0.73	0.82	0.86	89.7	91.2	91.4	7.4	2.6	2.4	28	6	0.137	184
FLS 200 L	30	1471	195	56	0.73	0.82	0.85	91	92	91.9	6.5	2.5	2.3	39	6	0.24	260
FLS 225 ST*	37	1476	240	70	0.66	0.77	0.82	91.6	93.3	93.6	7	2.6	2.4	49	6	0.28	290
FLS 225 M*	45	1483	290	79	0.76	0.84	0.87	93.2	94.3	94.5	7	2.5	2.6	55	6	0.7	388
FLS 250 M*	55	1479	355	103	0.71	0.80	0.82	93.9	94	94.4	6	2.4	2.5	70	6	0.7	395
FLS 280 S*	75	1483	484	137	0.68	0.79	0.84	93	94.8	94.9	7.7	2.9	3	95	6	0.815	475
FLS 280 M*	90	1478	581	162	0.72	0.81	0.85	93.9	94.5	95	6.9	2.9	3.1	112	6	1.015	565
FLS 315 ST	110	1482	710	203	0.71	0.80	0.83	93.7	94.5	94.8	7.3	2.9	2.7	141	8	1.83	850
FLS 315 M	132	1489	850	249	0.68	0.77	0.81	92.7	94.3	95	8	2.8	2.6	172	8	2.91	1000
FLS 315 LA	160	1487	1032	299	0.67	0.75	0.81	95.4	95.8	95.6	7.6	2.1	2.4	198	3	3.4	1050
FLS 315 LB •	200	1486	1291	377	0.66	0.74	0.80	95.6	96	95.8	7.6	2.3	2.3	255	3	3.4	1150
FLS 355 LA •	250	1490	1611	428	0.71	0.82	0.88	94	95.4	95.9	7.5	1.8	2.3	296	9	6.2	1510
FLS 355 LB •	300	1490	1930	512	0.71	0.82	0.88	94.2	95.6	96.1	6.9	1.8	1.6	360	5	6.2	1550
FLS 355 LC	315	1492	2019	603	0.59	0.72	0.79	92.7	94.8	95.5	8.7	2.3	2.2	386	5	6.5	1800
FLS 355 LC •	355	1491	2279	653	0.65	0.76	0.82	93.9	95.3	95.8	8	2.1	1.9	429	5	6.5	1800
FLS 355 LD •	400	1491	2564	698	0.76	0.84	0.86	95.3	96	96.3	6.4	2.1	2.1	477	6	7.4	1930
FLS 400 LB	400	1491	2559	691	0.78	0.85	0.87	95.4	96.3	96.6	8	2	2.6	478	4	11.7	2350
FLS 355 LKB	450	1490	2880	767	0.79	0.86	0.88	95.5	96.4	96.7	7.6	1.8	2.3	532	4	11.7	2320
FLS 400 LB	450	1490	2880	767	0.79	0.86	0.88	95.5	96.4	96.7	7.6	1.8	2.3	532	4	11.7	2350
FLS 355 LKB	500	1490	3200	854	0.79	0.86	0.88	96	96.1	96.5	6.5	1.7	2.2	592	4	11.7	2320
FLS 400 LVB	500	1490	3200	864	0.77	0.84	0.87	96	96.1	96.5	6.5	1.7	2.2	599	4	11.7	2350
FLS 450 LA	500	1492	3200	864	0.77	0.84	0.87	96	96.1	96.5	8	1.6	2.2	599	5	21	3100
FLS 450 LVA	550	1491	3525	940	0.78	0.85	0.88	96	96.1	96.5	7.9	1.5	2.1	651	5	21	3100
FLS 450 LB	630	1493	4030	1089	0.77	0.84	0.87	96	96.1	96.5	8.2	1.5	2.1	754	5	24	3450
FLS 450 LVB	675	1491	4326	1164	0.77	0.84	0.87	96	96.3	96.7	8	1.4	1.9	807	5	24	3450

\* Motors (EFF1)

• Class F temperature rise

For power ratings above 675 kW, please consult Leroy-Somer.

\* Torque curve

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## E1 - Selection data: single-speed

Voltage and f	requency	MAIN	S SUPP	LY 380 V	50 Hz	MAIN	S SUPP	LY 415 V	50 Hz			PPLY 4 om 440V to		60 Hz
	Power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	kW	min <sup>-1</sup>	А		%	min <sup>-1</sup>	А		%	kW	min <sup>-1</sup>	A		%
FLS 80 L	0.55	1390	1.6	0.78	69	1415	1.6	0.70	68	0.66	1705	1.55	0.75	72
FLS 80 L	0.75	1415	2	0.78	72.6	1430	2.1	0.71	71.2	0.9	1730	2	0.75	74.4
FLS 90 S	1.1	1416	2.6	0.86	75.5	1437	2.5	0.81	77.2	1.3	1726	2.5	0.84	78.9
FLS 90 L	1.5	1417	3.4	0.86	77.9	1436	3.4	0.79	78.4	1.8	1722	3.3	0.84	80.4
FLS 90 L	1.8	1427	4.1	0.84	79.4	1443	4	0.78	80.1	2.2	1733	4.1	0.82	81
FLS 100 LK	2.2	1450	4.7	0.85	83.2	1462	4.5	0.81	83.9	2.6	1755	4.6	0.84	84.8
FLS 100 LK	3	1448	6.4	0.85	84.3	1460	6.2	0.80	84.7	3.6	1752	6.3	0.83	85.9
FLS 112 M	4	1455	8.5	0.84	85	1464	8.4	0.78	84.7	4.8	1753	8.4	0.83	86.1
FLS 132 S	5.5	1444	11.4	0.85	86.5	1455	11	0.81	86	6.6	1750	11.2	0.85	87
FLS 132 M	7.5	1445	15.8	0.85	85	1455	15	0.82	85	9	1750	15.5	0.85	87
FLS 132 M	9	1440	17.4	0.90	86.9	1455	16.6	0.88	87.9	11	1750	17	0.88	88.7
FLS 160 M	11	1447	21.6	0.88	88	1459	21	0.84	88.7	12.6	1747	20	0.88	87.8
FLS 160 L	15	1447	29.1	0.88	89	1459	28	0.84	89.7	17.2	1747	28	0.88	88.8
FLS 180 MR	18.5	1457	36.1	0.88	88.5	1469	34	0.84	90.2	21	1757	34	0.88	88.3
FLS 180 L	22	1460	41.7	0.88	91.1	1465	40	0.84	91.5	25	1760	39	0.88	90.9
FLS 200 L	30	1467	58	0.86	91.4	1472	55	0.83	91.6	34.5	1767	55	0.86	91.2
FLS 225 ST	37	1472	70	0.86	93.4	1477	69	0.80	93	42.4	1773	66	0.86	93.2
FLS 225 M	45	1478	82	0.88	94.2	1483	78	0.85	94.4	52	1783	82	0.85	94.2
FLS 250 M	55	1476	104	0.85	94.5	1481	103	0.79	94.2	63	1776	102	0.83	94.2
FLS 280 S	75	1480	140	0.86	94.8	1484	136	0.81	94.4	86	1780	133	0.86	94.5
FLS 280 M	90	1477	168	0.86	94.8	1481	160	0.83	94.8	103	1777	163	0.84	94.8
FLS 315 ST	110	1479	207	0.85	94.8	1487	194	0.83	95.1	125	1779	195	0.85	94.6
FLS 315 M	132	1487	254	0.83	95.1	1488	249	0.78	94.4	150	1787	239	0.83	94.9
FLS 315 LA	160	1486	299	0.85	95.9	1488	300	0.78	95.3	185	1786	294	0.83	95.3
FLS 315 LB	200	1487	372	0.85	96.1	1487	385	0.76	95.3	230	1787	365	0.83	95.3
FLS 355 LA	250	1489	440	0.90	95.9	1490	423	0.86	95.8	285	1789	425	0.88	95.8
FLS 355 LB	300	1488	527	0.90	96.1	1490	500	0.87	96	345	1788	513	0.88	96
FLS 355 LC	315	1491	602	0.83	95.9	1494	614	0.75	95.2	360	1791	586	0.81	95.2
FLS 355 LC	355	1490	661	0.85	96	1493	664	0.78	95.4	405	1790	642	0.83	95.4
FLS 355 LD	400	1488	718	0.88	96.3	1491	690	0.84	96.1	460	1788	707	0.85	96.1
FLS 400 LB	400	1400	707	0.89	96.6	1492	672	0.86	96.3	460	1790	681	0.88	96.3
FLS 355 LKB	400	1490	795	0.89	96.6	1492	748	0.87	96.2	515	1789	763	0.88	96.3
FLS 400 LB	450	1489	795	0.89	96.6	1491	748	0.87	96.2	515	1789	763	0.88	96.3
FLS 355 LKB	500	1489	892	0.89	96.8	1491	833	0.87	96.2	575	1789	860	0.87	96.5
FLS 400 LVB	500	1489	892	0.88	96.8	1491	833		96	575	1792	860	0.87	
						1491		0.87			1792			96.5
FLS 450 LA	500	1492	895	0.88	96.5		840	0.86	96.3	575		862	0.87	96.2
FLS 450 LVA	550	1491	973	0.89	96.5	1490	913	0.87	96.3	630	1791	934	0.88	96.2
FLS 450 LB	630	1493	1132	0.88	96.1	1492	1063	0.86	95.9	725	1793	1092	0.87	95.8
FLS 450 LVB	675	1491	1205	0.88	96.7	1490	1132	0.86	96.5	775	1791	1160	0.87	96.4

For power ratings above 675 kW, please consult Leroy-Somer.

### E1 - Selection data: single-speed



IP 55 CI. F - ∆T 80 K 400 V +/- 10%

Can be used at 400 V  $\pm 10\%$  in the conditions defined on page 61

#### MAINS SUPPLY $\triangle$ 230 / Y 400 V or $\triangle$ 400 V 50 Hz

Power Apparent Moment Rated Rated Rated Power Torque Efficiency Weight factor  $I_d/I_n$  $C_d/C_n$  $C_m/C_n$ at 50 Hz speed torque current power curve of inertia kW min<sup>-1</sup> N.m 50 % 75 % 100 % 50 % 75 % 100 % kVA N٩ Туре А kg.m<sup>2</sup> kg FLS 80 L 0.8 0.55 0.74 3.6 0.25 2.5 0.68 60.3 2 1.9 3 0.0024 14 950 54 58 0.6 FLS 80 L 0.37 940 3.7 1.2 0.55 0.68 0.74 55 59 61 2.1 0.0032 15 3.8 1.9 0.8 4 FLS 80 L 0.55 955 5.5 1.8 0.46 0.59 0.67 60 64 65 4.4 2.5 2.6 1.3 2 0.0042 16 FLS 90 S 0.75 940 7.5 2.1 0.65 0.75 0.8 60 64 65.2 3.5 2 2.2 1.4 3 0.0039 21 ELS 90 L 1.1 940 11 27 0.66 0.76 0.81 70 73 73 5 4.8 18 22 1.8 Δ 0 0048 23 FLS 100 LK 1.5 955 15 35 0.61 0.72 0.78 76 78 78.3 6.3 22 28 25 2 0.0134 41 FLS 112 M 22 960 22 52 0.59 0.71 0 77 79 80 80 55 23 24 36 3 0.015 45 FLS 132 S 3 953 30 6.9 0.63 0.71 0.76 80 82.2 81.9 53 22 24 47 2 0.0376 71 FLS 132 M 4 970 40 9 0.61 0.72 0.78 81 82 82 1 6.7 28 27 62 1 0.0517 76 FLS 132 MU 5.5 970 54 12.2 0.63 0.74 0.79 81 82 82.1 7.1 32 2.7 8.5 1 0.0595 88 FLS 160 M 7.5 968 74 16 0.65 0.75 0.80 84.9 86.4 86 5 1.5 2.4 11 5 0.085 100 FLS 160 L 11 966 109 23 0.66 0.76 0.81 85.9 87.4 87 5 1.5 2.4 16 5 0.12 128 FLS 180 L 15 974 147 30 0.67 0.77 0.82 88.3 89.7 89.5 7.1 2.1 3.1 21 2 0.2 170 FLS 200 LA 18.5 975 181 36 0.68 0.78 0.83 88.9 90.5 90.7 7 2.2 3.3 25 2 0.29 240 **FLS 200 LB** 22 973 216 43 0.66 0.76 0.81 89.7 91.3 91.5 7 2.2 3.3 30 2 0.31 260 FLS 225 M 30 978 293 59 0.64 0.74 0.80 92.3 93.3 92 6 2 2.4 41 3 0.94 392 FLS 250 M 37 977 362 73 0.66 0.76 0.80 91.6 92.6 92.5 6.2 2.2 2.6 50 3 0.94 394 FLS 280 S 45 971 440 84 0.7 0.80 0.84 92 93.1 93 6 1.9 2.3 58 3 1.13 455 55 2 FLS 280 M 977 538 109 0.65 0.75 0.79 92 93.1 93 6.9 2.8 3.3 75 1.26 532 **FLS 315 ST** 75 987 731 133 0.77 0.84 0.86 94.2 94.9 94.8 6.5 2.3 2.1 92 6 1.8 850 FLS 315 M 90 987 875 161 0.76 0.83 0.85 95 95.7 95.6 6.7 1.7 1.5 111 7 2.6 1000 FLS 315 LA 110 983 1067 199 0.76 0.83 0.85 93.9 94.6 94.5 6 1.5 1.3 138 7 2.6 1050 FLS 315 LB 1280 241 0.74 0.83 95.3 96 95.9 7.4 2 1.8 167 7 3.5 1125 132 988 0.81 FLS 315 LB 150 1454 277 0.76 0.81 0.82 95.7 96.1 95.8 6.6 1.5 2.5 192 9 3.5 1125 986 FLS 355 LA 185 1783 346 0.68 0.77 0.81 94.8 95.7 95.8 7.5 2 3.3 240 3 5.4 1415 987 FLS 355 LB 988 0.68 0.77 0.81 94.5 95.5 95.6 7.4 1.9 3.1 286 3 6.3 1535 220 2129 412 FLS 355 LD 250 993 2406 459 0.72 0.79 0.82 95.3 95.8 95.8 7.8 2.1 2.3 317 5 8.6 1935 FLS 355 LD 300 992 2885 558 0.72 0.79 0.82 94.7 95.2 95.2 6.8 1.65 1.8 386 5 8.6 1935 FLS 355 LKB 350 994 3376 637 0.73 0.80 0.83 94.8 95.8 96 6.5 1.7 1.6 442 5 17 2350 FLS 400 LB 350 994 3376 637 0.73 0.80 0.83 94.8 95.8 96 6.5 1.7 1.6 442 5 17 2400 FLS 450 LA 400 996 3851 773 0.61 0 72 0 78 94 4 95.7 96.3 8 2 22 535 5 33 3230 FI S 400 I KB 500 996 4809 952 0.62 0 73 0 79 94 6 95.9 96.5 8 2 22 659 5 35 3350 ELS 450 LB 500 006 4809 952 0.62 0 73 0 79 94 6 95.0 96.5 8 2 22 659 5 35 3400 FLS 450 LB 550 996 5273 1034 0.63 0 74 0.8 94 6 95.9 96.5 75 1.8 1.9 716 5 35 3400

For power ratings above 550 kW, please consult Leroy-Somer.

\* Torque curve

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## E1 - Selection data: single-speed

Voltage and f	requency	MAIN	S SUPPI	LY 380 V	50 Hz	MAINS	S SUPP	LY 415 V	50 Hz			OFFICE A office of the second		60 Hz
	Power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	kW	min <sup>-1</sup>	A		%	min <sup>-1</sup>	A		%	kW	min <sup>-1</sup>	А		%
LS 80 L	0.25	940	0.8	0.78	60.4	950	0.8	0.71	60	0.3	1145	0.8	0.74	64.2
LS 80 L	0.37	940	1.2	0.77	63.5	955	1.2	0.7	64	0.45	1145	1.2	0.76	63.5
LS 80 L	0.55	945	1.8	0.72	66.3	960	1.8	0.65	64	0.66	1150	1.8	0.68	68.8
LS 90 S	0.75	930	2.1	0.83	66.3	945	2	0.79	64.6	0.9	1140	2	0.78	73.6
LS 90 L	1.1	935	2.8	0.83	72.9	950	2.7	0.78	73.5	1.3	1145	2.6	0.81	76.2
LS 100 LK	1.5	950	3.7	0.8	78	960	3.5	0.76	78.1	1.8	1160	3.6	0.78	80.3
LS 112 M	2.2	950	5.3	0.8	78.5	965	5.1	0.75	79.5	2.6	1155	5.1	0.78	81.3
LS 132 S	3	943	7.1	0.79	81.1	957	6.9	0.74	81.7	3.6	1145	7	0.78	82.7
LS 132 M	4	965	9.3	0.8	81.9	970	9.1	0.75	82	4.8	1170	9	0.8	83.7
LS 132 MU	5.5	965	11.2	0.81	92.1	975	12.3	0.76	81.9	6.6	1160	12.3	0.81	83.1
LS 160 M	7.5	959	16.4	0.82	84.9	970	15.9	0.77	85.2	8.6	1159	15.6	0.82	84.7
LS 160 L	11	960	23	0.84	87.2	969	22	0.79	87	12.6	1169	23	0.79	87
LS 180 L	15	970	30	0.86	89	977	29	0.81	89.6	17	1170	28	0.86	88.8
LS 200 LA	18.5	971	37	0.85	90.7	976	35	0.82	90.7	21	1171	34	0.85	90.5
LS 200 LB	22	970	45	0.82	91.4	977	43	0.78	91.3	25	1170	42	0.82	91.2
LS 225 M	30	974	61	0.82	91.6	980	58	0.78	92	34.5	1174	58	0.82	91.4
LS 250 M	37	973	75	0.81	92.4	979	72	0.78	92.1	42	1173	71	0.81	92.2
LS 280 S	45	967	87	0.85	92.6	972	83	0.82	92.6	52	1167	85	0.84	91.9
LS 280 M	55	973	110	0.82	92.6	978	107	0.77	93	63	1173	104	0.82	92.4
LS 315 ST	75	986	137	0.88	94.6	988	128	0.86	94.8	85	1188	131	0.86	94.6
LS 315 M	90	985	165	0.87	95.5	988	156	0.84	95.5	105	1185	159	0.87	95.3
LS 315 LA	110	981	206	0.86	94.6	985	198	0.82	94.6	125	1185	203	0.82	94.4
LS 315 LB	132	986	250	0.84	95.8	989	243	0.79	95.7	150	1186	235	0.84	95.6
LS 315 LB	150	988	284	0.84	95.8	990	277	0.79	95.6	170	1188	266	0.84	95.6
LS 355 LA	185	983	345	0.85	96	988	357	0.76	95.1	210	1184	328	0.84	95.8
LS 355 LB	220	985	418	0.84	95.4	988	413	0.78	95.1	250	1185	393	0.84	95.2
LS 355 LD	250	991	477	0.83	95.8	994	450	0.8	96.7	287	1191	450	0.83	96.5
LS 355 LD	300	990	571	0.84	95.1	993	549	0.8	95.2	345	1190	544	0.84	94.9
LS 355 LKB	350	993	676	0.82	96	995	669	0.76	95.9	400	1193	648	0.81	95.7
LS 400 LB	350	993	676	0.82	96	995	669	0.76	95.9	400	1193	648	0.81	95.7
LS 450 LA	400	995	778	0.81	96.5	996	784	0.74	96	460	1195	751	0.80	96.2
LS 400 LKB	500	995	961	0.82	96.5	996	955	0.76	96	575	1195	927	0.81	96.2
LS 450 LB	500	995	961	0.82	96.5	996	955	0.76	96	575	1195	927	0.81	96.2
LS 450 LB	550	995	1045	0.83	96.5	996	1036	0.77	96	632	1195	1007	0.82	96.2

For power ratings above 550 kW, please consult Leroy-Somer.





### E1 - Selection data: single-speed



IP 55 CI. F - ∆T 80 K 400 V +/- 10%

Can be used at 400 V  $\pm 10\%$  in the conditions defined on page 61

#### MAINS SUPPLY $\triangle$ 230 / Y 400 V or $\triangle$ 400 V 50 Hz

Moment Power Apparent Rated Rated Rated Power Torque Efficiency Weight factor  $I_d/I_n$  $C_d/C_n$  $C_m/C_n$ at 50 Hz speed torque current power curve of inertia kW min<sup>-1</sup> N.m 50 % 75 % 100 % 50 % 75 % 100 % kVA N٩ Туре А kg.m<sup>2</sup> kg FLS 80 L 0.8 0.46 0.64 1.6 1.6 0.18 2.5 0.58 52.3 5 0.0031 14 710 45 51 3 0.5 FLS 80 L 0.25 3.4 0.44 0.55 0.6 46 54 54.5 3.2 2.3 0.0041 16 720 1.1 2 0.8 4 FLS 90 S 0.37 685 5 1.2 0.46 0.63 0.71 59 63 64 3.5 1.7 1.7 0.9 8 0.0038 21 FLS 90 L 0.55 695 7.5 1.7 0.46 0.63 0.72 54 63.7 63 3.3 1.8 1.8 1.2 8 0.0047 23 FLS 100 LK 0.75 720 10 23 0 47 0.6 0.68 66 70 70.9 4.1 19 19 1.6 8 0.0085 41 FLS 100 LK 1.1 720 15 3.8 0 44 0.56 0.62 60 66 68 4.1 18 23 2.6 8 0.0117 43 FLS 112 M 1.5 725 20 48 0 45 0.57 0.63 68 72 72 5 4 21 22 33 8 0.015 45 FLS 132 S 22 715 30 72 0 44 0.55 06 72 74 74 32 14 1.8 5 5 0.0253 71 FLS 132 M 3 705 40 9.1 0 46 0.57 0.63 73 76 76 3.1 1.3 1.9 63 5 0 0334 81 **FLS 160 MA** 4 710 54 11.3 0 44 0.56 0.63 80.1 82 81.5 3.8 14 1.7 7.8 5 0.062 105 10.4 **FLS 160 MB** 5.5 710 74 15 0.46 0.58 0.65 80.6 82.5 82 3.8 1.4 1.7 5 0.071 111 83 FLS 160 L 7.5 715 100 20 0.46 0.58 0.65 81.6 83.5 3.8 1.5 1.8 14 5 0.086 128 FLS 180 L 11 724 147 27 0.51 0.63 0.7 82.4 84.9 85.1 3.9 1.4 1.7 19 5 0.21 175 FLS 200 L 15 729 196 34 0.53 0.66 0.72 86.2 88 88.1 5 1.8 2.6 24 9 0.32 265 FLS 225 ST 18.5 727 242 41 0.54 0.67 0.73 87.1 88.9 89 5 1.6 2.3 29 9 0.38 285 FLS 225 M 22 732 288 48 0.58 0.68 0.72 91.7 92.6 92.1 5.9 1.8 2.5 33 9 0.83 388 FLS 250 M 30 729 393 61 0.64 0.74 0.78 90.8 91.7 91.2 6.2 1.8 2.5 42 9 0.83 393 FLS 280 S 37 723 487 75 0.64 0.74 0.78 91 92.1 92 4.5 1.3 1.8 52 5 1.4 472 91.7 3 FLS 280 M 45 730 592 102 0.55 0.66 0.7 90.7 91.8 6 2.3 3.2 70 1.75 563 **FLS 315 ST** 55 738 715 102 0.71 0.8 0.83 94 94.5 94.2 7.4 2.1 3 71 3 2.7 850 FLS 315 M 75 743 972 147 0.68 0.76 0.78 94.3 95 94.8 7.4 2 2.2 102 4 3.1 1000 **FLS 315 LA** 90 742 1169 177 0.68 0.76 0.78 94.2 94.9 94.7 6.7 1.9 2.1 122 4 4.2 1030 FLS 315 LB 110 742 222 0.66 0.74 0.76 94.3 94.8 7.2 2 2.2 153 4 5.1 1125 1420 95 FLS 355 LA 132 741 1704 258 0.68 0.75 0.78 94.2 95.2 95.3 6.7 2 2.2 179 4 5.5 1415 FLS 355 LB 160 741 2065 312 0.68 0.75 0.78 94.2 95.2 95.3 6.9 2 2.2 4 1535 216 6 FLS 355 LD 741 2581 364 0.74 0.81 0.84 93.9 94.9 95 6.7 1.6 1.7 252 4 6.5 1935 200 **FLS 355 LKA** 250 743 3235 464 0.67 0.77 0.82 94.2 95.1 95.3 6.8 1.6 2.2 322 5 18.5 2170 FLS 400 LA 250 743 3235 464 0.67 0.77 0.82 94.2 95.1 95.3 6.8 1.6 2.2 322 5 18.5 2200 FLS 355 LKB 300 741 3882 552 0.68 0.78 0.83 94 94.8 95 6 1.1 1.5 382 5 21.6 2370 FLS 400 LB 300 741 3882 552 0.68 0.78 0.83 94 94.8 95 6 1.1 1.5 382 5 21.6 2400 95 FLS 400 LKA 350 746 4500 652 0.69 0 78 0.81 95.9 96.2 62 17 14 452 7 40 3100 FLS 450 LA 350 746 4500 652 0.69 0 78 0.81 95 95.9 96.2 62 17 14 452 7 40 3150 FI S 400 I KB 400 7/6 5148 737 0.71 0 79 0.82 94 9 95.8 96 1 67 1.9 1.6 510 7 17 3420 FLS 450 LB 400 746 5148 737 0 71 0 79 0.82 94 9 95.8 96 1 6.7 1.9 1.6 510 7 47 3470

For power ratings above 400 kW, please consult Leroy-Somer.

\* Torque curve

section D4.4 - page 63



## E1 - Selection data: single-speed

Voltage and f	requency	MAINS	S SUPPI	LY 380 V	50 Hz	MAINS	S SUPP	LY 415 V	50 Hz			OFFICE OF		60 Hz
	Power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	kW	min <sup>-1</sup>	A		%	min <sup>-1</sup>	A		%	kW	min <sup>-1</sup>	A		%
FLS 80 L	0.18	700	0.8	0.66	53	710	0.8	0.61	52	0.22	860	0.8	0.62	56.2
LS 80 L	0.25	710	1.1	0.63	56	720	1.2	0.57	53.1	0.3	870	1.1	0.59	58.8
LS 90 S	0.37	670	1.2	0.75	63	700	1.2	0.69	62	0.45	835	1.2	0.71	66.5
LS 90 L	0.55	680	1.8	0.74	62	700	1.8	0.67	64	0.66	810	1.8	0.71	66.5
LS 100 LK	0.75	715	2.3	0.71	70.6	720	2.3	0.66	69.9	0.9	870	2.2	0.7	72.6
LS 100 LK	1.1	710	3.6	0.68	68	720	3.9	0.6	65	1.3	870	3.6	0.64	71.5
LS 112 M	1.5	715	4.7	0.67	72.3	725	4.9	0.6	70.9	1.8	870	4.7	0.65	74.3
LS 132 S	2.2	710	7.6	0.6	73.5	720	8.0	0.53	72	2.6	855	7.3	0.59	75.5
LS 132 M	3	695	9.5	0.64	75	710	9.8	0.57	75	3.6	850	10.2	0.59	75
LS 160 MA	4	706	11.4	0.65	81.8	714	11.1	0.61	82.1	4.6	851	10.9	0.64	83.1
LS 160 MB	5.5	706	16	0.67	79.4	714	16	0.62	79.7	6.3	857	15	0.66	82.2
LS 160 L	7.5	707	21	0.67	82.4	718	20	0.62	82.4	8.6	859	19	0.66	84.1
LS 180 L	11	720	27	0.73	85.1	726	28	0.66	84.4	12.5	870	25	0.73	84.9
LS 200 L	15	729	34	0.76	88.6	730	35	0.68	87.7	17	879	32	0.76	87.6
LS 225 ST	18.5	723	41	0.76	89.5	729	42	0.69	89.9	21	876	40	0.73	90.9
LS 225 M	22	731	47	0.77	92.2	734	47	0.71	92.1	25	881	44	0.77	92
LS 250 M	30	725	63	0.8	90.5	731	61	0.75	90.8	34	875	59	0.80	90.3
LS 280 S	37	716	78	0.79	91.4	725	72	0.78	92.1	42	866	73	0.79	91.2
LS 280 M	45	727	101	0.74	91.8	734	97	0.70	91.9	52	879	97	0.73	92.3
LS 315 ST	55	737	104	0.85	94.2	740	100	0.82	93.8	65	884	100	0.87	93.8
LS 315 M	75	742	149	0.81	94.8	743	146	0.76	94.1	85	892	139	0.81	94.6
LS 315 LA	90	741	178	0.81	94.8	743	174	0.76	94.7	105	891	172	0.81	94.9
LS 315 LB	110	741	223	0.79	94.9	743	218	0.74	94.9	125	891	210	0.79	94.7
LS 355 LA	132	740	267	0.79	95.3	743	253	0.76	95.5	150	890	251	0.79	95.1
LS 355 LB	160	740	323	0.79	95.3	743	307	0.76	95.5	185	889	310	0.79	94.9
LS 355 LD	200	740	377	0.85	95	743	356	0.82	95.3	230	890	359	0.85	94.8
LS 355 LKA	250	742	470	0.85	95.2	744	463	0.79	95.2	285	892	444	0.85	94.9
LS 400 LA	250	742	470	0.85	95.2	744	463	0.79	95.2	285	892	444	0.85	94.9
LS 355 LKB	300	740	566	0.85	94.9	742	575	0.77	94.4	345	890	546	0.84	94.5
LS 400 LB	300	740	566	0.85	94.9	742	575	0.77	94.4	345	890	546	0.84	94.5
LS 400 LKA	350	745	660	0.84	96.1	746	626	0.81	96.1	400	895	632	0.83	95.8
LS 450 LA	350	745	660	0.84	96.1	746	626	0.81	96.1	400	895	632	0.83	95.8
LS 400 LKB	400	746	753	0.84	96.2	740	725	0.80	96.1	460	896	726	0.83	95.9
LS 450 LB	400	746	753	0.84	96.2	747	725	0.8	96.1	460	896	726	0.83	95.9

**Somer** 

For power ratings above 400 kW, please consult Leroy-Somer.

## E2 - Selection data: two-speed

#### IP 55 - CI. F Centrifugal applications

		MAINS SUPPLY /	400 V 50 Hz	
Туре	2/4 Poles Dahlander	4/6 Poles PAM* or 2 windings	4/8 Poles Dahlander	6/8 Poles PAM* or 2 windings
-	P <sub>N</sub> kW	P <sub>N</sub> kW	P <sub>N</sub> kW	P <sub>N</sub> kW
FLS 80 L	0.75 / 0.18	0.55 / 0.18	0.75 / 0.12	0.37 / 0.18
LS 90 S	1.1 / 0.22	0.75 / 0.25	1.1 / 0.18	0.55 / 0.27
LS 90 L	1.5 / 0.3	1.1 / 0.37	1.5 / 0.25	0.75 / 0.37
LS 100 LK	2.2 / 0.37	1.5 / 0.55	2.2 / 0.37	
LS 100 LK	3 / 0.55	2.2 / 0.75	3 / 0.55	1.1 / 0.55
LS 112 M	-	3 / 1.1	-	1.5 / 0.75
LS 112 MU	4 / 0.75	4 / 1.5	4 / 0.75	2.2 / 1.1
LS 132 M	5.5 / 1.1	5.5 / 1.8	5.5 / 1.1	3 / 1.5
LS 132 M	7.5 / 1.5	- <u> </u>	7.5 / 1.5	-
LS 160 MA	-	7.3/2.4	-	5 / 1.7
LS 160 MB	11 / 2.7		10 / 2.5	•
LS 160 L	15 / 3.7	10 / 3.3	14 / 3	7.3 / 2.4
LS 180 M	18.5 / 4.5	12.5 / 4	18.5 / 4.5	-
LS 180 L	22 / 5.5	14.5 / 5	22 / 4.8	10 / 3.3
LS 200 LA	-	20 / 6	-	12.5 / 4
LS 200 LB	30 / 7.5		30 / 6.5	15 / 5
LS 225 ST	-	25 / 8.2	-	•
LS 225 MT	37 / 9		37 / 8	•
LS 225 M	42 / 10.5	30 / 10	42 / 8.5	20 / 6.7
LS 250 M	45 / 11	37 / 12.2	45 / 9	25 / 8.2
LS 280 S	55 / 13.7	50 / 16.7	55 / 11	30 / 10
LS 280 M	75 / 18.7	60 / 20	75 / 15	37 / 12.2
LS 315 ST	90 / 27.5	72.5 / 25	90 / 18	50 / 16.7
LS 315 M	-	88.5 / 29	-	60 / 20
LS 315 LA	-	107.5 / 35	110 / 22	75.5 / 25
LS 315 LB	-	132 /45	-	100 / 39
LS 355 LA	-	167 / 55	160 / 32	123 / 41
LS 355 LB	-	200 / 66	200 / 40	147 / 49
LS 355 LD	-	270 / 88	220 / 44	200 / 67
LS 400 LA	-	300 / 100	300 / 60	230 / 78
LS 400 LB	-	335 / 110	450 / 90	250 / 85
LS 450 LA	-	370 / 120	500 / 100	300 / 100
FLS 450 LB	-	450 / 150	550 / 110	330 / 110

\* (PAM up to 132)

The specific electrical characteristics for these motors are available on request.



## E2 - Selection data: two-speed

IP 55 - CI. F General

		MAINS SUPPLY	Δ 400 V 50 Hz	
Туре	2/4 Poles Dahlander	4/6 Poles 2 windings	4/8 Poles Dahlander	6/8 Poles 2 windings
-	P <sub>N</sub> kW	P <sub>N</sub> kW	P <sub>N</sub> kW	P <sub>N</sub> kW
LS 80 L	0.75 / 0.55	-	0.5 / 0.22	-
LS 90 S	1.1 / 0.75	0.55 / 0.37	0.75 / 0.4	-
LS 90 L	1.5 / 1.1	0.75 / 0.55	1.1 / 0.5	-
LS 100 LK	2.2 / 1.5	1.1 / 0.75	-	-
LS 100 LK	3/2.2	1.5 / 1.1	1.5 / 0.75	-
LS 112 M	-	2.2 / 1.5	2.2 / 1.1	-
LS 112 MU	4.5 / 3.7	2.8 / 1.8	3 / 1.5	-
LS 132 M	6 / 4.5	4 / 2.5	5.5 / 3	-
LS 132 M	7.5 / 5.5	5.5 / 3.7	7.5 / 4	-
LS 160 MA	-	5.5/3.7	-	3.75 / 2.5
LS 160 MB	11/9	-	-	-
LS 160 L	15/11	7.5 / 5	12 / 6	5.5 / 3.7
LS 180 M	18.5 / 15.5	9 / 6.2	13 / 7.5	-
LS 180 L	22/16	11 / 7.3	15 / 9	7.5 / 5
LS 200 LA	-	15 / 10	18 / 11	9 / 6
LS 200 LB	30 / 22.5	-	22 / 15	11.5 / 7.7
LS 225 ST	-	18.5 / 12.3	27 / 18	-
LS 225 MT	37 / 27.5	-	-	-
LS 225 M	42 / 31	22.5 / 15	30 / 20	15 / 10
LS 250 M	45 / 33.5	27 / 15	37 / 25	18.5 / 12.5
LS 280 S	55 / 41	37 / 25	45 / 30	22.5 / 15
LS 280 M	75 / 55	45 / 30	55 / 37	27.5 / 18
LS 315 ST	90 / 67	55 / 37	68 / 45	37.5 / 25
LS 315 M	-	66 / 44	83 / 55	45 / 30
LS 315 LA	-	80 / 53	110 / 75	55 / 37
LS 315 LB	-	100 / 67	136 / 90	75 / 50
LS 355 LA	-	125 / 83	166 / 110	90 / 60
LS 355 LB	•	150 / 100	200 / 132	110 / 75
LS 355 LD		200 / 132	240 / 160	150 / 100
LS 400 LA	-	225 / 150	-	175 / 110
LS 400 LB		250 / 165	300 / 200	200 / 132
LS 450 LA	-	275 / 180	375 / 250	225 / 150
FLS 450 LB	-	330 / 225	475 / 315	250 / 160

E





E

	PAGES
F1 - Dimensions of shaft extensions	100
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F3 - Foot and flange-mounted ім вз5 (ім 2001)	102
F4 - Flange-mounted ім в5 (ім 3001)	103
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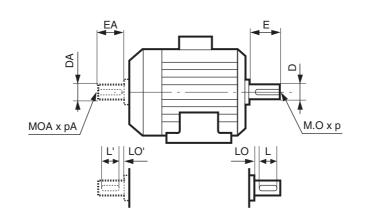


F

## F1 - Dimensions of shaft extensions

Dimensions in millimetres



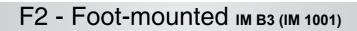


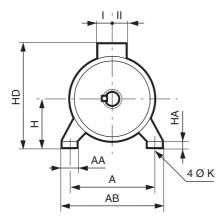


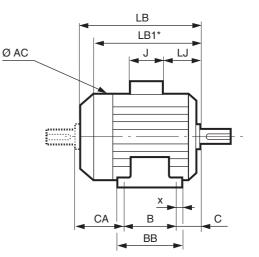
								Ма	in shaft	extensi	ons							
Туре				4,6	and 8 p	oles								2 poles				
	F	GD	D	G	Е	0	р	L	LO	F	GD	D	G	Е	0	р	L	LO
FLS 80 L	6	6	19j6	15.5	40	6	16	30	6	6	6	19j6	15.5	40	6	16	30	6
FLS 90 S/L	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6
FLS 100 LK	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6
FLS 112 M	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6
FLS 132 S/M/MU	10	8	38k6	33	80	12	28	63	10	10	8	38k6	33	80	12	28	63	10
FLS 160 M/L	12	8	42k6	37	110	16	36	90	20	12	8	42k6	37	110	16	36	90	20
FLS 180 MR/L	14	9	48k6	42.5	110	16	36	90	20	14	9	48k6	42.5	110	16	36	90	20
FLS 200 L	16	10	55m6	49	110	20	42	90	20	16	10	55m6	49	110	20	42	90	20
FLS 225 ST/MT/M	18	11	60m6	53	140	20	42	125	15	16	10	55m6	49	110	20	42	90	20
FLS 250 M	18	11	65m6	58	140	20	42	125	15	18	11	60m6	53	140	20	42	125	15
FLS 280 S/M	20	12	75m6	67.5	140	20	42	125	15	18	11	65m6	58	140	20	42	125	15
FLS 315 ST	22	14	80m6	71	170	20	42	140	30	18	11	65m6	58	140	20	42	125	15
FLS 315 M	22	14	80m6	71	170	20	42	140	30	18	11	65m6	58	140	20	42	125	15
FLS 315 L	25	14	90m6	81	170	24	50	140	30	20	12	70m6	62.5	140	20	42	125	15
FLS 355 L/LK	28	16	100m6	90	210	24	50	180	30	22	14	80m6	71	170	20	42	140	30
FLS 400 L/LK/LV	28	16	110m6	100	210	24	50	180	30	-	-	-	-	-	-	-	-	-
FLS 450 L/LV	32	18	120m6	109	210	24	50	180	30	-	-	-	-	-	-	-	-	-

								Secon	idary sh	aft exte	nsions							
ELS 90 S/L ELS 100 LK ELS 112 M ELS 132 S/M/MU ELS 132 S/M/MU ELS 160 M/L ELS 200 L ELS 225 ST/MT/M ELS 250 M ELS 315 ST ELS 315 L ELS 315 L ELS 355 L/LK				4, 6	and 8 p	oles								2 poles				
	FA	GF	DA	GB	EA	OA	pА	Ľ'	LO'	FA	GF	DA	GB	EA	OA	pА	Ľ'	LO'
FLS 80 L	5	5	14j6	11	30	5	15	25	3.5	5	5	14j6	11	30	5	15	25	3.5
FLS 90 S/L	6	6	19j6	15.5	40	6	16	30	6	6	6	19j6	15.5	40	6	16	30	6
FLS 100 LK	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6
FLS 112 M	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6
FLS 132 S/M/MU	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6
FLS 160 M/L	12	8	42k6	37	110	16	36	90	20	12	8	42k6	37	110	16	36	90	20
FLS 180 MR/L	14	9	48k6	42.5	110	16	36	90	20	14	9	48k6	42.5	110	16	36	90	20
FLS 200 L	16	10	55m6	49	110	20	42	90	20	16	10	55m6	49	110	20	42	90	20
FLS 225 ST/MT/M	18	11	60m6	53	140	20	42	125	15	16	10	55m6	49	110	20	42	90	20
FLS 250 M	18	11	60m6	53	140	20	42	125	15	18	11	60m6	53	140	20	42	125	15
FLS 280 S/M	20	12	60m6	53	140	20	42	125	15	18	11	60m6	53	140	20	42	125	15
FLS 315 ST	22	14	80m6	71	170	20	42	140	30	18	11	65m6	58	140	20	42	125	15
FLS 315 M	22	14	80m6	71	170	20	42	140	30	18	11	65m6	58	140	20	42	125	15
FLS 315 L	25	14	90m6	81	170	24	50	140	30	20	12	70m6	62.5	140	20	42	125	15
FLS 355 L/LK	28	16	100m6	90	210	24	50	180	30	22	14	80m6	71	170	20	42	140	30
FLS 400 L/LK/LV	28	16	110m6	100	210	24	50	180	30	-	-	-	-	-	-	-	-	-
FLS 450 L/LV	32	18	120m6	109	210	24	50	180	30	-	-	-	-	-	-	-	-	









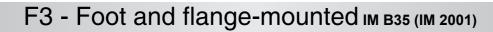
Dimensions in millimetres

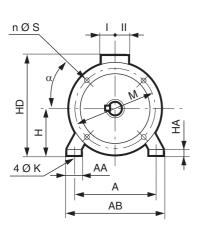
											Main	dime	nsions	i										
Туре	А	AB	в	BB	с	х	AA	к	НА	н	AC	LB	LB1*	CA			FLS					FLSC		
	7	AD	D	00	0	~	~~	ĸ	ПА		AO	LD	LDI	UA.	HD	LJ	J	I	Ш	HD	LJ	J	I	Ш
FLS 80 L	125	157	100	130	50	20	32	9	10	80	160	214	178	68	222	33	114	57	57	230	27	126	63	63
FLS 90 S	140	172	100	160	56	22	34	9	11	90	185	243	204	93	247	28	114	57	57	250	22	126	63	63
FLS 90 L	140	172	125	160	56	22	34	9	11	90	185	243	204	68	247	28	114	57	57	250	22	126	63	63
FLS 100 LK	160	200	140	174	63	22	42	12	12	100	226	323	276	125	276	55	114	57	57	293	37	150	75	75
FLS 112 M	190	230	140	174	70	22	45	12	12	112	226	323	276	119	288	55	114	57	57	305	37	150	75	75
FLS 132 S	216	255	140	223	89	31	58	12	15	132	264	387	328	164	323	46	114	57	57	345	28	150	75	75
FLS 132 M	216	255	178	223	89	31	58	12	15	132	264	387	328	126	323	46	114	57	57	345	28	150	75	75
FLS 132 MU	216	255	178	223	89	31	58	12	15	132	264	410	352	149	323	46	114	57	57	345	28	150	75	75
FLS 160 M	254	294	210	294	108	20	65	14	20	160	310	495	435	182	440	30	246	126	147	440	30	246	126	147
FLS 160 L	254	294	254	294	108	20	65	14	20	160	310	495	435	138	440	30	246	126	147	440	30	246	126	147
FLS 180 MR	279	324	241	295	121	25	80	14	25	180	310	515	450	158	460	30	246	126	147	460	30	246	126	147
FLS 180 L	279	330	279	335	121	28	70	14	28	180	350	555	480	160	481	42	246	126	147	481	42	246	126	147
FLS 200 L	318	374	305	361	133	28	80	18	44	200	394	681	595	248	530	51	246	126	147	530	51	246	126	147
FLS 225 ST	356	420	286	367	149	28	100	18	35	225	394	681	595	251	555	51	246	126	147	555	51	246	126	147
FLS 225 MT	356	420	311	367	149	28	100	18	35	225	394	681	595	226	555	51	246	126	147	555	51	246	126	147
FLS 225 M	356	426	311	375	149	32	80	18	27	225	540	780	630	326	656	70	352	173	210	656	70	352	173	210
FLS 250 M	406	476	349	413	168	32	80	22	27	250	540	780	630	269	681	70	352	173	210	681	70	352	173	210
FLS 280 S	457	527	368	432	190	32	80	22	27	280	540	860	710	302	711	70	352	173	210	711	70	352	173	210
FLS 280 M	457	527	419	483	190	32	80	22	27	280	540	960	810	357	711	70	352	173	210	711	70	352	173	210
FLS 315 ST	508	598	406	547	216	45	90	27	45	315	556	1068	910	452	761	68	352	173	210	761	68	352	173	210
FLS 315 M	508	600	457	598	216	45	100	27	45	315	624	1203	1030	536	835	70	452	217	269	835	70	452	217	269
FLS 315 L	508	600	508	598	216	45	100	27	45	315	632	1203	1030	485	835	70	452	217	269	835	70	452	217	269
FLS 355 LA/LB	610	710	630	710	254	40	110	27	35	355	700	1305	1118	427	910	61	452	217	269	910	61	452	217	269
FLS 355 LC/LD	610	710	630	710	254	40	110	27	35	355	700	1430	1242	552	910	61	452	217	269	910	61	452	217	269
FLS 355 LK**	610	750	630	815	254	40	128	27	45	355	787	1702	-	818	1117	52	700	224	396	1117	52	700	224	396
FLS 400 L/LV**	686	800	710	815	280	65	128	35	45	400	787	1702	-	712	1162	52	700	224	396	1162	52	700	224	396
FLS 400 LKA/LKB**	686	824	800	950	280	59	140	35	45	400	877	1740	-	660	1210	68	700	224	396	1210	68	700	224	396
FLS 450 L/LV**	750	890	800	950	315	94	140	35	45	450	877	1740	-	625	1260	68	700	224	396	1260	68	700	224	396

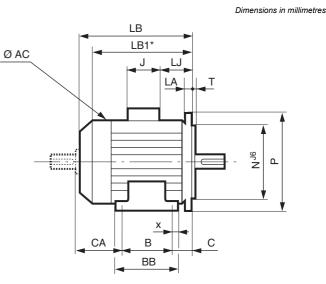
\* LB1 : non-ventilated motor

\*\* LB1 : possible - values to be confirmed









												Ма	in din	nensio	ons											
Туре	А	AB	в	BB	с	х	AA	к	НА	н	AC	LB	LB1*			F	LS					FL	SC			Sym.
	A	AD	D	DD	C	^	AA	ĸ	пА	п	AC	LD	LDI	HD	HJ	LJ	J	I	П	HD	HJ	LJ	J	I	Ш	Sym.
FLS 80 L	125	157	100	130	50	20	32	9	10	80	160	214	178	222	142	33	114	57	57	230	150	27	126	63	63	FF 165
FLS 90 S	140	172	100	160	76	22	34	9	11	90	185	263	224	247	153	48	114	57	57	250	162	22	126	63	63	FF 165
FLS 90 L	140	172	125	160	76	22	34	9	11	90	185	263	224	247	153	48	114	57	57	250	162	22	126	63	63	FF 165
FLS 100 LK	160	200	140	174	63	22	42	12	12	100	226	323	276	276	176	55	114	57	57	293	193	37	150	75	75	FF 215
FLS 112 M	190	230	140	174	70	22	45	12	12	112	226	323	276	288	176	55	114	57	57	305	193	37	150	75	75	FF 215
FLS 132 S	216	255	140	223	89	31	58	12	15	132	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75	FF 265
FLS 132 M	216	255	178	223	89	31	58	12	15	132	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75	FF 265
FLS 132 MU	216	255	178	223	89	31	58	12	15	132	264	410	352	323	195	46	114	57	57	345	213	28	150	75	75	FF 265
FLS 160 M	254	294	210	294	108	20	65	14	20	160	310	495	435	440	280	30	246	126	147	440	280	30	246	126	147	FF 300
FLS 160 L	254	294	254	294	108	20	65	14	20	160	310	495	435	440	280	30	246	126	147	440	280	30	246	126	147	FF 300
FLS 180 MR	279	324	241	295	121	25	80	14	25	180	310	515	450	460	280	30	246	126	147	460	280	30	246	126	147	FF 300
FLS 180 L	279	330	279	335	121	28	70	14	28	180	350	555	480	481	280	42	246	126	147	481	280	42	246	126	147	FF 300
FLS 200 L	318	374	305	361	133	28	80	18	44	200	394	681	595	530	330	51	246	126	147	530	315	51	246	126	147	FF 350
FLS 225 ST	356	420	286	367	149	28	100	18	35	225	394	681	595	555	330	51	246	126	147	555	315	51	246	126	147	FF 400
FLS 225 MT	356	420	311	367	149	28	100	18	35	225	394	681	595	555	330	51	246	126	147	555	315	51	246	126	147	FF 400
FLS 225 M	356	426	311	375	149	32	80	18	27	225	540	780	630	656	431	70	352	173	210	656	431	70	352	173	210	FF 400
FLS 250 M	406	476	349	413	168	32	80	22	27	250	540	780	630	681	431	70	352	173	210	681	431	70	352	173	210	FF 500
FLS 280 S	457	527	368	432	190	32	80	22	27	280	540	860	710	711	431	70	352	173	210	711	431	70	352	173	210	FF 500
FLS 280 M	457	527	419	483	190	32	80	22	27	280	540	960	810	711	431	70	352	173	210	711	431	70	352	173	210	FF 500
FLS 315 ST	508	598	406	547	216	45	90	27	45	315	556	1068	910	761	446	68	352	173	210	761	446	68	352	173	210	FF 600
FLS 315 M	508	600	457	598	216	45	100	27	45	315	624	1203	1030	835	520	70	452	217	269	835	520	70	452	217	269	FF 600
FLS 315 L	508	600	508	598	216	45	100	27	45	315	632	1203	1030	835	520	70	452	217	269	835	520	70	452	217	269	FF 600
FLS 355 LA/LB	610	710	630	710	254	40	110	27	35	355	700	1305	1118	910	555	61	452	217	269	910	555	61	452	217	269	FF 740
FLS 355 LC/LD	610	710	630	710	254	40	110	27	35	355	700	1430	1242	910	555	61	452	217	269	910	555	61	452	217	269	FF 740
FLS 355 LK**	610	750	630	815	254	40	128	27	45	355	787	1702	-	1117	762	52	700	224	396	1117	762	52	700	224	396	FF 740
FLS 400 L/LV**	686	800	710	815	280	65	128	35	45	400	787	1702	-	1162	762	52	700	224	396	1162	762	52	700	224	396	FF 940
FLS 400 LKA/LKB**	686	824	800	950	280	59	140	35	45	400	877	1740	-	1210	810	68	700	224	396	1210	810	68	700	224	396	FF 940
FLS 450 L/LV**	750	890	800	950	315	94	140	35	45	450	877	1740	-	1260	810	68	700	224	396	1260	810	68	700	224	396	FF 1080

LEROY\* SOMER

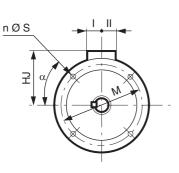
\* LB1 : non-ventilated motor

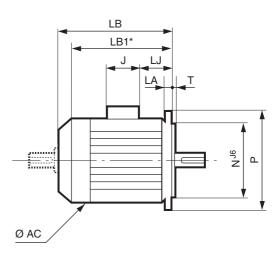
\*\* LB1 : possible - values to be confirmed



## F4 - Flange-mounted IM B5 (IM 3001)

Dimensions in millimetres





IEC			Facepla	te dime	ension	s	
Symbol	М	Ν	Р	т	n	S	LA
FF 165	165	130	200	3.5	4	12	10
FF 165	165	130	200	3.5	4	12	10
FF 165	165	130	200	3.5	4	12	10
FF 215	215	180	250	4	4	15	12
FF 215	215	180	250	4	4	15	12
FF 265	265	230	300	4	4	14.5	14
FF 265	265	230	300	4	4	14.5	14
FF 265	265	230	300	4	4	14.5	14
FF 300	300	250	350	5	4	18.5	15
FF 300	300	250	350	5	4	18.5	15
FF 300	300	250	350	5	4	18.5	15
FF 300	300	250	350	5	4	18.5	15
FF 350	350	300	400	5	4	18	15
FF 400	400	350	450	5	8	18	16
FF 400	400	350	450	5	8	18	16
FF 400	400	350	450	5	8	18	16
FF 500	500	450	550	5	8	18	18
FF 500	500	450	550	5	8	18	18
FF 500	500	450	550	5	8	18	18
FF 600	600	550	660	6	8	22	25
FF 600	600	550	660	6	8	22	25
FF 600	600	550	660	6	8	22	25
FF 740	740	680	800	6	8	22	25
FF 740	740	680	800	6	8	22	25
FF 740	740	680	800	6	8	22	25
FF 940	940	880	1000	6	8	28	28
FF 940	940	880	1000	6	8	28	28
FF 1080	1080	1000	1150	6	8	28	30

Туре								
	AC	LB	LB1	HJ	LJ	J	I	Ш
FLS 80 L	160	214	178	142	33	114	57	57
FLS 90 S	185	263	224	153	48	114	57	57
FLS 90 L	185	263	224	153	48	114	57	57
FLS 100 LK	226	323	276	176	55	114	57	57
FLS 112 M	226	323	276	176	55	114	57	57
FLS 132 S	264	387	328	195	46	114	57	57
FLS 132 M	264	387	328	195	46	114	57	57
FLS 132 MU	264	410	352	195	46	114	57	57
FLS 160 M	310	495	435	280	30	246	126	147
FLS 160 L	310	495	435	280	30	246	126	147
FLS 180 MR	310	515	450	280	30	246	126	147
FLS 180 L	350	555	480	301	42	246	126	147
FLS 200 L	394	681	595	330	51	246	126	147
FLS 225 ST	394	681	595	330	51	246	126	147
FLS 225 MT	394	681	595	330	51	246	126	147
FLS 225 M	540	780	630	431	70	352	173	210
FLS 250 M	540	780	630	431	70	352	173	210
FLS 280 S	540	860	710	431	70	352	173	210
FLS 280 M	540	960	810	431	70	352	173	210
FLS 315 ST	556	1068	910	446	68	352	173	210
FLS 315 M	624	1203	1030	520	70	452	217	269
FLS 315 L	632	1203	1030	520	70	452	217	269
FLS 355 LA/LB	700	1305	1118	555	61	452	217	269
FLS 355 LC/LD	700	1305	1242	555	61	452	217	269
FLS 355 LK**	787	1702	-	762	52	700	224	396
FLS 400 L/LV**	787	1702	-	762	52	700	224	396
FLS 400 LKA/LKB**	877	1740	-	810	68	700	224	396
FLS 450 L/LV**	877	1740	-	810	68	700	224	396
** LB1 : possible -	values	to be c	onfirme	d				

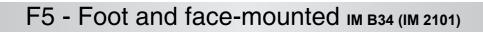
Main dimensions

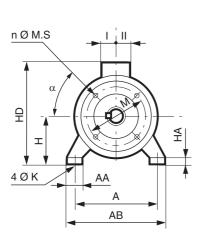
\* LB1 : non-ventilated motor

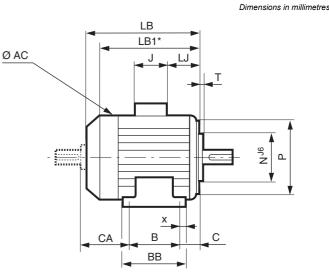
Flange-mounted motors in position IM 3001 (IM B5) are only available up to frame size 225. See section C1 for mounting arrangements.

\*\* LB1 : possible - values to be confirmed









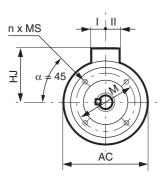
												Ma	in dim	ensio	ns											
Туре	•		в	BB	с	v	AA	к	НА	н	AC	LB	LB1*			F	LS					FL	SC			C:
	A	AB	Б	DD	C	^	AA	ĸ	па	п	AC	LD	LDI	HD	HJ	LJ	J	Ι	Ш	HD	HJ	LJ	J	Ι	П	- Sym.
FLS 80 L	125	157	100	130	50	20	32	9	10	80	160	214	178	222	142	33	114	57	57	230	150	27	126	63	63	FT 100
FLS 90 S	140	172	100	160	56	22	34	9	11	90	185	243	204	247	153	28	114	57	57	250	162	22	126	63	63	FT 115
FLS 90 L	140	172	125	160	56	22	34	9	11	90	185	243	204	247	153	28	114	57	57	250	162	22	126	63	63	FT 115
FLS 100 LK	160	200	140	174	63	22	42	12	12	100	226	323	276	276	176	55	114	57	57	293	193	37	150	75	75	FT 130
FLS 112 M	190	230	140	174	70	22	45	12	12	112	226	323	276	288	176	55	114	57	57	305	193	37	150	75	75	FT 130
FLS 132 S	216	255	140	223	89	31	58	12	15	132	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75	FT 215
FLS 132 M	216	255	178	223	89	31	58	12	15	132	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75	FT 215
FLS 132 MU	216	255	178	223	89	31	58	12	15	132	264	410	352	323	195	46	114	57	57	345	213	28	150	75	75	FT 215

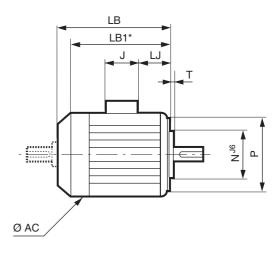
\* LB1 : non-ventilated motor



## F6 - Face-mounted IM B14 (IM 3601)

Dimensions in millimetres





		Flar	nge di	mensi	ons	
IEC Symbol	М	Ν	Ρ	т	n	MS
FT 100	100	80	120	3	4	M6
FT 115	115	95	140	3	4	M8
FT 115	115	95	140	3	4	M8
FT 130	130	110	160	3.5	4	M8
FT 130	130	110	160	3.5	4	M8
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12

							Main	dimer	isions						
Туре	AC	LB	LB1*			F	LS					FL	SC		
	AC	LD	LDI	HD	HJ	LJ	J	I	Ш	HD	HJ	LJ	J	I	Ш
FLS 80 L	160	214	178	222	142	33	114	57	57	230	150	27	126	63	63
FLS 90 S	185	243	204	247	153	28	114	57	57	250	162	22	126	63	63
FLS 90 L	185	243	204	247	153	28	114	57	57	250	162	22	126	63	63
FLS 100 LK	226	323	276	276	176	55	114	57	57	293	193	37	150	75	75
FLS 112 M	226	323	276	288	176	55	114	57	57	305	193	37	150	75	75
FLS 132 S	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75
FLS 132 M	264	387	328	323	195	46	114	57	57	345	213	28	150	75	75
FLS 132 MU	264	410	352	323	195	46	114	57	57	345	213	28	150	75	75

\* LB1: non-ventilated motor

F



### 3-phase TEFV induction motors FLS cast iron Optional features

### G1 - Non-standard flanges

As an option, LEROY-SOMER motors can be fitted with flanges and faceplates that are larger or smaller than standard. This means that motors can be adapted to all types of situation without the need for costly and time-consuming modifications. The tables below give flange and faceplate dimensions and flange/motor compatibility.

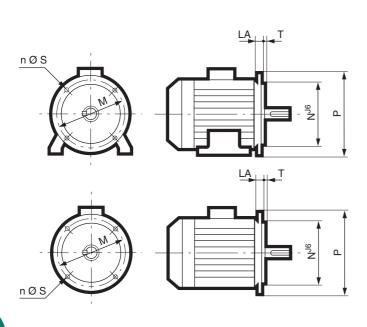
The bearing and shaft extension for each frame size remain standard.

#### MAIN FLANGE DIMENSIONS

Flange-mounted (FF)

Face-mounted (FT)

Dimensions in millimetres

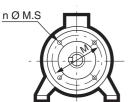


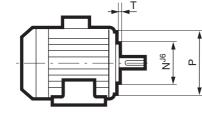
IEC			Flang	e dimen	sions		
symbol	м	N	Р	т	n	S	LA
FF 115	115	95	140	3	4	10	10
FF 130	130	110	160	3.5	4	10	10
FF 165	165	130	200	3.5	4	12	10
FF 215	215	180	250	4	4	15	12
FF 265	265	230	300	4	4	15	14
FF 300	300	250	350	5	4	18	15
FF 350	350	300	400	5	4	18	15
FF 400	400	350	450	5	8	18	16
FF 500	500	450	550	5	8	18	18**
FF 600	600	550*	660	6	8	22	25
FF 740	740	680*	800	6	8	22	25
FF 940	940	880*	1000	6	8	28	28
FF 1080	1080	1000*	1150	6	8	28	30

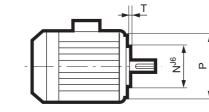
\* Tolerance Njs<sup>6</sup> from FF 600 upwards

\*\* LA = 22 for frame sizes  $\geq 280$ 

Dimensions in millimetres







Symbol		F	aceplate	dimensio	ns	
IEC	м	N	Р	т	n	M.S
FT 85	85	70	105	2.5	4	M6
FT 100	100	80	120	3	4	M6
FT 115	115	95	140	3	4	M8
FT 130	130	110	160	3.5	4	M8
FT 165	165	130	200	3.5	4	M10
FT 215	215	180	250	4	4	M12
FT 265	265	230	300	4	4	M12



nØM.S

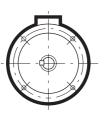
## G1 - Non-standard flanges

Flange-mounted (FF)												Face-r	nount	ed (FT	)					
Flange type Motor type	FF 115	FF 130	FF 165	FF 215	FF 265	FF 300	FF 350	FF 400	FF 500	FF 600	FF 740	FF 940	FF 1080	FT 85	FT 100	FT 115	FT 130	FT 165	FT 215	FT 265
FLS 80 L	О	О	•	*										*	•	*	*	*		
FLS 90	*	*	٠	*										_	*	٠	*	О		
FLS 90 (Foot)	0	О	0	0											*	•	*	0		
FLS 100 LK	О	О	О	٠												*	٠	О	*	
FLS 112 M	О	О	О	•												*	•	0	*	
FLS 112 MR		О	О	٠	*											*	٠	*	*	
FLS 132 S/M/MU			0	0	•	0												*	•	*
FLS 160 M/L	_		_	*	*	٠	*							_						
FLS 180 MR						•	*													
FLS 180 L						٠	*													
FLS 200 L							•	*												
FLS 225 ST/MT							*	•												
FLS 225 S/M								•	*											
FLS 250 M								*	٠											
FLS 280 S									•											
FLS 280 M									٠											
FLS 315 S									*	•										
FLS 315 M/L										٠										
FLS 355 L										0	•									
FLS 355 LK											•	*								
FLS 400											*	•								
FLS 400 LK												٠	*							
FLS 450												*	•							

Standard

O Adapted shaft

\* Adaptable without shaft modifications



NOTE: for flanges up to FF 350, the flange is drilled with 4 holes at an angle of  $45^{\circ}$  in relation to the axis of the terminal box.

NOTE: from flange FF 400 upwards, the flange is drilled with 8 holes at an angle of 22°30 in relation to the axes.



H

## G2 - Variable speed options

The induction motors described in this catalogue are easily integrated into controlled systems and control applications that use frequency inverters.

For these kinds of application, accessories are often required to make operation easier. These accessories include:

- D.C. tachogenerators, which give perfect synchronization of motor speed by slip compensation.

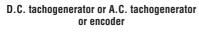
- A.C. tachogenerators for speed measurement.

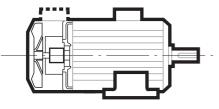
- Forced ventilation for motors used at high or low speeds (see section C4.2).

- Holding brakes for maintaining the rotor in the stop position without needing to leave the motor switched on.

- Encoders which provide digital information for accurate speed maintenance and position control.

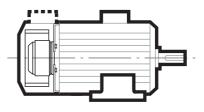
These options can be used singly or in combination as shown in the table opposite.



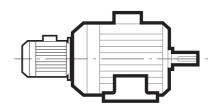


Brake

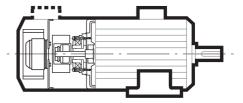
Forced ventilation



Forced exial or radial ventilation\*

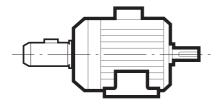


Forced ventilation, brake (D.C. tacho or A.C. tacho or encoder)





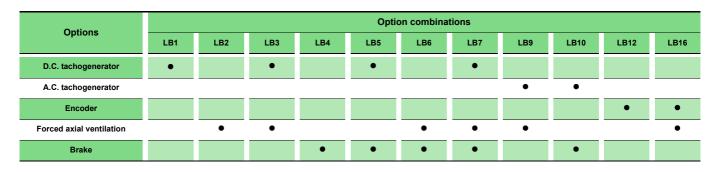




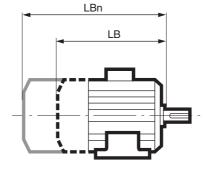
\* For frame sizes 160 and above

LEROY\* SOMER

## G2 - Variable speed options



Turne	Main dimensions LBn											
Туре	LB1	LB2	LB3	LB4	LB5	LB6	LB7	LB9	LB10	LB12	LB16	
FLS 80	LB + 39	LB + 100	LB + 100	LB + 36	-	LB + 125	LB + 200	-	LB + 125	-	-	
FLS 90	LB + 45	LB + 93	LB + 93	LB + 35	-	LB + 117	LB + 193	-	LB + 117	-	-	
FLS 100	LB + 36	LB + 90	LB + 90	LB + 79	-	LB + 140	LB + 218	-	LB + 105	-	-	
FLS 112	LB + 36	LB + 90	LB + 90	LB + 79	-	LB + 140	LB + 218	-	LB + 140	-	-	
FLS 132	LB + 45	LB + 75	LB + 75	LB + 62	-	LB + 95	LB + 165	-	LB + 95	-	-	
FLS 160 / 180 MR	-	LB + 158	-	-	-	-	-	-	-	LB + 95	LB + 278	
FLS 180	-	LB + 136	-	-	-	-		-	-	LB + 95	LB + 226	
FLS 200	-	LB + 145	-	-	-	-	-	-	-	LB + 95	LB + 251	
FLS 225 ST/MT	-	LB + 145	-	-	-	-	-	-	-	LB + 95	LB + 251	
FLS 225 M	-	LB + 138	-	-	-	-	-	-	-	LB + 95	LB + 138	
FLS 250	-	LB + 138	-	-	-	-	-	-	-	LB + 95	LB + 138	
FLS 280	-	LB + 138	-	-	-	-	-	-	-	LB + 95	LB + 138	
ST FLS 315 M/L	-	LB + 388 LB + 352	-	-	-	-	-	-	-	LB + 95	LB + 388 LB + 352	
FLS 355 LA to LD	-	LB + 407	-	-	-	-	-	-	-	LB + 95	LB + 407	
FLS 355 LK / FLS 400 LA to LVB	-	LB + 293	-	-	-	-	-	-	-	LB + 95	LB + 293	
FLS 400 LK / FLS 450	-	LB + 440	-	-		-	-	-	-	LB + 95	LB + 440	





### G3 - Mechanical options

## G3.1 - ADAPTORS FOR VIBRATION SENSOR

On request, our motors can be fitted with adaptors (SPM type) on flanges, in order to fit vibration sensors (not provided).

The adaptors form a connection with the snap-on transmitter.

Being specially designed for harsh environments, they are fitted with a PVC seal after undergoing the following surface treatments:

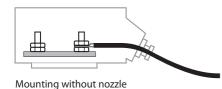
- 1 zinc : 15 μm Zn
- 2 silver for very corrosive environments : 2 μm Cu + 30 μm Ag



#### **G3.2 - TERMINAL BOX NOZZLES**

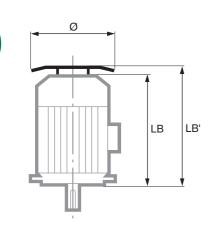
The terminal box nozzle facilitates connection of the power cables to the motor, when using cables with large cross-sections on which a small radius of curvature is impossible.

The three possible methods of mounting are shown below for a horizontal motor, frame size  $\geq$  225 M, with the terminal box on top of the motor.



Mounting with nozzle in horizontal position

#### G3.3 - DRIP COVERS



Drip cover for operation in vertical position, shaft end facing down

Туре	LB'	Ø		
FLS 80	LB + 20	145		
FLS 90 and FLS 100	LB + 20	185		
FLS 112 M	LB + 20	185		
FLS 112 MU	LB + 25	210		
FLS 132	LB + 30	240		
FLS 160 and 180 MR	LB + 60	320		
FLS 180 L	LB + 60	360		
FLS 200 L	LB + 75	400		
FLS 225 ST/MT	LB + 75	400		
FLS 225 M and FLS 250 M	LB + 130	420		
FLS 280 and FLS 315	LB + 130	420		
FLS 355 L	LB + 135	500		
FLS 355 LK	LB + 160	650		
FLS 400	LB + 160	650		
FLS 450	LB + 160	650		

#### **G3.4 - UNIVERSAL MOUNTING**

This enables motors in this range (IEC flange and shaft extension) to be connected to LEROY-SOMER gearboxes:

- Compabloc 2000 (parallel gears)

- Orthobloc 2000 (helical bevel and parallel gears)

Details of this option and of the gearboxes are given in the Leroy-Somer catalogues "Cb 2000 concentric shaft geared motors" and "Ot 2000 helical bevel geared motors and gear units".



### H1 - Voltage drop along cables (standard NFC 15.100)

Voltage drops are calculated using the formula:

$$u = b \left(\rho_1 \frac{L}{S} \cos \varphi + \lambda L \sin \varphi\right) I_s$$

where *u* = voltage drop

b = factor equal to 1 for three-phase circuits, and equal to 2 for single-phase circuits

Note: Three-phase circuits with a neutral that is completely out of balance (loss of two phases) are treated as single-phase circuits.

 $\rho_{\rm 1}$  = resistivity of the conductors in normal duty taken as being equal to the resistivity at the normal duty temperature, ie. 1.25 times the resistivity at 20°C, giving 0.0225  $\Omega {\rm mm}^2 {\rm /m}$  for copper and 0.036  $\Omega {\rm mm}^2 {\rm /m}$  for aluminium.

L = length of cabling conduits in metres

S = cross-section of conductors in mm<sup>2</sup>

 $\cos \phi$  = power factor: if the exact figure is not available, the PF is taken as being 0.8 (sin  $\phi$  = 0.6)

 $\lambda$  = linear reactance of conductors, taken as being equal to 0.08 m $\Omega/m$  if the exact figure is not available

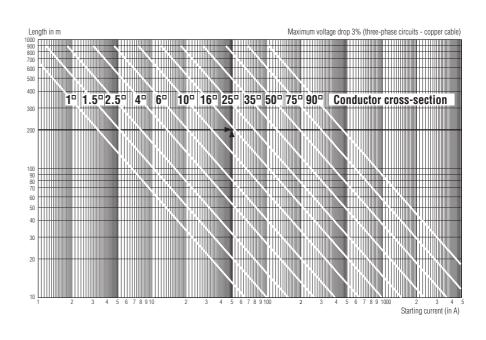
 $I_s$  = current in use, in amps

The higher the current, the greater the voltage drop will be. The voltage drop should therefore be calculated for the starting current to see if this is suitable for the application. If the most important criterion is the starting torque (or starting time), the voltage drop should be limited to 3% maximum\* (the equivalent of a loss of torque of around 6 to 8%).

\* the relative voltage drop (as a %) equals:

$$\Delta u = 100 \frac{u}{U_0}$$

 $U_0$  = voltage between phase and neutral



## Maximum power for D.O.L. motors (See table opposite)

The table opposite shows maximum kW ratings for D.O.L. motors connected to the mains supply.

#### Minimizing motor starting problems

For the installation to remain in good working order, it is necessary to avoid any significant temperature rise in the cabling conduits, while making sure that the protection devices do not interrupt starting.

Operating problems in other equipment connected to the same supply are due to the voltage drop caused by the current demand on starting, which can be many times greater than the current absorbed by the motor at full load.

#### ▼ Maximum power for D.O.L. motors (kW)

Type of motor	Three-phase 380/400V					
Type of premises	Full power D.O.L.	other starting methods				
Residential areas	5.5	11				
Other premises <b>}</b> Overhead power line underground pwr line	11 22	22 45				

"Other premises" includes the service sector, the industrial sector, general housing services, the agricultural sector, etc.

For motors driving a high inertia machine, motors with long starting times, brake motors or change of direction by current reversal, the electricity supply company must carry out all the necessary checks before installation.



## H2 - Earthing impedance

French government decree 62.1454 of 14 November 1962 concerning the protection of operatives in workplaces in which electrical currents are used, requires that when the neutral is connected to the earth by a limiting impedance, the rms value of the fault current multiplied by the resistance of the earth terminal of the mass in which the fault occurs must not exceed:

- 24 V in highly conductive workplaces

- 50 V in other cases

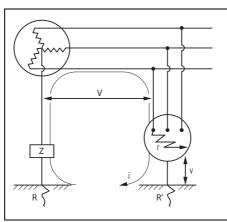
(Ref. standard UTE C 12.100 - page 12, Article 32)

This may be written:

$$v = R'i$$
  
and 
$$V = (Z + R + R' + r) i$$
  
whence 
$$Z = R' \frac{V}{v} - (R + R' + r)$$

and consequently:

$$Z \ge R' \frac{V}{v_L} - (R + R' + r)$$



- V : phase voltage
- Z : limiting impedance
- R : resistance of neutral earth
- R' : resistance of the earth of the mass where the fault occurs
- r : internal fault resistance
- i : fault current
- v : potential of the mass in relation to the earth
- $v_{L}$  : maximum value imposed for that potential

#### Example 1

Highly conductive premises where:

- $R = 3\Omega$  $R' = 20\Omega$
- r = 10Ω V = 220V
- V = 220

 $Z \ge 20 \ x \ \frac{220}{24} \ \text{-} \ (3 + 20 + 10) = 150 \ \Omega$ 

Example 2

Other cas	es:
R =	= 6Ω
R' =	= 10 Ω
r =	= 0Ω
V =	= 380 V
	380

$$Z \ge 10 \ x \ \frac{380}{50} \ \text{-} \ (6 + 10 + 0) = 60 \ \Omega$$





## H3 - Packaging weights and dimensions

	ROAD TRANSPORT									
Frame size		IM 1001	IM 3001 - IM 3011							
	Tare (kg)	Dimensions in mm (L x W x H)	Tare (kg)	Dimensions in mm (L x W x H)						
		Cardboard boxes								
80	1.5	380 x 215 x 280	1.5	380 x 215 x 280						
90	2	475 x 240 x 320	2	475 x 240 x 320						
100	2	455 x 280 x 360	2	455 x 280 x 360						
112	2	455 x 280 x 360	2	455 x 280 x 360						
132	3	565 x 325 x 410	3	565 x 325 x 410						

	Pallets								
160 / 180	5	780 x 430	5	780 x 430					
200 - 225 ST /MT	6	900 x 460	6	900 x 460					
225 M - 250	13	1150 x 500	13	1150 x 500					
280 - 315	18	1850 x 700	18	1850 x 700*					
355	18	2100 x 840	18	2100 x 840*					
355 LK to 450	28	2300 x 950	28	2300 x 950					

\* motors in IM 3011, pallet of 850 x 850 with floor dimensions of 1100 x 1000

	SEA TRANSPORT										
Frame size		IM 1001	IM	3001 - IM 3011							
	Tare (kg)	Dimensions in mm (L x W x H)	Tare (kg)	Dimensions in mm (L x W x H)							
		Plywood crates									
80		on request	on request								
90		on request		on request							
100	21	740 x 480 x 610	24	740 x 480 x 610							
112	21	740 x 480 x 610	24	740 x 480 x 610							
132	21	740 x 480 x 610	24	740 x 480 x 610							
160	45	900 x 540 x 620	50	900 x 550 x 700							
180 MR	45	900 x 560 x 640	45	900 x 550 x 650							
180 L	50	950 x 580 x 690	50	950 x 580 x 690							
200 L	60	1100 x 630 x 750	60	1100 x 600 x 750							
225 ST/MT	70	1150 x 650 x 770	70	1150 x 650 x 770							
225 M	80	1250 x 700 x 810	80	1250 x 700 x 840							
250 M	80	1250 x 700 x 860	100	1250 x 750 x 950							
280 S/M	120	1550 x 790 x 1050	120	1550 x 790 x 1050							
315 ST	130	1600 x 830 x 1090	140	1600 x 860 x 1170							
315 M/L	145	1750 x 860 x 1160	150	1750 x 860 x 1230							
355 LA/LB	170	1900 x 940 x 1230	190	1900 x 1000 x 1370							
355 LC/LD	180	2050 x 940 x 1230	200	2050 x 1000 x 1370							
355 LK	230	2300 x 1020 x 1470	245	2300 x 1000 x 1620							
400 L/LV	240	2300 x 1030 x 1510	290	2300 x 1200 x 1800							
400 LK	270	2450 x 1120 x 1610	305	2450 x 1200 x 1800							
450 L/LV	270	2450 x 1120 x 1610	335	2450 x 1350 x 1900							

- These values are given for individual packages

- Frame sizes up to 132 grouped in cardboard containers on a standard 1200 x 800 pallet



### H4 - Position of lifting rings

# Position of lifting rings for lifting the motor only (not connected to the machine)

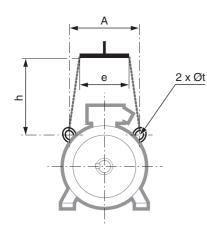
The positions of the lifting rings and the minimum dimensions of the loading bars are given below in order to help with preparation for handling the motors. If these precautions

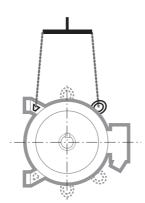
are not followed, there is a risk of warping or crushing some equipment such as the terminal box, protective cover or drip cover.

*Important:* Motors intended for use in the vertical position may be delivered on a pallet in the horizontal position. When the motor is pivoted, the shaft must under no

circumstances be allowed to touch the ground, as the bearings may be irreparably damaged.

#### - horizontal position

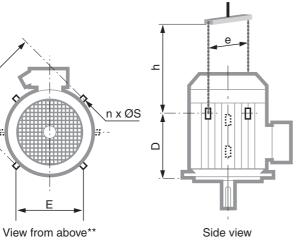




Turne		Horizonta	I position	
Туре	А	e min	h min	t
FLS 100	120	200	150	9
FLS 112	120	200	150	9
FLS 132	160	200	150	9
FLS 160	200	260	150	14
FLS 180 MR	200	260	150	14
FLS 180 L	200	260	150	14
FLS 200	270	260	165	14
FLS 225 ST/MT	270	260	150	14
FLS 225 M	360	265	200	30
FLS 250	360	380	200	30
FLS 280	360	380	500	30
FLS 315 ST	310	380	500	17
FLS 315 M/L	600	600	500	60
FLS 355	600	600	500	60
FLS 400	735	710	500	30
FLS 450	730	710	500	30

- vertical position





Type			Verti	cal pos	ition		
туре	С	E	D	n**	S	e min*	h min
FLS 160	320	200	230	2	14	320	350
FLS 180 MR	320	200	230	2	14	320	270
FLS 180 L	390	265	290	2	14	390	320
FLS 200	410	300	295	2	14	410	450
FLS 225 ST/MT	410	300	295	2	14	410	450
FLS 225 M	480	360	405	4	30	540	350
FLS 250	480	360	405	4	30	540	350
FLS 280 S	480	360	485	4	30	590	550
FLS 280 M	480	360	585	4	30	590	550
FLS 315 ST	590	-	590	2	17	630	550
FLS 315 M/L	700	600	860	4	60	700	550
FLS 355	700	600	860	4	60	700	550
FLS 400	810	350	1135	4	30	810	600
FLS 450	960	400	1170	4	30	960	750

\* : if the motor is fitted with a drip cover, allow an additional 50 to 100 mm to avoid damaging it when the load is swung.

\*\* : if n = 2, the lifting rings form an angle of 90° with respect to the terminal box axis if n = 4, this angle becomes 45°

i, and angle becomes re



## H5 - Identification, exploded views and parts list

### H5.1 - NAMEPLATES

*/5	LERO) SOMI	/◎ <u>M</u> 0 R N	OT. 3∩ 999999	JJ000 <sup>.</sup>	C 90L T 1	<u><u></u> <b>C E</b></u>		LEROY SOME	∕° MO R Ne	T. 3 ∿ F 85702 JJ		4 kg : 26	
IP5	5 IK0	8	cl.F	40C	S.S1	kg 21	IP55	5 IK08	l cl.F	40C	S1	%	d/h
	V	Hz	min -1	kW	cos	Α		V	Hz	min <sup>-1</sup>	kW	cos j	Α
EFF 2	▲ 380 ▲ 230 ▲ 400 ▲ 415 ▲ 440 ▲ 460	50 50 50 60 60	1420 1428 1428 1435 1710 1720	1.50 1.50 1.50 1.50 1.80 1.80	0.86 0.82 0.82 0.79 0.85 0.85	3.4 5.7 3.3 3.4 3.6 3.3		380 400 590 () 415 440 460	50 - - 60 -	1467 1471 - 1472 1762 1767	30 - - 34.5 -	0.86 0.85 - 0.83 0.86 -	58 56 33 55 58 55
-							GRA	ISSE ES	SO UNIF	REX N3			
*Othe	er logos r	nay be	e used as nent BEF	s an opt	ion, Ierina			6313 C 6313 C	-	23 c 23 c		00/7000 H 00/7000 H	

#### - Definition of symbols used on nameplates



#### Legal mark indicating that the equipment conforms to the requirements of European Directives.

MOT 3 ~	: Three-phase A.C. motor
FLS	: FLS range
FLSC	: FLS range Corrobloc finish
90	: Frame size
L	: Housing symbol
TR	: Impregnation index

#### Motor no.

N° : Serial number J : Year of production J : Month of production 001 : Batch number : Efficiency indicator (EFF 2)

IP55 IK08:	Index of protection
I cl. F :	Insulation class F
40°C :	Max. ambient operating
	temperature (IEC 34-1)
<b>S%</b> :	Duty - Duty (operating) factor
<b>d/h</b> :	Number of cycles per hour
kg :	Weight
<b>v</b> :	Supply voltage
Hz :	Supply frequency
min <sup>-1</sup> :	Revolutions per minute (rpm)
kW :	Rated output power
<b>cos</b> φ :	Power factor
<b>A</b> :	Rated current
Δ :	Delta connection
<b>Y</b> :	Star connection

## Bearings

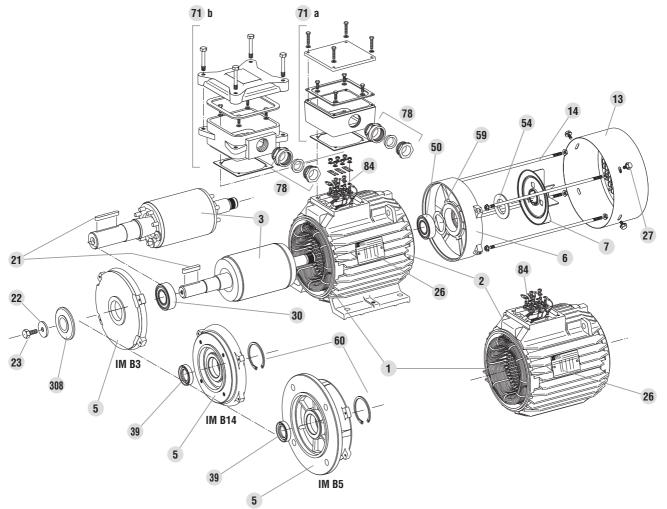
DE : Drive end bearing **NDE** : Non drive end bearing 23 cm<sup>3</sup>: Amount of grease at each regreasing (in cm<sup>3</sup>) 9000/7000 H : Interval (regreasing in hours) for  $\theta$  amb 40°C at frequency 50 Hz/60 Hz ESSO UNIREX N3 : Type of grease

#### Please quote when ordering spare parts



H5 - Identification, exploded views and parts list

H5.2 - FRAME SIZE: 80 to 132



		F	rame size: 80 to 132		
Ref.	Description	Ref.	Description	Ref.	Description
1	Wound stator	21	Shaft extension key	54	Non drive end seal
2	Housing	22	Shaft extension washer	59	Preloading (wavy) washer
3	Rotor	23	Shaft extension screw	60	Circlip
5	Drive end shield (DE)	26	Nameplate	71a	FLS terminal box
6	Non-drive end shield (NDE)	27	Fan cover screw	71b	FLSC terminal box
7	Fan	30	Drive end bearing	78	Cable gland
13	Fan cover	39	Drive end seal	84	Terminal block
14	Tie rods	50	Non drive end bearing	308	Labyrinth seal

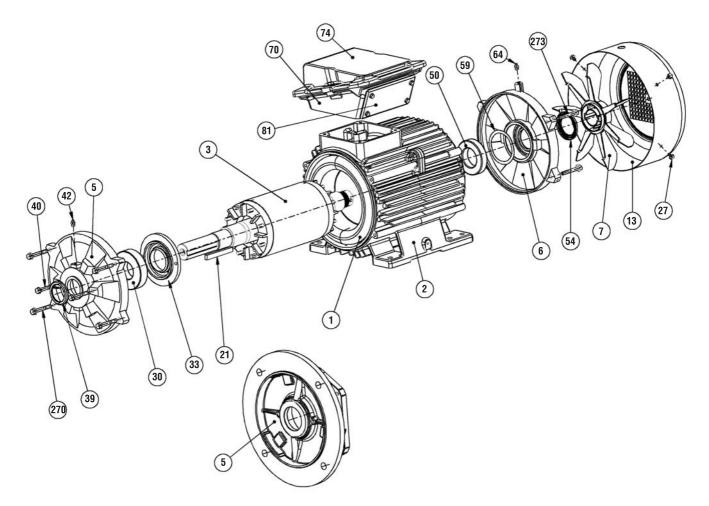
Note: The above illustration of parts does not necessarily show details, forms and volumes accurately.



H

H5 - Identification, exploded views and parts list

H5.3 - FRAME SIZE: 160 - 180

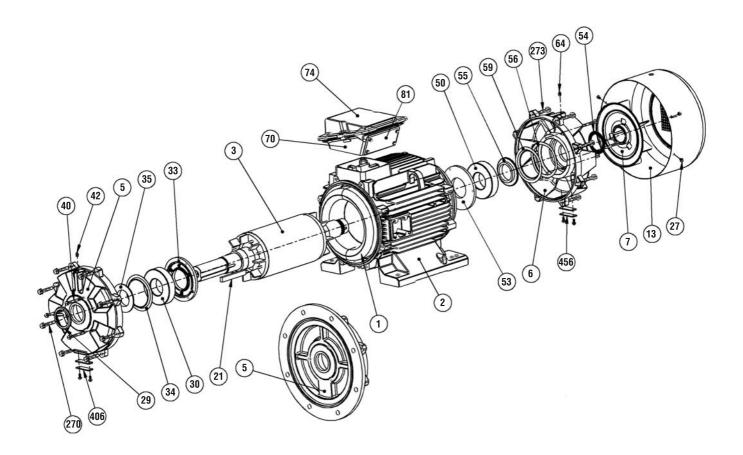


		F	Frame size: 160 - 180		
No.	Description	No.	Description	No.	Description
1	Wound stator	27	Fan cover screw	59	NDE preloading (wavy) washer
2	Housing	30	Drive end bearing	64	NDE grease nipple (rear)
3	Rotor	33	DE internal cover (front)	70	Stator terminal box
5	Drive end shield (DE)	39	DE seal	74	Terminal box lid
6	Non-drive end shield (NDE)	40	Cover fixing screw	81	Cable gland support plate
7	Fan	42	DE grease nipple (front)	270	DE shield fixing screw
13	Fan cover	50	NDE bearing (rear)	273	NDE shield fixing screw
21	Shaft extension key	54	NDE seal		



H5 - Identification, exploded views and parts list

#### H5.4 - FRAME SIZE: 200 to 225 MT

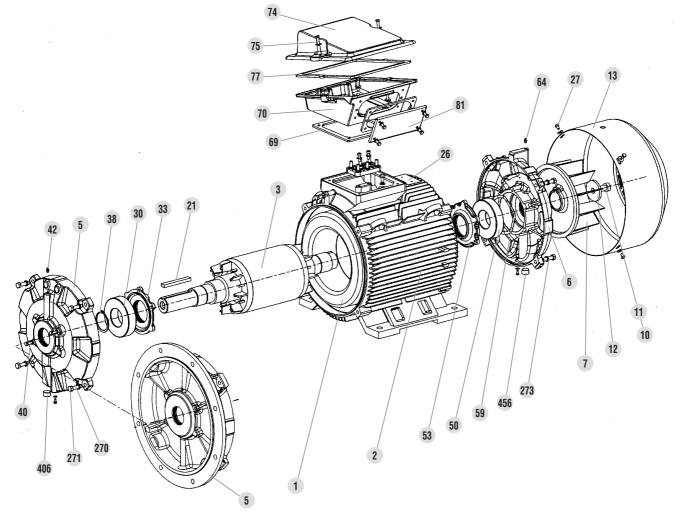


	Frame size: 200 to 225 MT				
No.	Description	No.	Description	No.	Description
1	Wound stator	33	DE internal cover (front)	56	Moving part of NDE grease valve (rear)
2	Housing	34	Fixed part of DE grease valve (front)	59	NDE preloading (wavy) washer
3	Rotor	35	Moving part of DE grease valve (front)	64	NDE grease nipple (rear)
5	Drive end shield (DE)	39	DE seal	70	Stator terminal box
6	Non-drive end shield (NDE)	40	Cover fixing screw	74	Stator terminal box lid
7	Fan	42	DE grease nipple (front)	81	Cable gland support plate
13	Fan cover	50	NDE bearing (rear)	270	DE shield fixing screw
21	Shaft extension key	53	NDE internal cover (rear)	273	NDE shield fixing screw
27	Fan cover screw	54	NDE seal	406	Cover plate of DE grease valve (front)
30	Drive end bearing	55	Fixed part of NDE grease valve (rear)	456	Cover plate of NDE grease valve (rear)



H5 - Identification, exploded views and parts list

#### H5.5 - FRAME SIZE: 225 M to 280

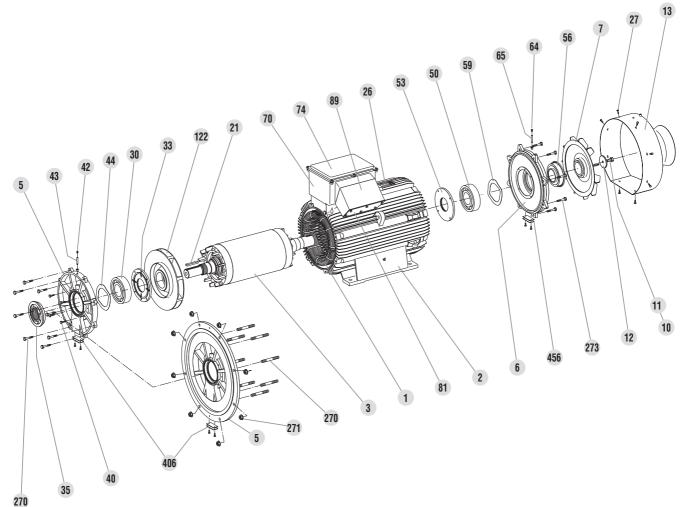


		Fra	ame size: 225 M to 280		
No.	Description	No.	Description	No.	Description
1	Wound stator	26	Nameplate	69	Terminal box base seal
2	Housing	27	Fan cover screw	70	Stator terminal box
3	Rotor	30	Drive end bearing	74	Stator terminal box lid
5	Drive end shield (DE)	33	DE internal cover (front)	75	Terminal box cover fixing screw
6	Non-drive end shield (NDE)	38	DE bearing circlip (front)	77	Terminal box cover seal
7	Fan	40	Cover fixing screw	81	Cable gland support plate
10	Turbine or fan screw (280 - 4p)	42	DE grease nipple (front)	270	DE shield fixing screw
11	Brake washer (not shown) (280 - 4p)	50	NDE bearing (rear)	271	DE shield fixing nut
12	Lock washer (280 - 4p)	53	NDE internal cover (rear)	273	NDE shield fixing screw
13	Fan cover	59	NDE preloading (wavy) washer	406	Cover plate of DE grease valve (front) - (plug)
21	Shaft extension key	64	NDE grease nipple (rear)	456	Cover plate of NDE grease valve (rear) - (plug)



H5 - Identification, exploded views and parts list

H5.6 - FRAME SIZE: 315 to 355 LD

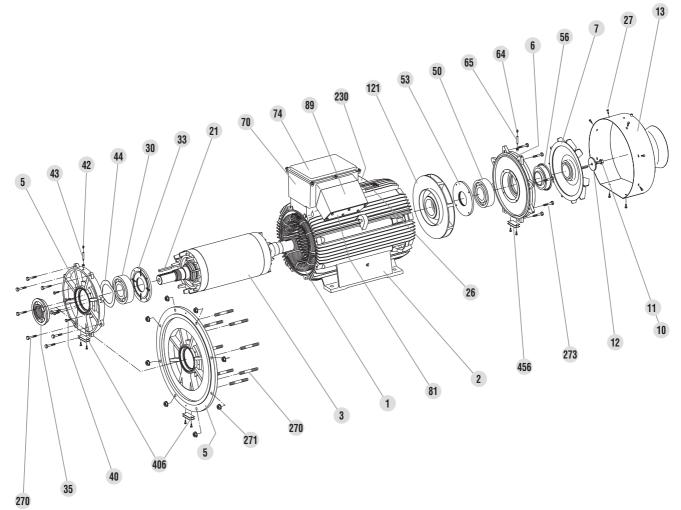


	Frame size: 315 to 355 LD				
No.	Description	No.	Description	No.	Description
1	Wound stator	27	Fan cover screw	64	NDE grease nipple (rear)
2	Housing	30	Drive end bearing	65	Extension for NDE grease nipple
3	Rotor	33	DE internal cover (front)	70	Stator terminal box
5	Drive end shield (DE)	35	Moving part of DE grease valve (front)	74	Stator terminal box lid
6	Non-drive end shield (NDE)	40	Cover fixing screw	81	Cable gland support plate
7	Fan	42	DE grease nipple (front)	89	Connection - Terminal box nozzle (optional)
10	Turbine or fan screw	43	Extension for DE grease nipple	122	Stirrer (only from 315 M to 355 LD)
11	Brake washer (not shown)	44	DE preloading (wavy) washer (from 315 M)	270	DE shield fixing screw
12	Lock washer	50	NDE bearing (rear)	271	DE shield fixing nut
13	Fan cover	53	NDE internal cover (rear)	273	NDE shield fixing screw
21	Shaft extension key	56	Moving part of NDE grease valve (rear)	406	Cover plate of DE grease valve (front)
26	Nameplate	59	NDE preloading (wavy) washer (315 ST)	456	Cover plate of NDE grease valve (rear)



H5 - Identification, exploded views and parts list

#### H5.7 - FRAME SIZE: 355 LK to 450



Frame size: 355 LK to 450						
No.	Description	No.	Description	No.	Description	
1	Wound stator	27	Fan cover screw	65	Extension for NDE grease nipple	
2	Housing	30	Drive end bearing	70	Stator terminal box	
3	Rotor	33	DE internal cover (front)	74	Stator terminal box lid	
5	Drive end shield (DE)	35	Moving part of DE grease valve (front)	81	Cable gland support plate	
6	Non-drive end shield (NDE)	40	Cover fixing screw	89	Connection - Terminal box nozzle	
7	Fan	42	DE grease nipple (front)	121	Air circulator	
10	Turbine or fan screw	43	Extension for DE grease nipple	230	Auxiliary terminal box (355 LK to 450)	
11	Brake washer (not shown)	44	DE preloading (wavy) washer	270	DE shield fixing screw	
12	Lock washer	50	NDE bearing (rear)	271	DE shield fixing nut	
13	Fan cover	53	NDE internal cover (rear)	273	NDE shield fixing screw	
21	Shaft extension key	56	Moving part of NDE grease valve (rear)	406	Cover plate of DE grease valve (front)	
26	Nameplate	64	NDE grease nipple (rear)	456	Cover plate of NDE grease valve (rear)	















### LEROY-SOMER

#### I - SCOPE OF APPLICATION

These General Conditions of Sale ("GCS") shall apply to the sale of all products, components, software and services (referred to as "Products") proposed or sold by the Seller to the Client. Said GCS shall also apply to all quotation or offers made by the Seller, and are an integral part of all orders. "Seller" is understood to mean all companies directly or indirectly controlled by LEROY-SOMER. As a complementary measure, orders are also subject to the latest version in force of the Inter-Union General Conditions of Sale for France of the F.I.E.E.C. (Fédération des Industries Electrical, Electroniques et de Communication [Federation of Electrical, Electronic and Communication Industries]], inasmuch as they are not contrary to the GCS.

The acceptance of the Seller's offers or quotations, or any order, entails the acceptance without reservation of these GCS and rules out all contrary provisions shown on all other documents and, in particular, on the Client's order forms and the Client's General Conditions of Purchase.

Purchase. If the sale concerns castings, by way of derogation to Paragraph 1 above, said castings shall be subject to the latest version in force of the *Conditions Générales Contractuelles des Fonderies Européennes* [General Contractual Conditions of European Foundries]. The Products and services sold pursuant to these GCS may under no circumstances be used for applications in the nuclear field, as such sales expressly fall under technical specifications and specific contracts that the Seller reserves the right to refuse.

### II - ORDERS

I - ORDERS
 All orders, even those taken by the Seller's agents and representatives, and regardless of the transmission method, shall only bind the Seller atter written acceptance thereby of the order.
 The Seller reserves the option of modifying the characteristics of its Products without notice. However, the Client shall retain the possibility of specifying the characteristics on which its commitment is contingent. In the absence of any such express stipulation, the Client may not refuse delivery of new, modified Products.
 The Seller may not be held liable for an unsatisfactory selection of Products if said selection results from conditions of use that are incomplete and/or mistaken, or not disclosed to the Seller by the Client. Except in the event of a stipulation to the contrary, the offers and quotations remitted by the Seller shall only be valid for thirty days as from the date on which they are drawn up.
 Where the Products must comply with standards, specific regulations and/or be received by control and inspecting agencies, the price request must be accompanied by the technical specification, all terms and conditions the Seller must comply with. Reference shall be made thereto on the quotation or offer. Approval and attendance costs shall always be borne by the Client.

#### III - PRICES

Tariffs are expressed exclusive of tax and may be revised without notice.

notice. Prices are either deemed to be firm for the period of validity specified on the quotation, or subject to a revision formula attached to the offer and which specifies, according to the regulations, parameters pertaining to the materials, products, various services and salaries for which the indices are published in the B.O.C.C.R.F. (*Bulletin Officiel de la Concurrence, de la Consommation et de la Répression des Fraudes* [French Official Journal of Competition and Consumer Matters, and Anti-Fraud Measures]

Anti-Fraud Measures), and consenter matters, and Anti-fraud Measures), and Anti-fraud Measures), and All additional costs, in particular approval costs, specific checks, etc., shall be invoiced in addition.

#### IV - DELIVERY

IV - DELIVERY Sales are governed by the latest edition in force of the INCOTERMS published by the Internal Chamber of Commerce ("I.C.C. INCOTERMS"). The Products shall be dispatched according to the conditions stated on the order acknowledgement issued by the Seller for all orders of Products.

Products: the event of specific provisions, the prices correspond to Except in the event of specific provisions, the prices correspond to Products that are made available in the Seller's factories, including basic packaging. Except in the event of a provision to the contrary, the Products shall always be transported at the risk of the addressee. In all cases, it shall be the responsibility of the addressee to make any claims to the carrier, within the delivery time and in the forms specified by law, concerning the state or number of parcels received, and to concomitantly provide the Seller with a copy of such declaration. Failure to comply with said procedure shall exempt the Seller from any liability. In any event, the Seller's liability may not exceed the amount of the indemnities received from its insurers.

Seller's liability may not exceed the amount of the indemnities received from its insurers. If the provisions concerning transportation are amended by the Client subsequent to the acceptance of the order, the Seller reserves the right to invoice any supplemental costs that may result therefrom. Except in the event of a contractual or statutory obligation to the contrary, packaging shall not be returnable. In the event that a delivery of Products is delayed for a reason not attributable to the Seller, the Products stored on the Seller's premises shall be insured at the exclusive risk of the Client. Consideration for storage, costs will be invoiced at a rate of 1% (*one per cent*) of the total amount of the order, per week or partial week of storage, with no deductible or *de minimis* amount, as from the date of Products availability provided for in the contract. Upon expiration of a period of thirty days as from said date, the Seller may, at its discretion, either freely dispose of the Products, or invoice the Client in full for payment, according to the timeframes and amount provided for contract.Upon expiration of a period of the noder, said Products, or invoice the Client in full for payment, according to the timeframes and amount provided for contractually. In any event, down payments shall inure to the Seller as indemnities, without prejudice to any other action the Seller may take.

#### V - DELIVERY TIME

V - DELIVERY TIME The Seller shall only be bound by the delivery time mentioned on its order acknowledgement. Said delivery time shall only start to run as from the date of issuance of the order acknowledgement by the Seller, and subject to the fulfilment of the conditions provided for on the confirmation receipt, in particular receipt of the down payment for the order, notification of the opening of an operative irrevocable and confirmed documentary credit that complies in all respects to the Seller's request (in particular regarding the amount, currency, validity and licence), acceptance of the payment conditions accompanied by the implementation of any guarantees requested, etc. Exceeding delivery time shall not grant the Client entitlement to damages and/or penalties. Except in the event of a specific condition to the contrary, the Seller reserves the right to make partial deliveries. Delivery times shall be interrupted by right and without the need for any judicial formalities, by any failure to pay or late payment by the Client.

VI - TESTS - QUALIFICATION The Products manufactured by the Seller are checked and tested before leaving its factories. Clients may be present at said tests if specified on the order. Specific tests and/or trials, as well as approval of Products, requested by the Client, whether carried out on the Client's premises or in the Seller's factories, on site, or by control and inspection agencies, must be specified on the order and are always at Client's expense. Prototypes for Products specially developed or adapted for a Client must be qualified by the Client before serial production in order to ensure that it is compatible with the other components that make up its equipment, and that it is adapted to the intended use. Said qualification will also enable the Client to ensure that the Products comply with the technical specification. In this respect, the Client and Seller shall sign a Product Approval Form in two original, one of which shall be retained by the Client and one by the Seller.

In the event that the Client requires delivery without having firstly qualified the Products, said Products shall be delivered as they stand and shall always be deemed to be prototypes ; the Client shall then be solely liable for using the Products or delivering them to its own clients. However, the Seller may also decide not to deliver the Products that have not received the Client's prior approval.

#### VII - PAYMENT CONDITIONS

All sales shall be deemed to be completed and payable at the Seller's registered office, without any possible derogation, regardless of the payment method, where the contract was concluded and where payment method, delivery was made

defivery was made. Where the Client is located out of French territory, invoices shall be payable in cash upon receipt, or by a bank draft or a bill of exchange, within 30 (thirty) days net. All early payment compared to the deadline fixed shall give right to a discount of 0.2% (*nought point two* per cent) per month, of the amount concerned of the invoice. Except in the event of provisions to the contrary, where the Client is located outside of French Territory, invoices shall be payable in cash against remittance of shipping documents, or by irrevocable documentary credit confirmed by a first rate French bank, at Client's expense.

expense. Payment shall be understood to mean the funds being made available on the Seller's bank account and must imperatively be made in the

on the Seller's bank account and must imperatively be made in the invoicing currency. Pursuant to French Law no. 2001-420 of 15 May 2001, failure to pay an invoice when due shall trigger, after service of formal notice that has remained without effect, payment to the Seller of a flat-rate penalty on the due date of the receivable, which shall be applied to amount inclusive of tax of monies owed if the invoice is liable to VAT (Value Added Tax), and the suspension of pending orders. Said penalty is equal to the European Central Bank Rate + 7 basis points. The collection of said monies via littorian shall trioger an increase of

equal to the European Central Bank Hate + 7 basis points. The collection of said monies via litigation shall trigger an increase of 15% (fifteen per cent) of the amount claimed, with a minimum of Euros 500 exclusive of tax (five hundred euros exclusive of tax), with tax in addition if due. Moreover, subject to compliance with the statutory provisions in force,

Moreover, subject to compliance with the statutory provisions in force, in the event of total or partial failure to pay any invoice or instalment whatsoever, regardless of the payment method used, all amounts that remain owed to the Seller (including its subsidiaries, affiliated or allied companies, whether French or foreign) for all deliveries and services, regardless of the due date originally provided for, shall immediately come due

become due. Notwithstanding any specific payment conditions provided for between the parties, the Seller reserves the right to require, in the event of a decline in the Client's credit rating, a payment incident or bankruptcy of the Client's the Client

the payment in cash, before the Products leave the factory, for all the payment in cash, before in Froduct orders currently being fulfilled, - down payments to be made on all orders, - alternative or different payment guarantee

### VIII - PAYABLE AND RECEIVABLE BALANCE Except where prohibited by law, the Seller and the Client expressly agree to balance their payables and receivables arising from their trade relations, even if all conditions defined by law for legal balancing are not met.

For the application of said clause, the Seller shall mean any company of the LEROY-SOMER Group.

#### IX - TRANSFER OF RISK / RESERVE OF TITLE

Risk shall be transferred as soon as the Products are made available, according to the delivery conditions stipulated on the order actioned doment

Available, according to the delivery conditions stipulated on the order acknowledgement. The transfer to the Client of title shall take place after payment in full. In the event that the restitution of the Products delivered is claimed by the Seller, the Seller is entitled to retain any down payment as compensation. Remittance of a bill that creates an obligation to pay (bill of exchange or other) shall not constitute payment and discharge. For as long as the price has not been paid in full, the Client is required to inform the Seller, within twenty-four hours, of the sequestration, requisition or confiscation of the Products for the benefit of a third party, and to take all protective measures to make known the Seller's property right in the event of action by creditors, and to cause such right to be respected.

#### - CONFIDENTIALITY

X - CONFIDENTIALITY Each of the parties undertakes to maintain the confidentiality of all technical, trade, financial or other information received from the other party, whether orally, in writing or by any other means of communication, when any order is negotiated and/or fulfilled. This confidentiality obligation shall apply throughout the period during which the order is fulfilled and for 5 (five) years subsequent to completion or cancellation thereof, regardless of the reasons therefor.

#### XI - INDUSTRIAL AND INTELLECTUAL PROPERTY

XI - INDUSTRIAL AND INTELLECTUAL PROPERTY Data, studies, results, information or software, whether patentable or not obtained by the Seller when any order is fulfilled shall remain the exclusive property of the Seller. With the exception of instruction and maintenance manuals, documents of any nature remitted to the Client shall remain the exclusive property of the Seller and must be returned to it upon request, even if the Client was invoiced for part of the cost of the study, and said documents may not be disclosed to third parties or used without the Seller's prior written arcement

#### - CANCELLATION / TERMINATION

XII - CANCELLATION / TERMINATION The Seller reserves the right to cancel or terminate immediately, at the Seller's discretion, by right and without the need for any judicial formalities, the contract in the event of failure to pay any portion whatsoever of the price, when due, or in the event of any breach of any of the Client's contractual obligations. Down payments and any amount already paid shall remain in Seller's hands in the form of indemnities, without prejudice to the Seller's right to claim damages. In the event that the contract is cancelled, the Products must be returned to the Seller immediately, regardless of where the Products are located, at Client's expense and risk, under penalty of 10% (*ten per cent*) of the value thereof, per week's delay. thereof, per week's delay

#### XIII - WARRANTY

The Seller warrants the Products against all operating defects caused by a material or manufacturing fault, for a period of twelve months as from the date on which the Products are made available, unless a diffe nt statutory provision subse quently applies, under the c

defined below. The warranty may only be triggered insofar as the Products have been stored, used and maintained in accordance with the Seller's instructions stored, used and mainfained in accordance with the Seller's instructions and manuals. The warranty does not apply where the defect results, in particular, from : - inadequate monitoring, maintenance or storage, - normal wear and tear on the Products, - servicing or modification of the Products without the Seller's prior written authorisation, - abnormal use of the Products or use of the Products for a purpose other than that intended, - faulty installation of the Products on the premises of the Client and/or the end user.

the end user, - failure by the Client to disclose the purpose or conditions of use of the Desturbe

failure to use genuine spare parts, force majeure or any event that is beyond the control of the Seller.



In any case, the warranty is limited to the replacement or repair of the parts or Products deemed faulty by the Seller's technical departments. If the repair is entrusted to a third party, the repair shall only be carried out once the Seller has agreed to the quotation for the repair.

All Products returns must have been given the Seller's prior, w

The Products to be repaired must be dispatched carriage paid, to the address given by the Seller. If the Products are not accepted under warranty, their return to the Client shall be invoiced to the Client or the end user

This warranty shall apply to the Seller's Products that are made readily available and therefore does not cover the de-installation and re-installation of said Products in the equipment into which it is mounted. Repair, modification or replacement of any part or Product during the warranty period may not result in the warranty period being extended. The provisions of this article constitute the Seller's sole obligation concerning the warranty of the Products delivered.

#### XIV - LIABILITY

The Seller's liability is strictly limited to the obligations stipulated in these GCS and those expressly accepted by the Seller. All penalties and indemnities provided for therein constitute lump sum damages that include discharge for the Seller and are exclusive of any other penalty activide weither the seller. or indemnification

With the exception of the Seller's gross negligence and the compensation of bodily injury, the Seller's liability shall be limited, in total, to the contractual amount, exclusive of tax, of the Product(s) that give(s) right to compensation. The Seller may under no circumstances be required to indemnify consequential, indirect and / or punitive damages that the Client may use as the basis for a claim; as a result, the Seller may not be required to indemnify in particular, production losses on portation losses or lost

to indemnify, in particular, production losses, operating losses or lost profit or, in general, any damage eligible for indemnification other than bodily injury or damage to property.

The Client undertakes to hold harmless the Seller and / or its insurers from any and all claims made by its insurers and/or any third party in a contractual relation with the Client, in excess of the limit and for the exclusions listed above.

#### XV - SPARE PARTS AND ACCESSORIES

Spare parts and accessories shall be supplied upon request, to the extent of their availability. Associated costs shall be invoiced in addition. The Seller reserves the right to require a minimum quantity or invoicing amount per order.

#### **XVI - WASTE MANAGEMENT**

AVI - WAS IE MARAGEMENT The Products that form the purpose of the sale does not fall within the scope of the European Directive 2002/96/EC (WEEE) dated January 27<sup>th</sup>, 2003, and all related legislation of Member States of the European Union that result therefrom, on the composition of electrical and electronic equipment and the disposal of waste from such equipment. In accordance with Article L 541-2 of the French Environment Code, it is the responsibility of the waste holder to ensure the disposal thereof or to cause the disposal thereof at its own expense.

#### XVII - FORCE MAJEURE

XVII - FORCE MAJEURE With the exception of the Client's obligation to pay the monies owed to the Seller in respect of an order, the Client and Seller may not be held liable for the total or partial failure to perform their contractual obligations if such failure results from the occurrence of a force majeure. Delays or disturbances in production that totally or partially result from war (whether declared or not), terrorist act, strikes, riots, accidents, fires, floods, natural disasters, transportation delays, shortage of components or materials, governmental decision or action (including prohibition on import/export or the withdrawal of an import/ export licence) shall, in particular, be deemed a force majeure.

export licence) shall, in particular, be deemed a force majeure. If one of the parties is delayed or prevented from performing its obligations by reason of this Article for a period in excess of 180 consecutive days, each party may then terminate, by right and without any need for judicial formalities, the unperformed part of the order, by written notice to the other party, without liability. However, the Client shall be required to pay the price agreed pertaining to the Products already delivered on the date of termination.

#### XVIII - PROHIBITION ON UNLAWFUL PAYMENTS

The Client shall refrain from being engaged in any activity that would expose the Seller or any of its affiliates to a risk of penalties under laws and regulations of any relevant jurisdiction prohibiting improper payments, including but not limited to bribes or gifts of an obviously unreasonable amount, to any government or agency officials, to political parties or their officials or candidates for public office, or to any employee of any customer or supplier.

#### XIX - TRADE COMPLIANCE LAWS

XIX - TRADE COMPLIANCE LAWS The Client agrees that all applicable import, export control and sanctions laws, regulations, orders and requirements, as they may be amended from time to time, including without limitation those of the European Union, the United States of America, and the jurisdictions in which the Seller and the Client are established or from which Products may be supplied, and the requirements of any licences, authorisations, general licences or licence exceptions relating thereto (Trade Compliance Laws") will apply to its receipt and use of Products, as well as related services and technology. In no event shall the Client use, transfer, release, export or re-export the Products, related services or technology in violation of Trade Compliance Laws. Seller shall have no obligation to supply any. Products, or services

Seller shall have no obligation to supply any Products, or services unless and until it has received any necessary licences or authorisations or has qualified for general licences or licence exceptions under Trade Compliance Laws.

exceptions under I rade Compliance Laws. If for any reason any such licences, authorisations or approvals are denied or revoked, or if there is a change in any Trade Compliance Laws that would prohibit Seller from fulfilling the contract, or would in the reasonable judgement of Seller otherwise expose Seller and/or Seller's Affiliate(s) to a risk of liability under Trade Compliance Laws, Seller shall be relieved without liability of all obligations under the contract contract

#### XX - SEVERABILITY

All clauses and/or provisions of these General Conditions that are deemed or become null or void shall not cause the nullity or voidance of the contract, but solely the clause and/or provision concerned.

#### XXI - DISPLITES

THIS CONTRACT SHALL BE GOVERNED BY AND INTERPRETED IN ACCORDANCE WITH THE LAWS OF FRANCE.

IN ACCORDANCE WITH THE LAWS OF FRANCE. ANY DISPUTE IN RELATION TO THE INTERPRETATION OR THE EXECUTION OF THIS CONTRACT NOT AMICABLY SETTLED BETWEEN THE PARTIES WITHIN A 30 DAY PERIOD, SHALL BE SETTLED BY THE COMPETENT COURT OF ANGOLIÊME (FRANCE), EVEN IN THE CASE OF INTRODUCTION OF THIRD PARTIES OR THE ENVOLVEMENT OF SEVERAL DEFENDANTS. HOWEVER, THE SUPPLIER RESERVES THE EXCLUSIVE RIGHT TO BRING THE DISPUTE TO THE COMPETENT COURTS OF THE SELLER OR THE CLIENT.



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RCS ANGOULÊME N° B 671 820 223 S.A. au capital de 62 779 000 €

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